# Jet-Induced Ground Effects on a Parametric Flat-Plate Model in Hover

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# **Summary**

The jet-induced forces generated on short takeoff and vertical landing (STOVL) aircraft when in close proximity to the ground can have a significant effect on aircraft performance. Therefore, accurate predictions of these aerodynamic characteristics are highly desirable. Empirical procedures for estimating jet-induced forces during the vertical/short takeoff and landing (V/STOL) portions of the flight envelope are currently limited in accuracy. The jet-induced force data presented in this report significantly add to the current STOVL configurations data base. Further development of empirical prediction methods for jet-induced forces, to provide more configuration diversity and improved overall accuracy. depends on the viability of this STOVL data base. The data base may also be used to validate computational fluid dynamics (CFD) analysis codes.

This report presents the hover data obtained at the NASA Ames Jet Calibration and Hover Test (JCAHT) facility for a parametric flat-plate model. The model tested was designed to allow variations in the planform aspect ratio, number of jets, nozzle shape, and jet location. There were 31 different planform/nozzle configurations tested. Each configuration had numerous pressure taps installed to measure the pressures on the undersurface of the model. All pressure data, along with the balance jet-induced lift and pitching-moment increments, are tabulated. For selected runs, pressure data will be presented in the form of contour plots that show lines of constant pressure coefficient on the model undersurface. Nozzle-thrust calibrations and jet-flow-pressure survey information are also provided.

# Nomenclature

Nomenciature		
A <sub>jet</sub>	sum of jet area for a given configuration, in. <sup>2</sup>	
axial	balance axial force, lb	
cp	pressure coefficient, $\Delta p/q_{jeb}$ psi	
d	individual jet diameter, in.	

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D <sub>e</sub>	equivalent jet diameter based on total jet area, in.		
e	half the distance between adjacent jets, in.		
h	model height above ground plane, in.		
$\Delta L$	jet-induced lift, lb		
$N_1$	balance normal force number 1, lb		
$N_2$	balance normal force number 2, lb		
p	pressure, psig		
Pamb	ambient pressure, psia		
Pref	reference pressure, psig		
Pt	local total pressure, psia unless noted		
Pt,n	total pressure of the nozzle, psia		
Pt/Pamb	nozzle pressure ratio		
Pt,z	total pressure at distance Z, psia		
Δp	pressure difference, psi		
ΔΡΜ, ΔΜ	jet-induced pitching moment, inlb		
<b>q</b> jet	jet dynamic pressure, $q_{jet} = T/(2 * A_{jet})$ , psi		
$\mathbf{q}_{\mathbf{n}}$	jet dynamic pressure at the nozzle exit, psi		
$q_z$	jet dynamic pressure at distance Z, psi		
T	total jet thrust for a given configuration, lb		
$V_{\infty}$	freestream velocity, ft/sec		
X	longitudinal position on the planform with $X = 0$ halfway between the nozzle set, in.		
$\mathbf{X}_{\mathbf{n}}$	longitudinal distance from the nozzle center, in.		
$\mathbf{Y}_{\mathbf{n}}$	lateral distance from the nozzle center, in.		
Y	lateral position on the planform with $Y = 0$ along planform plane of symmetry, in.		

distance downstream of the nozzle exit, in.

#### Introduction

A test program to expand the data base on jet-induced forces for short takeoff and vertical landing (STOVL) aircraft both in and out of ground effect has been completed. The test program addresses multi-jet suckdown, fountain effects, ground vortex effects of a single circular or rectangular jet, and twin rectangular thrust reverser effects. Hover tests performed at NASA Ames Research Center from January 25, 1991, to March 8, 1991, are reported. In addition to force balance instrumentation, all test models contained pressure instrumentation on the undersurface. Forward-speed data from NASA Langley Research Center for similar configurations are reported in reference 1.

Data from these tests add significantly to the current jet-induced force data base for STOVL configurations. Further development of empirical prediction methods for jet-induced forces, to provide more configuration diversity and improved overall accuracy, depends on the viability of this STOVL data base. In addition, computational fluid dynamics (CFD) codes can be validated using this data base.

The available data and the shortfalls of the existing data base (for hover) are briefly addressed. A detailed discussion of the limitations of current prediction methodology for jet-induced forces is provided in reference 2. The JCAHT facility, the models used in the hover tests, and the instrumentation used with these models are described. Finally, the test data are presented, including nozzle calibrations, along with a short discussion on some of the data. A sketch of each configuration tested and the tabulation of the data are included in the appendix.

# **Background**

Accurate predictions of the aerodynamic characteristics for advanced STOVL aircraft in close proximity to the ground are highly desirable. The jet-induced forces generated on these aircraft can have a significant effect on aircraft performance, especially when calculating thrust and control requirements for operations close to the ground. Thus, the ability to accurately estimate the jet-induced ground effects of vertical/short takeoff and landing (V/STOL) aircraft becomes an important part of the design procedure and cannot be overlooked. Several empirical estimating procedures for jet-induced ground effects are available for the hover and short takeoff and landing (STOL) portions of the flight regime, but are limited in accuracy (ref. 2).

The existing STOVL-configuration data base for jetinduced forces is insufficient to enable the development of a methodology to adequately predict the aerodynamics characteristics of configurations which are of current interest. This includes configurations with high disk loading (nozzle pressure ratios (NPRs) greater than 2), large planform-to-jet area ratios (greater than 100), nonsymmetric thrust and jet patterns, and widely differing undersurface geometries.

The ground effects induced by jet flows impinging on the ground are dependent on many aircraft parameters. The complete aircraft configuration (jet shape, location, angle, and number, along with the shape of the aircraft planform and undersurface) is an important factor in the magnitude of the ground effects encountered.

The relative positioning and the number of the jets are strong factors in determining jet-induced effects. Multi-jet configurations can experience large lift losses (suckdown) and large fountain effects during hover. Figure 1(a) shows the different flow regions around an aircraft in hover. Figure 1(b) shows the flow regions during forward flight or crosswind hover close to the ground. In this situation a "ground vortex" is formed by the collision of the jet flow along the ground with the free-stream air. This vortex can significantly alter the suckdown forces by further changing the flow field around the aircraft. Existing isolated jet investigations of the ground vortex have shown that the test conditions can affect the vortex size and shape. It appears that the ground boundary associated with testing in a wind tunnel is one significant parameter in predicting the effects of the ground vortex (ref. 3).

The current empirical prediction methods for the jetinduced aerodynamic characteristics of STOVL configurations require the summation of several parameters. The overall accuracy is limited to that of each individual parameter. Table 1 presents the individual increments of the current prediction methods for STOVL- or V/STOLaircraft lift during hover and an assessment of the prediction accuracy for each increment.

Table 1. Accuracy of current prediction methods

Increment	Accuracy of method	
1. Base loss out-of-ground effect	Adequate	
2. Equivalent single-jet suckdown	Under estimated	
3. Fountain lift	Over estimated	
4. Additional multi-jet suckdown	Over estimated	

The existing methodology can reasonably predict the sum value of these four items for limited configurations. The over estimation of the fountain lift (item 3) and the additional multi-jet suckdown (item 4) tend to cancel, giving a

correct total jet-induced lift-increment. However, most new configurations are outside of the existing data base, and the sum of over estimation of the fountain and multijet terms (items 3 and 4) provides poor results.

Also, the prediction methods do not provide an estimate of pitching moments induced in hover for configurations that are not symmetrical fore and aft. Since most configurations are not symmetrical fore and aft, no empirical prediction methods exist for pitching moments during hover. Better prediction or measurement of the parameters is required to use the methodology for more diverse configurations. Obtaining pressure data on and around the model will improve the current prediction methods.

A more detailed discussion of the limitations of the current jet-induced effects prediction methodology is provided in reference 2.

# **Facility Description**

#### General

The NASA Ames Jet Calibration and Hover Test (JCAHT) facility is shown in figure 2 (ref. 4). This facility provides jet-induced effects data on STOVL configurations both in and out of ground effect during hover in still air. The facility consists of a hover test rig (HTR), a jet calibration rig (JCR), and a jet-wake survey rig. Two high-pressure supply lines can be independently controlled, providing up to 300 psig air at either the JCR or the HTR.

The JCAHT facility was used to calibrate each of the nozzles used at the Ames and Langley test facilities, and to obtain extensive hover characteristics for a series of nozzle arrangements and flat-plate planforms.

#### **Hover Test Rig**

The hover test rig (HTR) is the heart of the JCAHT facility. It is used to measure the jet-induced forces on a STOVL model hovering in and out of ground effect. A picture of the delta-wing model attached to the HTR is shown in figure 3. The forces on the model are measured by a six-component strain-gage balance that is supported from the structure of the rig and is located between the nozzle plenum assemblies. The plenums and associated nozzles are attached directly to the rig, but do not make contact with the model (i.e., the nozzles are nonmetric). By attaching only the model to the balance, the jet-induced forces imposed on the model can be directly measured. Gaps between the model and nozzles are kept

as small as possible (nominally 0.05 in.) to minimize or eliminate errors from flow entrainment through the gap.

In order to simulate different heights above the ground, a ground plane is moved to different heights relative to the model by a remote-control hydraulic lift fixed to the rig. For the tests described in this report, the ground plane was  $8 \text{ ft} \times 8 \text{ ft}$  (fig. 4) and was centered underneath the model.

To get the test data in a nondimensional form to compare with other model configurations and sizes, the thrust, flow angles, and velocity profiles of the jets installed on the HTR must be known. The JCR is used for this purpose.

### **Jet Calibration Rig**

The jet calibration rig (JCR) is used to calibrate thrust (jet force) that is not measured on the HTR and is used for correlation with a reference pressure that can be measured on the HTR. The JCR measures thrust forces produced by a jet flow and is shown in figure 5(a). High-pressure air enters the rig from the left, and is split into two flows that travel through a set of balance isolation coils designed to minimize pressure effects on the balance. The two airflows are brought back together at an outlet plenum that sits directly over the balance on the right side of the rig. The plenum and nozzle arrangements to be tested are bolted in an inverted position (jet flow pointed up) directly to the outlet plenum. Both the thrust magnitude and the thrust angle of the jet can be determined from the balance readings. A total-pressure probe is available for measuring the pressure distribution at the exit plane of the nozzle. This total pressure is used to calculate NPR (an important parameter in correlating jet-induced effects) and to correlate with a nozzle reference pressure located within the nozzle-plenum assembly. The correlation between total and reference pressure is used while operating the nozzle on the HTR to provide thrust and NPR information.

#### Jet-Wake Survey Rig

The jet-wake survey rig is a three-axis traverse mechanism. Located next to the JCR, it positions a Pitot survey probe (fig. 5(a)). The Pitot probe measures the total pressure in the nozzle flow (fig. 5(b, c)). The Pitot probe can be moved on all three axes to provide nozzle exit-flow survey traces parallel to or perpendicular to the nozzle exit plane.

# **Model Description**

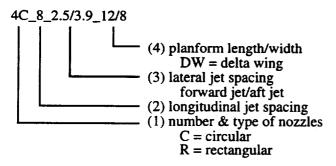
The parametric flat-plate model tested on the HTR had modular panels (with and without pressure taps). There

were a variety of nozzles that could be placed at different locations in and around the model. Details about the planform panels, the nozzles, and the model instrumentation follow.

#### Planform Panels

The planform panels tested on the HTR included a delta wing and several rectangular shapes. The planform shape, nozzle spacing, number of nozzles, and NPR were varied to produce 31 different configurations. The planforms were designed to be modular so pieces could be interchanged to provide many different configurations with minimal hardware. In addition to the pressureinstrumented delta wing (fig. 6(a)), there were 17 different rectangular plates labeled P1-P17. Figure 6(b) shows some of these plates; note the circular and rectangular nozzle cutouts. Plates P1-P13 were instrumented with pressure taps, while plates P14-P17 were not. Pressuretap numbers were uniquely assigned starting with the delta wing and ending with plate P13. This provided pressure tap numbers ranging from 1 to 242. Although numbered, ports 92 and 158 were not installed in the model and do not appear in the data or configuration files. A summary of the 31 configurations tested is provided in figure 7(a-c). The appendix contains a 1:4 sketch of each configuration tested and the data obtained.

Each configuration has an associated code name that describes the planform and nozzle parameters. The configuration code is made up of four parts separated by an underline character:



This configuration code refers to a configuration with four circular jets. The longitudinal (forward to aft) jet spacing is 8 in. The forward-jet lateral spacing is 2.5 in. and the aft-jet lateral spacing is 3.9 in. The planform is 12 in. long and 8 in. wide. Two other examples of configuration code names are:

The first example refers to a model with two circular jets with a 12 in. spacing. Side-by-side jet spacing is zero; therefore, the jets are along the model centerline. The planform is the delta wing. The second example has three circular jets with a forward to aft jet spacing of 16 in. The two forward jets are laterally spaced 2.5 in. apart and the remaining aft jet is located along the centerline. The planform is 20 in. long and 8 in. wide.

Nominally, half of each planform was instrumented with pressure taps (fig. 8) since the planforms and nozzle arrangements were symmetrical about the body longitudinal centerline. Exceptions were planforms with 2.5 in. and 3.9 in. side-by-side nozzles where pressure taps were located laterally along the centerline passing through the two nozzles (fig. 9). Flow patterns between the nozzles at low heights were anticipated to be, and sometimes found to be, nonsymmetrical. Detailed pressure-tap locations are provided in appendix A after the model sketch for each configuration tested. Although there were 31 planform and nozzle arrangements, there were actually 32 different pressure-field configurations tested. Configuration 2C\_16\_0\_12/24 had two different pressure-tap layouts. To provide more data on the fountain decay on the aircraft undersurface, plates P2 and P11 were switched. This second configuration was designated with an "X" at the end of the code name (2C\_16\_0\_12/24X).

With the exception of the delta-wing planform, the modular planform pieces were held together with a frame made from aluminum 90 deg angle stock. The L-shaped corner of the aluminum angle stock was kept toward the inside of the frame structure to keep the model edge as thin as possible; unpublished data indicate that the edge contour can affect the jet-induced characteristics.

#### **Nozzles**

There were six nozzles calibrated on the Ames JCR. Each nozzle had a "type" designation of 1–6. Table 2 provides a short description of each nozzle type. Table 3 summarizes nozzle geometry and the configurations with which they were used.

Table 2. Description of the nozzle types used

Nozzle type	Description
1	Forward circular nozzle
2	Aft circular nozzle
3	Twin 3.9 in. center-to-center nozzles
4	Twin 2.5 in. center-to-center nozzles
5	Aft rectangular nozzle
6	Forward rectangular nozzle

Table 3. Summary of nozzle information

Nozzle type	Diameter or length/width	Area (in. <sup>2</sup> )	Used on configuration
1	1.2 in.	1.13	All 2C_[8,12,16] All 3C3.9
2	1.2 in.	1.13	All 2C_[8,12,16] All 3C2.5
3	0.87 in. each	1.16 total	2C_0_3.9_12/8
(3.9 in. spacing)	$D_e = 1.22 \text{ in.}$		3C_8_3.9_12/8
			3C_12_3.9_16/8
			3C_16_3.9_20/8
			All 4C
4	0.85 in. each	1.13 total	2C_0_2.5_12/8
(2.5 in. spacing)	$D_e = 1.20 \text{ in.}$		3C_8_2.5_DW
			3C_8_2.5_12/8
			3C_12_2.5_DW
			3C_12_2.5_16/8
			3C_16_2.5_20/8
			All 4C
5, 6	$0.613 \text{ in.} \times 1.840 \text{ in.}$	1.13	All 2R
	$D_e = 1.20 \text{ in.}$		

Because the models for both the Ames HTR and the Langley wind tunnel were nonmetric with the nozzles, the nozzles had to be calibrated for thrust. This calibration (performed with the JCR) provided the necessary thrust and nozzle-pressure calibrations so that the correct nozzle conditions could be set and monitored when run on the HTR or at the Langley wind tunnel. A more detailed discussion of each nozzle type is presented under "Nozzle Calibrations/Surveys" in the "Jet Calibrations" section.

The NPR is defined as the nozzle total pressure divided by room (ambient) total pressure, and is the primary flow parameter used in empirical jet-induced prediction techniques. An NPR of 1.0 means no air is flowing through the nozzle.

Total-pressure surveys were obtained at the nozzle exit planes in order to calculate the actual NPR. The surveys were used to document the jet-exit velocity profile, and can be used to indicate how well the nozzles are performing. Exit profiles are shown under "Nozzle Calibrations/ Surveys" in the "Jet Calibrations" section.

#### Instrumentation

Measurements during model testing on the HTR consisted of room (ambient) pressure and temperature, model surface pressures, and nozzle reference pressures. Model surface pressures from all plates to be tested were plumbed to four mechanical scanivalve connectors.

The instrumentation used during this test consisted of two six-component strain-gage balances, a scanivalve module consisting of four 48-port scanivalves, various pressure transducers for measuring nozzle, plenum, and ambient pressures, and one thermocouple for measuring ambient temperature.

The balance is used to measure model jet-induced aerodynamic forces while on the HTR or the nozzle thrust while on the JCR. Since the balance is comprised of six different gages, a load on any single gage will also produce some output (usually small) on the other gages; these are referred to as "gage interactions." These interactions are taken into account by the data acquisition system as part of the balance calibration data. The balance used on the JCR during this test was a 1.5-in.-diameter strain-gage balance. The balance gage capacities are 300 lb on the axial gage, 500 lb on the normal force gages (N1 and N2). 250 lb on the side force gages (S1 and S2), and 60 ft/lb on the rolling-moment gage. A similar balance was used for the HTR with the only difference being a 100 lb limit on the axial gage. During data acquisition on the HTR, the scanivalves were stepped through all 48 ports at each height. Each height was considered one run point. The rate of acquisition was approximately 1 port/second.

A 25 psia pressure transducer and a thermocouple were used to measure the room (ambient) pressure and temperature during testing.

#### Jet Calibrations

Data from the JCR calibration were used when calibrating the nozzles. Calibrations from the nozzles were in turn used when testing the model on the HTR. The "Calibration of the Jet Calibration Rig" section will explain how the calibration was done and provide the corresponding results. The "Nozzle Calibrations/Surveys" section will present pressure and thrust data along with pressure surveys of the nozzle flow. The final section, "Comparison of Jet Decay Rates," compares the jet decay rates between the current nozzle sets and selected studies.

#### Calibration of the Jet Calibration Rig

The JCR is designed to minimize forces on the balance due to the high pressure air lines so that only the forces from the jet (or thrust system) are obtained. The high-pressure air lines induce a force on the balance which must be calibrated out so that only the jet forces are obtained. Each of the six nozzle sets calibrated on the JCR were mounted so that their thrust was directly in line with the balance axial gage. The six-component strain-gage balance was mounted on the JCR with the axial gage perpendicular to the floor.

The calibration of the JCR consisted of determining the effect of the rig components on the balance. Pressurizing the coils (when running) may produce a small force in the balance normal direction and possibly a small amount in the axial direction (trying to unwind the coils). Since the coil system is symmetrical, no forces should be seen on the balance side force or rolling moment gages as the coils are pressurized. This hypothesis was confirmed by the calibration data.

The first step in calibrating the JCR was to load only the axial gage to determine the measured versus applied load curves (fig. 10) for the axial gage with and without pressure in the coils. Figure 10 shows no effect of pressure but a +2 percent shift in the calibration slope. This discrepancy was accounted for in the thrust calculations.

Figure 11 shows the effect of coil pressure (166 psig maximum) on the N1 and N2 normal-force gages and the axial gage. The axial gage shows negligible effects from a coil pressure of 166 psig. However, the normal-force gages show a linear effect with pressure. Figure 12 shows the effect of combining coil pressure with normal loading on the normal and axial-force gages. Data plotted in figure 12(a, b) are for both the loading and the unloading of the N1 gage (applied normal load) in the normal-force gage direction. Figure 12(c) shows the effect on the axial gage from both coil pressure and normal loading. The axial gage is unaffected by coil pressure, but is slightly

affected by a normal load. Slopes and offsets from these plots were used to determine the corrections to the balance output in computing actual nozzle thrust.

#### Nozzle Calibrations/Surveys

Nozzle calibrations and surveys used in the investigations were conducted in the JCAHT facility on the JCR. There were six nozzle arrangements calibrated (refer to tables 2 and 3 for a summary of nozzle descriptions, geometries, and usage).

The JCR with nozzle-type 1 installed is shown in figure 5(b). Most of the nozzles were designed to be used in the Langley wind tunnel model, which uses the same delta-wing planform as the Ames model but contains an upper surface shell. Because the plenum and nozzles had to fit within this shell, the nozzles had to be fairly short. In an attempt to improve flow quality in these short nozzles, a perforated flow-distribution plate was installed a small distance upstream from the nozzle exit. These nozzles also used an adapter for installation on the HTR. For the nozzle calibrations and surveys, the same nozzle, adapter, and plenum assembly were mounted on the JCR as shown in figure 5(b).

Surveys of the jet-exit flow were made using a Pitot probe mounted on the jet-wake survey rig (fig. 5(a, b)). A continuous trace of the Pitot pressure reading was plotted as a function of traverse position on an analog x-y plotter. The general procedure for flow surveys consisted of taking surveys across the jet at the exit plane. These surveys were then used to assess the flow quality and determine if alterations to the perforated plates were required. If alterations were required, another flow survey was done to determine the flow quality and document the changes. A vertical traverse (z axis) was taken to document the decay of the jet core flow as a function of the distance from the nozzle exit. Additional pressure surveys were taken across the jet flow at various distances downstream from the nozzle exit.

To calibrate for nozzle thrust, the measured thrust (from the JCR balance corrected for rig interactions) was plotted against NPR. Nozzle total pressure was measured with a total-pressure probe at the nozzle exit. Then the NPR was plotted against nozzle reference pressure. These calibrations were needed to calculate thrust because only the nozzle reference pressures were measured when mounted on the HTR.

Thrust calibrations from the JCR appeared to be linear from NPRs of 1.5-6.23. The calibrations were expected to be linear for NPRs greater that 1.89 since the nozzle was choked and should respond linearly with a change in pressure. The small nonlinearity present from an NPR of 1.5

to 1.89 was within the data scatter of the calibration and was not accounted for.

Each of the nozzles tested had a single porous plate at the inlet of the nozzle with the exception of nozzle-type 3 (twin jets, 3.9 in. spacing) which had three sets of porous plates to help provide a good exit-pressure distribution.

Nozzle-types 1 and 2- These 1.2-in.-diameter circular nozzles were the baseline nozzles used in the investigations and one is shown attached to the JCR in figure 5(b). The nozzles were used separately in either the forward (nozzle-type 1) position or the aft (nozzle-type 2) position. Figure 13 shows a sketch of a 1.2-in.-diameter nozzle, including the nozzle adapter and the perforatedplate location. A pressure tap was installed about 0.1 in. upstream from the nozzle contraction to provide a reference pressure for thrust calibrations. The nozzles have a modified American Society of Mechanical Engineers (ASME) nozzle-exit contour as shown in figure 14. The thrust and NPR calibrations for the front and aft circular nozzles (types 1 and 2) are presented in figure 15 and show excellent agreement. These nozzles were also used in the model tested in the Langley wind tunnel.

A pressure survey at the nozzle exit for nozzle types 1 and 2) is shown in figure 16 for various NPRs. Because of the short distance available to develop the jet flow (from the plenum exit to the perforated plate in the nozzle), it was not possible to obtain a uniform or "top hat" total-pressure distribution at the nozzle exit. However, the jet decay curves (fig. 17) show a potential core up to about 5 or 6 jet diameters at subcritical pressure ratios, thus generally indicating a good-quality jet. At supercritical pressure ratios (NPR = 4 and 6) the shock cell structure is apparent in the decay curves. The large drop in total pressure immediately downstream from the exit and subsequent oscillations are due to the pressure losses in the plume-expansion region and across the normal shock that existed in front of the Pitot probe.

Nozzle-type 3— These 0.87 in. diameter nozzles were were available from a previous study and were used only on the hover part of this study. These nozzles were used as a pair and were attached to a plenum cover plate so that the center-to-center (side-by-side) spacing of the nozzle exits were 3.9 in. (fig. 18). These nozzles conform to the ASME long-radius nozzle definition (fig. 19). Because these nozzles had a relatively long flow-development section and the distance from the plenum to the exit was relatively long (14.4 individual jet diameters), the nozzles were used without flow distribution plates. In contrast to the shorter nozzles (types 1 and 2), the exit pressure profiles for these nozzles were very uniform. The pressure in the plenum, feeding the nozzle pair, was used as the reference pressure for thrust and NPR calculations.

The thrust and NPR calibrations are shown in figure 20. Thrust was calibrated for the pair since there was no way to measure the thrust of the left and right nozzles separately. Separate flow (pressure) surveys were made for each nozzle and show excellent agreement (fig. 21). This indicates good flow distribution between the two nozzles. The flow surveys made at various distances downstream from the jet exit (fig. 22(a, b)) show that the jets are far enough apart that their flows do not begin to merge until about 15 diameters from the exit. The apparent loss in total pressure in the middle of the jet at a height of 5 in. (z/d = 5.8) and a NPR = 6.2 (fig. 22(b)) is due to the total-pressure loss behind the normal shock that forms in front of the Pitot tube in the supersonic flow.

Nozzle-type 4- These nozzles, with an exit diameter of 0.85 in. (fig. 23), were attached as a pair to a plenum plate so that the center-to-center (side-by-side) spacing of the nozzle exits was 2.52 in. They also had a modified ASME nozzle contour (fig. 24). The plenum to which these nozzles were attached was relatively small with a wire mesh inside to help provide a more uniform flow into the nozzles. The reference pressure tap was located in the plenum. The thrust and NPR calibrations are shown in figure 25. Again, as with the 3.9-in.-spaced nozzles, the thrust calibration was done for the pair. Separate flow surveys were done for each of the nozzles at the exit plane (fig. 26) with the pressures measured on the centerlines showing excellent agreement. The flow surveys made at various distances downstream from the exit (fig. 27(a, b)) indicate that merging of the nozzle flow begins at 6-10 diameters downstream. As with the 3.9-in.-spacing jets, the apparent pressure loss in the center of the flow for the NPR = 6.2 case (fig. 27(b)) is due to the total-pressure loss behind the normal shock that forms in front of the Pitot probe.

The jet-decay curves (fig. 28) show a potential core of 5-6 nozzle diameters at subcritical pressure ratios, thus indicating good quality flow. At supercritical pressure ratios (NPR = 4 and 6), the shock cell structure is apparent in the jet-decay curves. The large drop in total pressure immediately downstream from the exit and the subsequent oscillations are due to the pressure loss across the normal shock located in front of the Pitot probe.

These nozzles were also used in the model at the Langley wind tunnel.

Nozzle-types 5 and 6— These rectangular nozzles are shown in figure 29. Each nozzle had the same exit dimensions of 0.613 in.  $\times$  1.840 in. with a contoured wall section along the long edge and a flat wall section along the short edge leading to the exit plane. The contoured nozzle section is shown in figure 30. A porous plate was located at the entrance of the nozzle. The thrust and NPR

calibration curves (fig. 31) show that the aft nozzle (type 5) had a slightly lower thrust than the forward nozzle (type 6). These thrust differences were taken into account when setting and computing the thrust and NPR of the front and aft nozzles during model testing. The porous plates at the nozzle entrance were modified to increase the flow at the narrow ends. The exit pressure distributions (figs. 32 and 33) show lower flow at the narrow ends of the rectangular nozzles. These were the best profiles attainable without redesign. Although the flow distribution at the nozzle exit plane may not have been ideal, the surveys at various distances downstream from the exit (fig. 34(a-d)) and the decay curves (fig. 35) indicated relatively good quality flow.

The type 5 and 6 nozzles were also used in the model at the Langley wind tunnel.

#### **Comparison of Jet Decay Rates**

A jet issuing into still air mixes with the surrounding air and decays as shown by the data in figures 17, 28, and 35. Kucheman and Weber (ref. 5) have shown that close to the exit the mixing does not penetrate to the centerline, thus leaving a full velocity core (potential core) for a distance of about six nozzle-exit diameters for subsonic jets. Beyond this point, the mixing causes the velocity on the center axis to decrease in direct proportion to the distance. The dynamic pressure sensed by the Pitot probe will therefore be inversely proportional to the square of the distance from the exit plane.

The decay curves for the jets from the four nozzle sets of the present investigation have been replotted using a log-log scale and are shown in figure 36(a)(c-e). Similar data for a 1.23 in. diameter nozzle from a previous test are also included (fig. 36(b)). As expected, beyond the end of the potential core the ratio of the total pressure measured by the Pitot probe to that of the nozzle is inversely proportional to the square of the distance from the exit.

This decay relationship should be true at all NPRs. However at NPRs above 1.89, where supersonic flow is generated, the total pressure loss behind the normal shock that forms in front of the Pitot probe indicates lower pressures than are actually present. At these conditions, the inverse square relationship can only be seen at greater distances from the nozzle exit where the flow has become subsonic. At these higher NPRs, the decay curves are shifted to the right indicating that the "effective" potential-core length increases with NPR.

The decay curves for a J-85 jet engine with several nozzle configurations were measured in reference 6 and have been replotted in figure 37(a-c). Again, as with small cold-air jets (fig. 36(a-e)) the jet dynamic pressure decays

with the square of the distance from the nozzle exit, and the potential-core length increases with nozzle pressure ratio. The exception to the inverse square relationship occurs with the four-nozzle configuration. Beyond a distance of seven effective diameters (14 individual jet diameters) the decay rate decreases (probably because the closely spaced jets are beginning to merge into a single jet).

The effective-core lengths for the various nozzles are compared in figure 38(a, b). The effective-core lengths for the J-85 engine powered nozzles (at a given NPR) are less than for the small cold-air driven jets probably because of the greater distortion of the exit dynamic-pressure distribution (top of fig. 38(a)). The short-nozzle J-85 configuration exhibits a large drop in pressure at the center because of the wake of the turbine disk fairing in the flow. If the decay curves were nondimensionalized by an areaweighted average of the exit dynamic-pressure distribution, the core lengths would probably be much closer.

The effective-core lengths of all of the circular nozzles increase with the 1/4 power of the NPR. However, the effective-core length of the rectangular nozzle increases with the 1/6 power. These power laws appear to fit at both subcritical and supercritical NPRs.

#### **Model Test Results**

All the model test data are presented in the appendix. Since all test runs were done with cold, dry high-pressure air flowing through the nozzles, temperatures at the nozzle exits were often below freezing (32 °F). When running for a prolonged period of time, ice formed on the outside of the nozzles. In some cases this ice actually closed the gap between the nozzles and the model. Balance data for run points where this occurred are not presented. The nozzles and model were frequently de-iced and the gap clearances were carefully watched. However, there could be a few run points where the balance data was biased due to ice bridging the gap. Any large discrepancies found between the integration of the pressure data and the balance data (presented at the end of each data listing in the appendix), especially the pitching-moment data, might be due to unnoticed icing problems.

It should also be noted that the resolution of the pitching moment is about five times coarser than the lift measurements. Pitching moment is determined by the two 500 lb normal-force gages, as opposed to the 100 lb axial (lift) gage. Unfortunately, many of the test conditions produced small pitching moments that could not be measured as accurately as the lift forces.

Model test results on the effects of three parameters are briefly discussed here. These parameters are: jet spacing (8, 12, 16, 2.5, and 3.9 in.), planform size, and NPR. Both balance and pressure data are used in discussing these parameters. Most of the pressure data are presented using contour plots that show lines of constant pressure coefficient on the model undersurface. The pressure coefficient used is defined as  $\Delta p/q_{jet}$ , where  $q_{jet}$  is the calculated incompressible-jet dynamic pressure given by  $q_{jet} = T/(2 * A_{jet})$ .

In each of the contour plots, the solid contour lines indicate positive pressures and the dotted lines represent negative pressures. Nominally, the difference between contour lines was 1, or  $c_p = 0.001$ , since the data were multiplied by 1000 before plotting. In some cases, the difference between contour lines was increased to make the plot more readable. The  $c_p$  contours were generated over the entire model undersurface by reflecting the pressure information about the longitudinal axis of the planform. For configurations in which the pressure taps crossed the model symmetry, pressure information was used directly (the pressure-tap counterparts from the other side of the planform were not reflected).

As a result of a limitation in the plotting process, some of the contour plots show contour lines extending slightly outside the model planform. In order to generate the contour plots, the pressure data had to be in a rectangular, or "regular," grid format. Because the pressure taps were not laid out in a regular pattern, a representative regular pattern had to be generated. The values of the regular grid points were determined by a weighted interpolation scheme stated by

$$Z_{jk} = \frac{\sum_{i=1}^{n} \frac{1}{D_{i}^{w}} Z_{i}}{\sum_{i=1}^{n} \frac{1}{D_{i}^{w}}}$$

where

 $Z_{jk}$  is the value to be computed for node jk of the grid

Z<sub>i</sub> is value of an irregular point

 $D_i$  is the distance from the node jk to the irregular point  $Z_i$ 

w is the weighting factor (2.0 for this analysis)

n is the number of irregular points that fall in the "search area" for the irregular points  $Z_i$ . In this analysis, the search area is two cells to the left,

two cells to the right, two cells above, and two cells below.

Since values for the regular grid points were determined based on data from the immediate area, some grid points just outside the planform were assigned values. Because the original data points did not normally lie on the regular grid points, the original data values were not usually preserved. This was especially true for large narrow peaks in some of the data. The actual maximum and minimum  $c_p$  values are therefore supplied with most of the contour plots. These values came directly from the data listed in the appendix.

#### **Jet Spacing**

The effect of the relatively large forward to aft jet spacing was looked at only for the two-jet delta-wing configuration. These effects are shown in figure 39(a-c). Pressure data from the model's undersurface is plotted for the 8, 12, and 16 in. jet spacing at NPR = 2 and  $h/D_e = 2.36$ (h = 4 in.). These figures show that the fountain flow is intense, but relatively small at the close jet spacing. spread out, but smaller in magnitude at the intermediate 12 in. spacing, and actually quite large, both in area and magnitude, with the wider 16 in. spacing. Figure 40 shows the corresponding balance and integrated pressure data. This data shows an increase in suckdown for the 12 in. jet spacing, which can probably be attributed to the reduced fountain strength (fig. 39(b)). The cause for the large differences between the balance and pressure data at a jet spacing of 16 in. in figure 40(a) and at a jet spacing of 8 in. in figure 40(b) is unknown. The unsteady nature of the flow field and the slowness of the mechanical scanivalves may possibly be a cause for this difference as the pressure ports are scanned in sequence, taking about 1.5 min, as opposed to an instantaneous acquisition.

Also note in figure 39(a-c) the large negative pressures in between the jets and the fountain. These are generated by a vortex structure located in this same area and extends to the ground. As the jet spacing is reduced, the negative pressures tend to become more negative. This indicates an increase in the strength of the vortex structures. This trend tends to hold true until the jet spacing is reduced to a point where the vortex structure between the fountain and the jets seems to disappear.

The model surface pressures of the closer 2.5 and 3.9 in. jet spacing are shown in figure 41(a, b). Data from the configuration with a pair of 2.5 in. spaced jets at various heights at a NPR of 2.0 are shown in figure 41(a). Figure 41(b) shows data from a configuration with a pair of 3.9 in. spaced jets at the same test conditions. Although the maximum and minimum pressures are generally larger

at the lower heights for the configuration with 2.5 in. jet spacing, the fountain loses its effectiveness quicker than with the 3.9 in. spaced jets. Balance and pressure data (fig. 42) shows that the 2.5 in. jet spacing configuration has more suckdown than the 3.9 in. jet spacing configuration.

During testing, plots of the actual pressure data between the 2.5 in. spaced jets (fig. 43) showed that the flow was not always symmetrical as was the case for the 3.9 in. (fig. 41(b)) and wider spaced two-jet configurations. The same pressure distribution also shows that the usual vortex (wide negative-pressure regions) between the jets and the fountain does not exist with the 2.5 in. jet spacing configuration. Instead, there is almost exclusively a positive-pressure region spanning between the jets. From the contour plots of figure 41(a), it appears that the maximum pressures are skewed at an angle between the jets. It was thought that this skewing may have been caused by differences in nozzle thrust. Previously, the JCR showed excellent agreement between the nozzles (figs. 25-27). A total-pressure probe was mounted at the center of the jet exit for each nozzle, to make sure that the nozzle pressures (and thrusts) were symmetric. As can be seen in figure 44, the pressures of each nozzle are in almost perfect agreement. This may indicate that, in this case, the model flow structure was very sensitive to small changes in jet flow structure or model-ground geometry.

#### Planform Size

The planform shape can also greatly affect the overall lift loss and pitching moments acting on an aircraft, especially close to the ground. Figure 45(a-h) compares the effects of planform shape between a small rectangular planform enclosing the nozzles and the delta-wing configuration. The fore/aft jet spacing is 8 in. Comparing the cp contours between the planforms shows that the positive pressures in the fountain region are quite similar, except at the top height. However, the negative pressures on similar regions of the planforms are not similar and will equalize with a cp approaching zero at the planform edges. The area in which negative pressures can act on figure 45(b) is much smaller than the area in which negative pressures can act on figure 45(a), where there is a more gradual equalization of cp over the larger space from the jets to the planform edge. This larger area where the negative pressures can act tends to increase the overall configuration suckdown and results in a nose-up pitching moment at the lower heights (fig. 46). Also, the fountain pressures on the belly of the model tend to move forward at the edge of the planform (fig. 45(a-f)(h)). It is interesting to note that at the top height,  $h/D_e = 5.89$ , the fountain under the smaller rectangular planform (fig. 45(h)) is still

evident, while no fountain is evident under the delta-wing planform (fig. 45(g)).

Similar data are shown for the three-jet configuration in figure 47(a-i), but at a 12 in. fore/aft jet spacing. Figure 48 shows the corresponding balance and integrated pressure data. Data for this configuration were obtained at  $h/D_e$  as low as 1.18 (h = 2 in.). At these low heights, the larger delta-wing planform had greatly reduced fountain pressures and increased negative pressures (also indicated by the plots of fig. 48 showing increased suckdown and pitching moments for the delta wing) compared to the rectangular planform (fig. 47(a, b)). Even though only the jet spacing was changed between this and the previous configuration (fig. 45), the cp distribution is quite different. However, the resultant jet-induced loads are very similar as shown in figure 49, which shows the difference in balance data between the 8 and 12 in. jet spacing configurations. With the wider (12 in.) fore/aft jet spacing, the fountain on the model undersurface is skewed toward the front jets at the low heights and moves aft as height is increased. More specifically, the fountain center region moves aft as model height is increased, but the outer region of the fountain appears to stay in the same place. This may indicate that the fountain flow is not perpendicular to the ground plane, but at some angle that may or may not vary with height. This could be the case if the ground flow from the aft jet penetrates farther along the ground. Then, if the fountain flow between the two front jets penetrates farther aft (as distance from the ground is increased) it could "push" the center of the main fountain flow of the three-jet pattern aft, thus creating the "horseshoe" pattern at intermediate fountain heights as shown in figure 47(e-h)(j).

#### **Nozzle Pressure Ratio**

Another parameter of the jet-induced characteristics is NPR. Figure 50(a-c) and 51(a-c) show the effect of NPR for two- and three-jet delta-wing configurations with the same 12 in. fore/aft jet spacing at  $h/D_e = 3.54$  (h = 6 in.). It appears that the planform's undersurface pressure-contour structures and magnitudes changed little with NPR. The same conclusion can be drawn from the nondimensionalized balance data shown in figure 52(a) for the jet-induced lift increment. However, the pitching moment seems to have a larger variation (and data scatter), especially at NPR = 6.

# **Concluding Remarks**

This report presented hover data obtained at the Ames JCAHT facility for a parametric flat-plate model. The model tested was a flat-plate design that allowed variations in planform aspect ratio, number of jets, nozzle shape, and jet location. There were 31 different planform-nozzle configurations tested. Each configuration had numerous pressure taps installed to measure the pressures on the model undersurface. All pressure data, along with the balance jet-induced lift and pitching moment increments, are tabulated. For selected runs, pressure data was presented in the form of contour plots that show lines of constant pressure coefficient on the model undersurface. Nozzle thrust calibrations and jet-flow-pressure survey information were also provided.

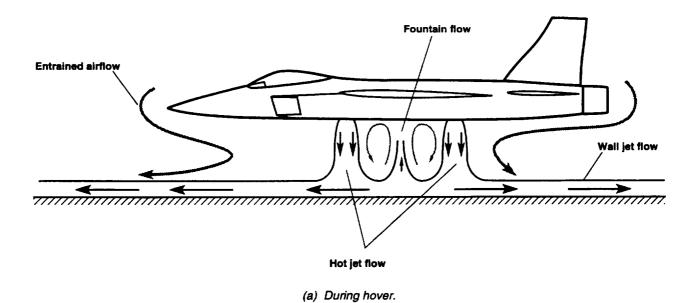
As expected, jet spacing and layout had a significant effect on jet-induced lift loss and pitching moments. Unexpectedly, the 12 in. fore/aft spaced two-jet configuration had more suckdown than either the 8 in. or 16 in. spaced two-jet configuration. In addition, the very closely spaced (2.5 in.) two-jet configuration did not have the usual vortex (wide negative pressure regions) in between the jets and the fountain. At low heights, the 2.5 in. spaced jet configuration had a very skewed, nonsymmetrical high-pressure or fountain region between the jets. This may indicate that, in this case, the model flow structure was very sensitive to small changes in jet flow structure or model—ground geometry.

Comparing the  $c_p$  contours among the planforms for the 8 in., 12 in., and 16 in. fore/aft jet spacing shows that the positive pressures in the fountain region are quite similar, except at the top heights. However, the negative pressures on similar regions of the planforms are not similar and will equalize with a  $c_p$  approaching zero at the planform edges. For some of the three-jet configurations, a "horse-shoe" shaped fountain (high pressure region) was observed on the model undersurface.

It appears that the planform's undersurface pressurecontour structure and magnitudes changed little with NPR. Data presented in this report adds significantly to the current STOVL-configurations data base. Further development of empirical prediction methods for jet-induced forces to provide for more configuration diversity and improved overall accuracy, as well as the validation of CFD codes, depend on this data base.

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- McLemore, H. C.: Jet-Induced Lift Loss of Jet VTOL Configurations in Hovering Conditions. NASA TN-D-3435, 1966.



Fountain flow

Ground vortex

Wall jet flow

Hot jet flows

(b) At forward speed or with a headwind.

Figure 1. Flow structure around a short takeoff and vertical landing (STOVL) aircraft in ground effect.

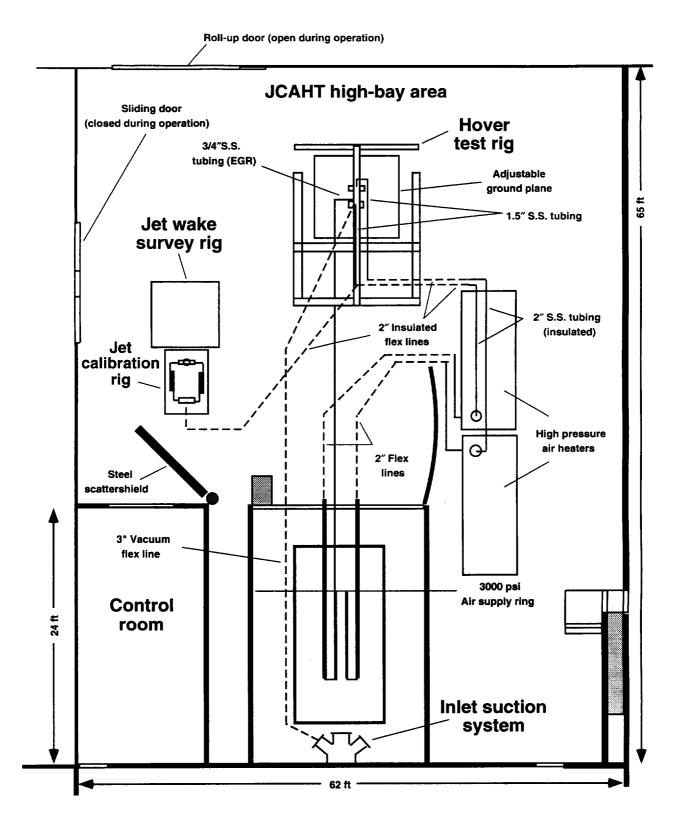


Figure 2. Layout of the Jet Calibration and Hover Test (JCAHT) facility.



Figure 3. The hover test rig (HTR) support with a delta-wing configuration attached.



Figure 4. Delta-wing configuration with the 8 ft  $\times$  8 ft ground plane in close proximity.

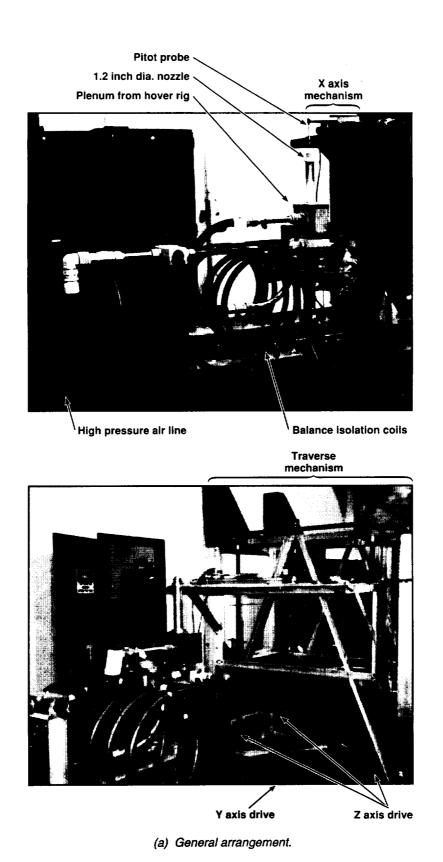
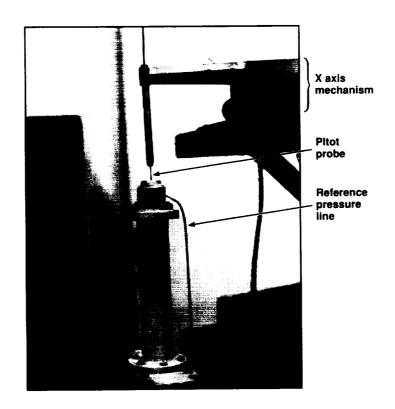
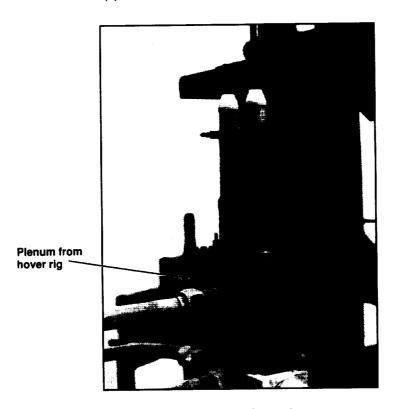


Figure 5. Jet calibration rig (JCR) set used for thrust calibrations and jet flow surveys.

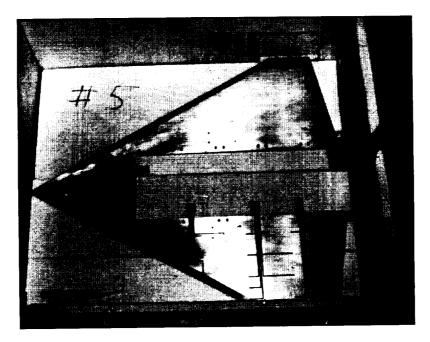


(b) 1.2-in-diameter circular nozzle.

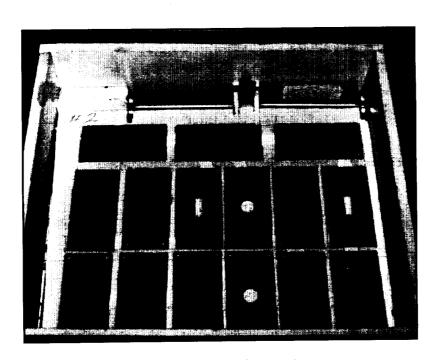


(c) 3.8-in-spaced side-by-side nozzles.

Figure 5. Concluded.

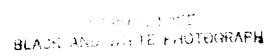


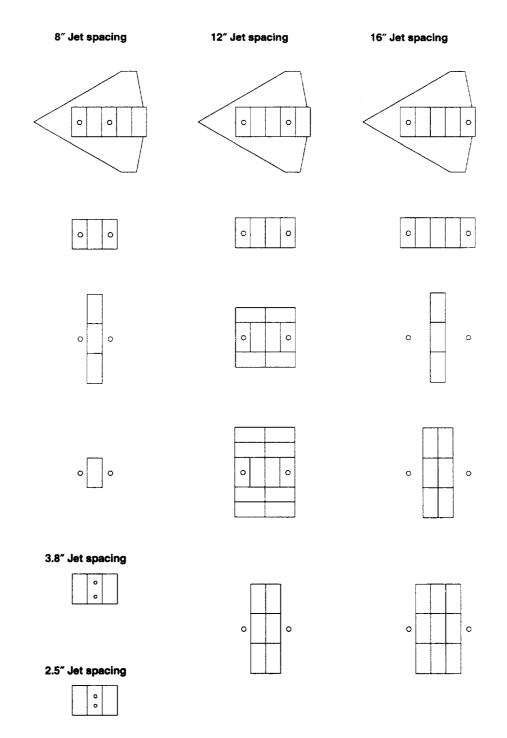
(a) Delta-wing planform section.



(b) Rectangular planform sections.

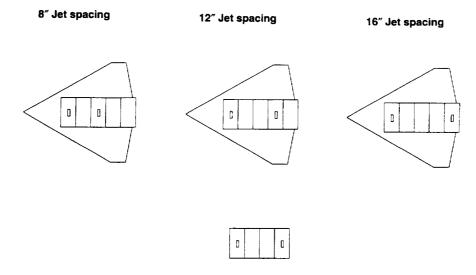
Figure 6. Planform sections for model configurations.



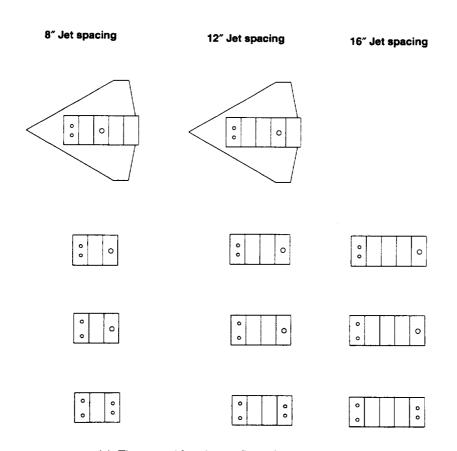


(a) Two-jet configurations, circular jets.

Figure 7. Summary of configurations tested.



(b) Two-jet configurations, rectangular jets.



(c) Three- and four-jet configurations, circular jets.

Figure 7. Concluded.

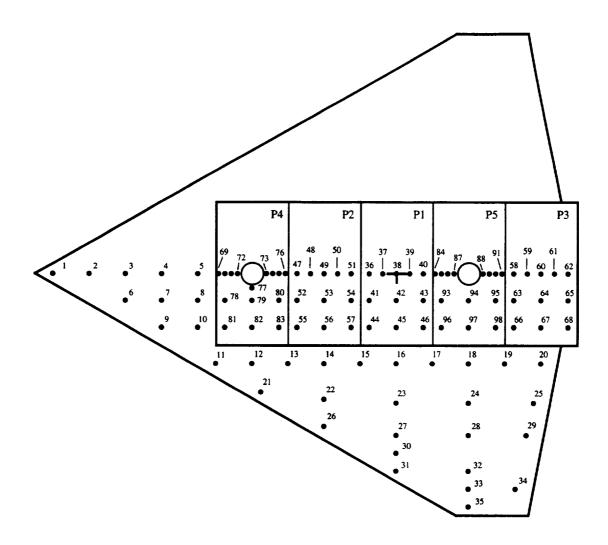


Figure 8. Pressure-tap layout for the two-jet delta wing configuration (2C\_12\_0\_DW).

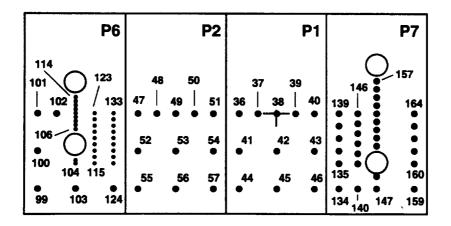


Figure 9. Pressure-tap layout showing pressure taps between side-by-side jets (4C\_12\_2.5/3.9\_16/8).

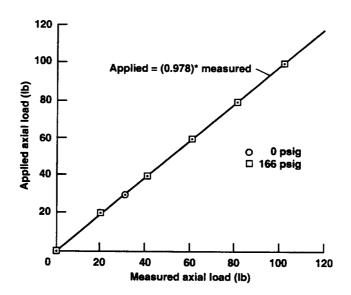


Figure 10. Applied versus measured axial loading for 0 and 166 psig jet calibration rig (JCR) coil pressure.

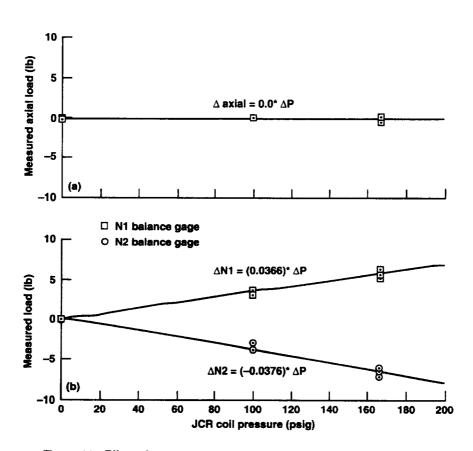


Figure 11. Effect of pressure on the balance N1, N2, and axial force gages.

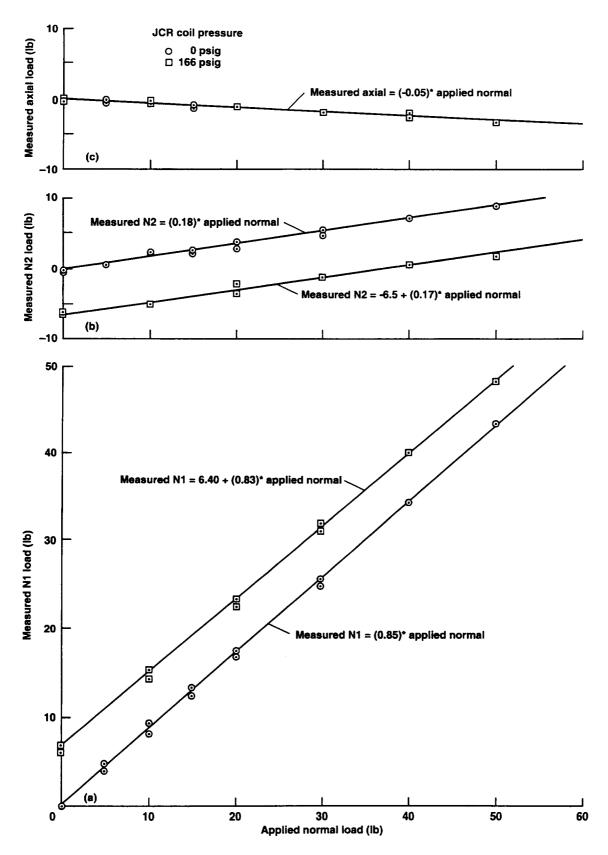


Figure 12. Effects of coil pressure and normal-force loading on balance gages.

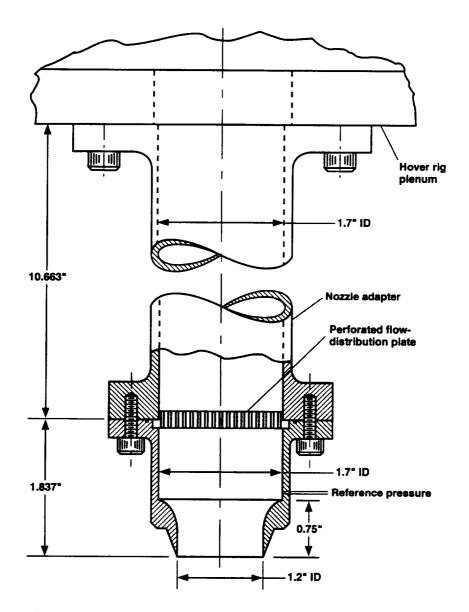
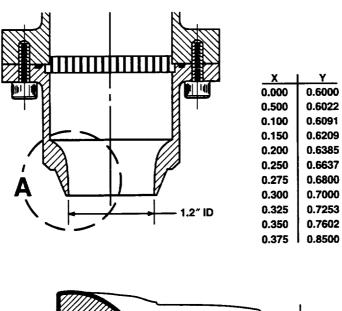


Figure 13. 1.2-in.-diameter nozzle and nozzle adapter, nozzle-types 1 and 2.



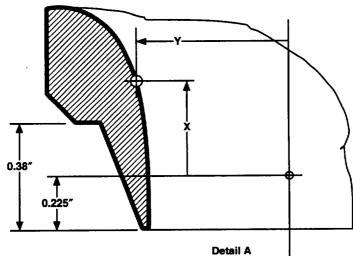


Figure 14. Nozzle contour for nozzle-types 1 and 2.

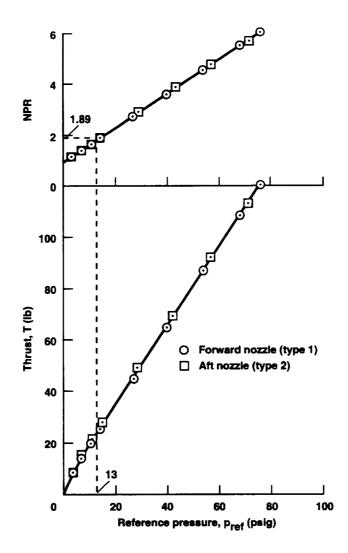


Figure 15. Thrust and nozzle pressure ratio (NPR) calibration of the 1.2-in.-diameter (type 1 and 2) nozzles.

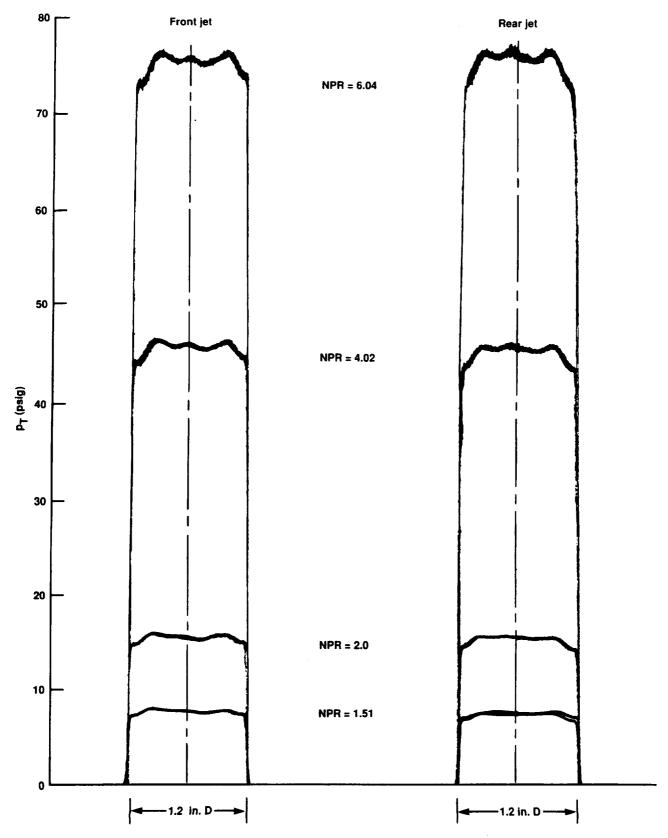


Figure 16. Exit total pressure profiles for the 1.2-in.-diameter (type 1 and 2) nozzles.

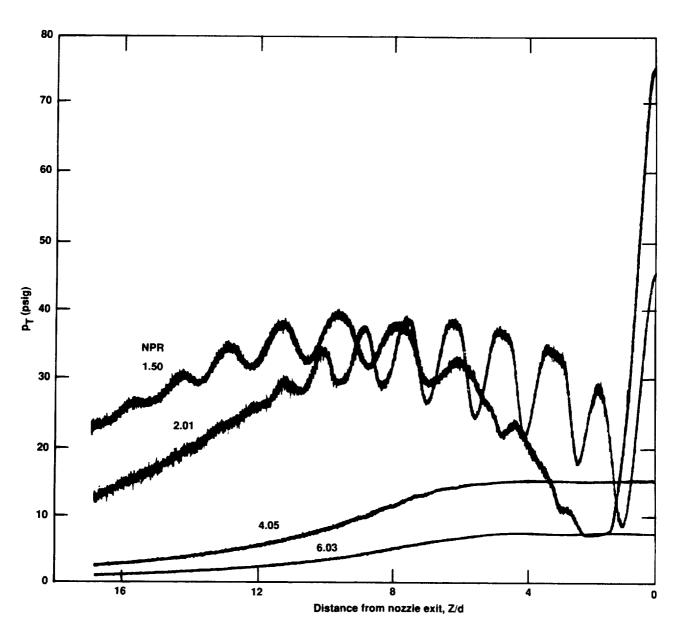


Figure 17. Decay curves for the 1.2-in.-diameter (type 1 and 2) nozzles.

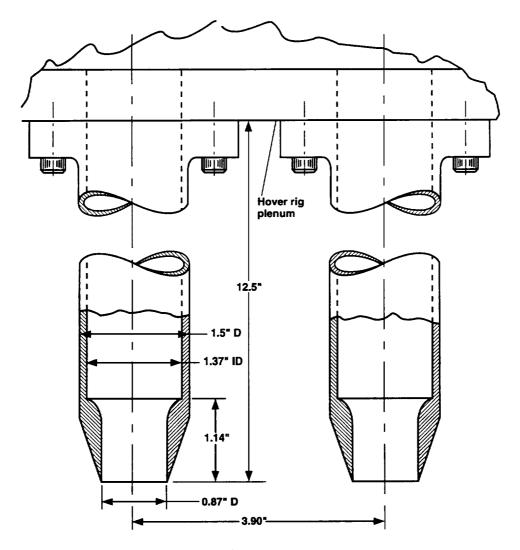


Figure 18. Nozzle-type 3, 0.87-in.-diameter, side-by-side nozzles (3.9 in. spacing).

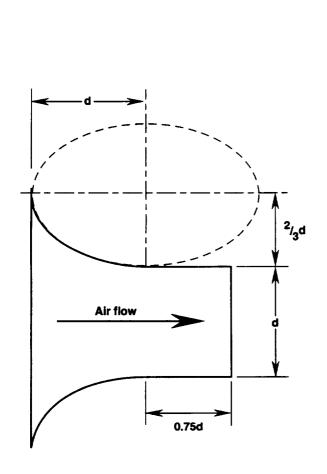


Figure 19. American Society of Mechanical Engineers (ASME) long-radius nozzle definition.

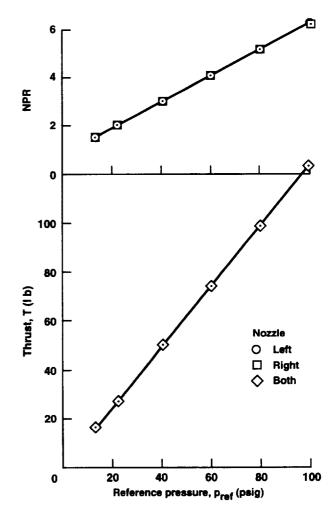


Figure 20. Thrust and nozzle pressure ratio (NPR) calibration of the 3.9-in.-spaced side-by-side (type 3) nozzles.

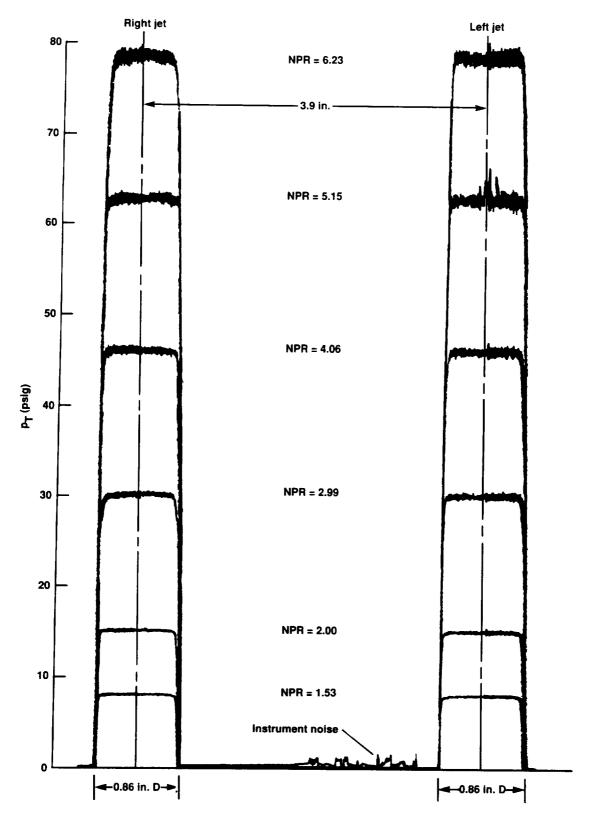


Figure 21. Exit total-pressure profiles for the 3.9-in.-spaced side-by-side (type 3) nozzles.

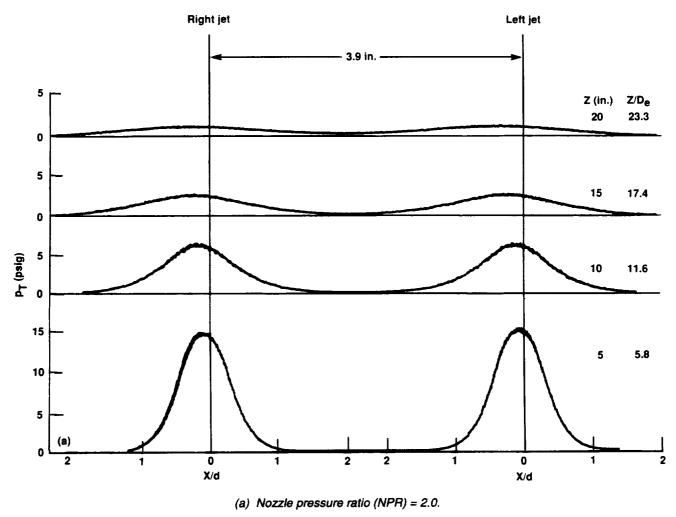
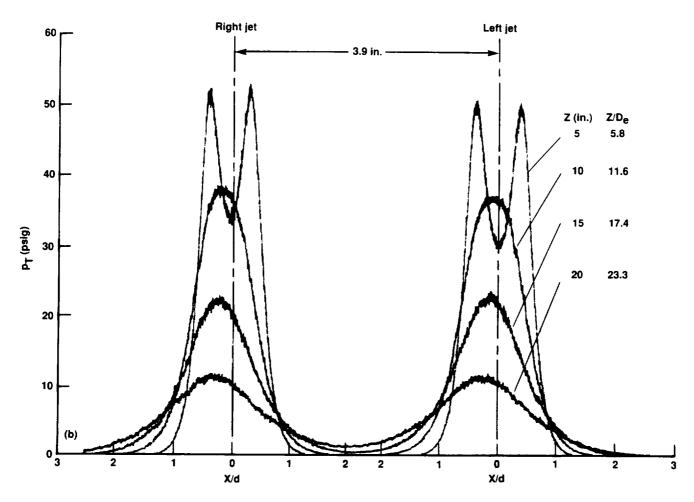


Figure 22. Total-pressure profiles at various distances downstream from the exits for the 3.9-in.-spaced side-by-side (type 3) nozzles.



(b) Nozzle pressure ratio (NPR) = 6.2. Figure 22. Concluded.

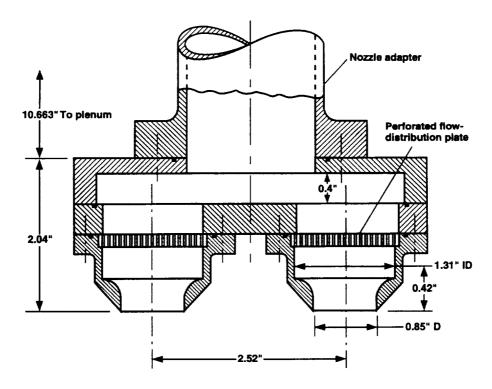


Figure 23. Nozzle-type 4, 0.85-in.-diameter side-by-side nozzles (2.52 in. spacing).

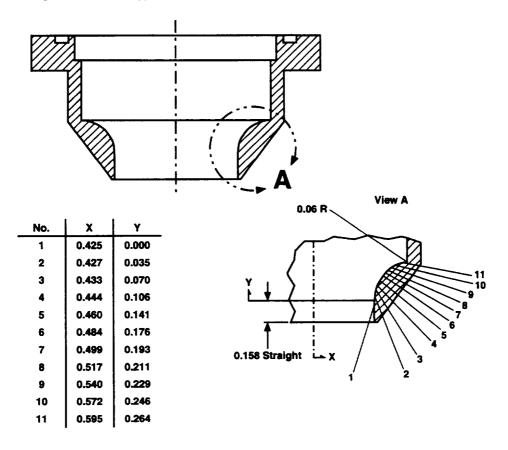


Figure 24. Exit contour details for nozzle-type 4.

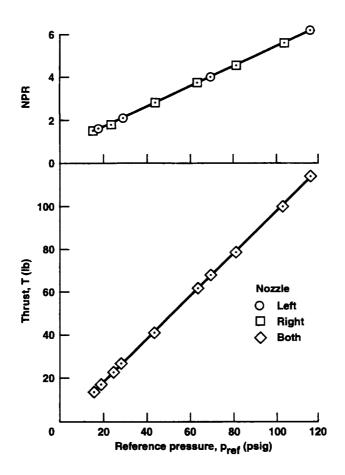


Figure 25. Thrust and nozzle pressure ratio (NPR) calibration of the 2.52-in.-spaced side-by-side (type 4) nozzles.

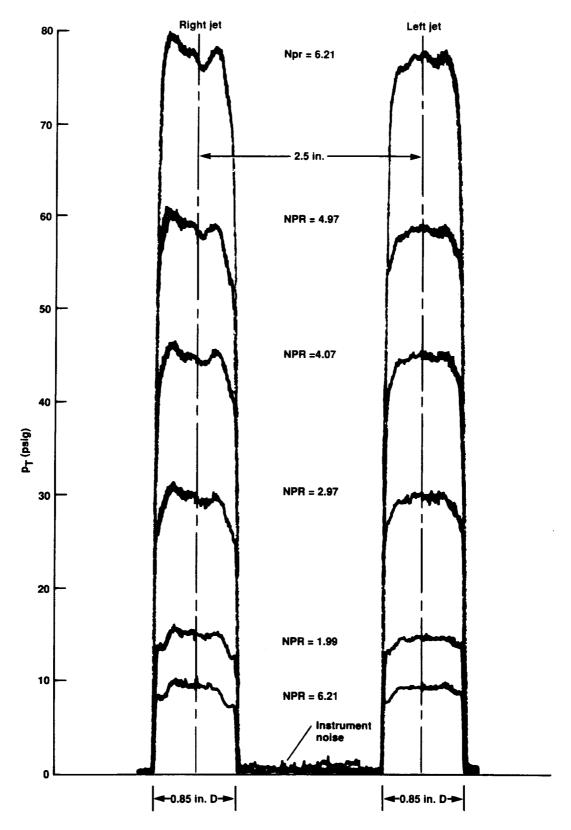


Figure 26. Exit total-pressure profiles for the 2.52-in.-spaced side-by-side (type 4) nozzles.

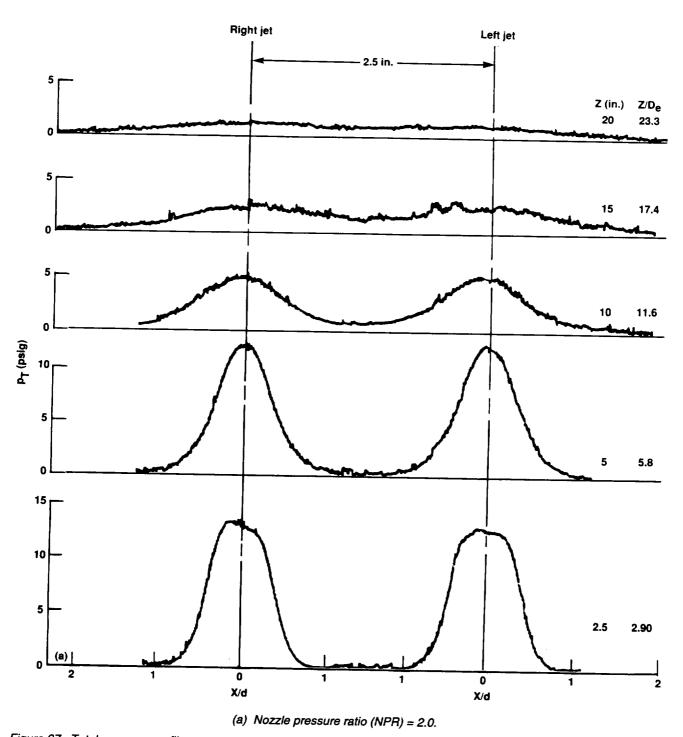
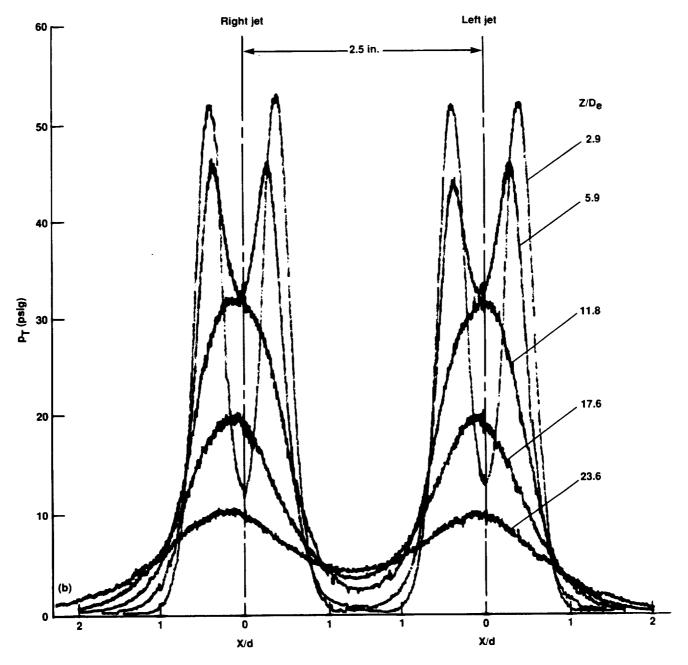


Figure 27. Total-pressure profiles at various distances downstream from the exits of the 2.52-in.-spaced side-by-side (type 4) nozzles.



(b) Nozzle pressure ratio (NPR) = 6.2. Figure 27. Concluded.

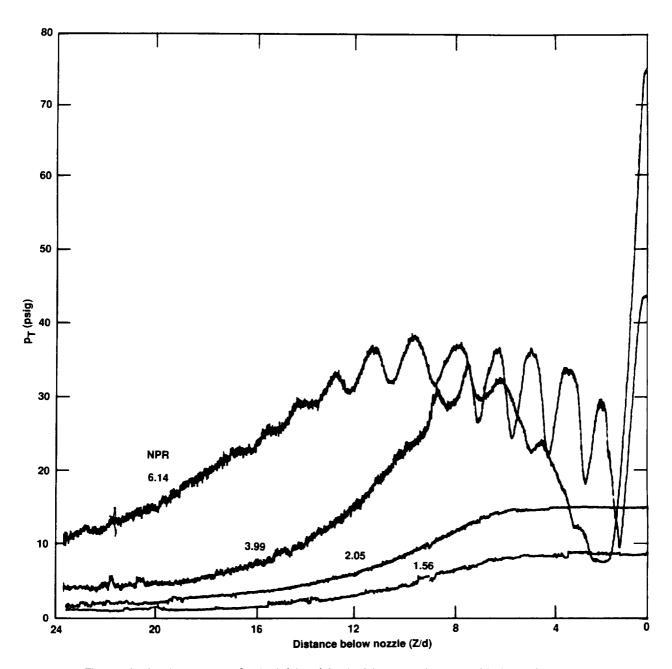


Figure 28. Jet-decay curves for the left jet of the 2.52-in.-spaced side-by-side (type 4) nozzles.

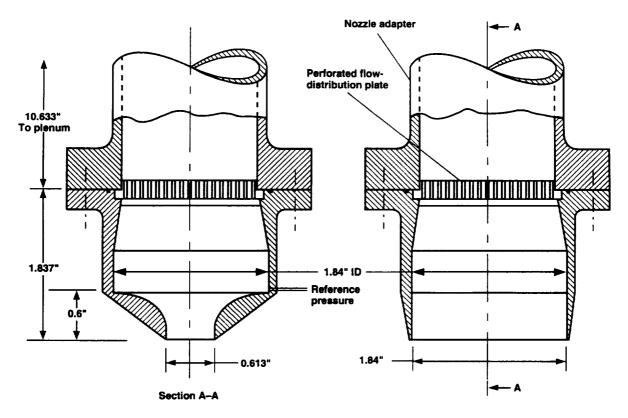


Figure 29. Sketch of the rectangular nozzles (types 5 and 6).

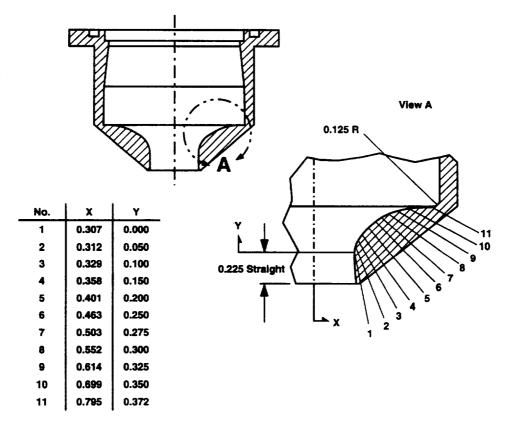


Figure 30. Exit contour detail of the rectangular nozzles (types 5 and 6).

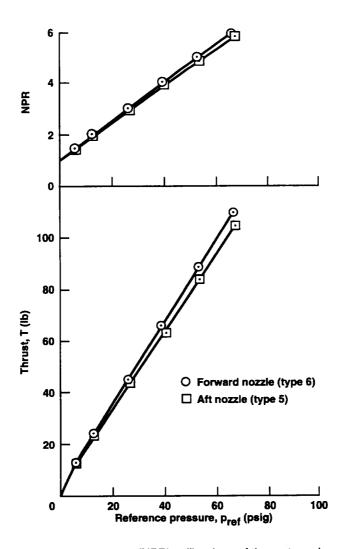


Figure 31. Thrust and nozzle pressure ratio (NPR) calibrations of the rectangular nozzles (types 5 and 6).

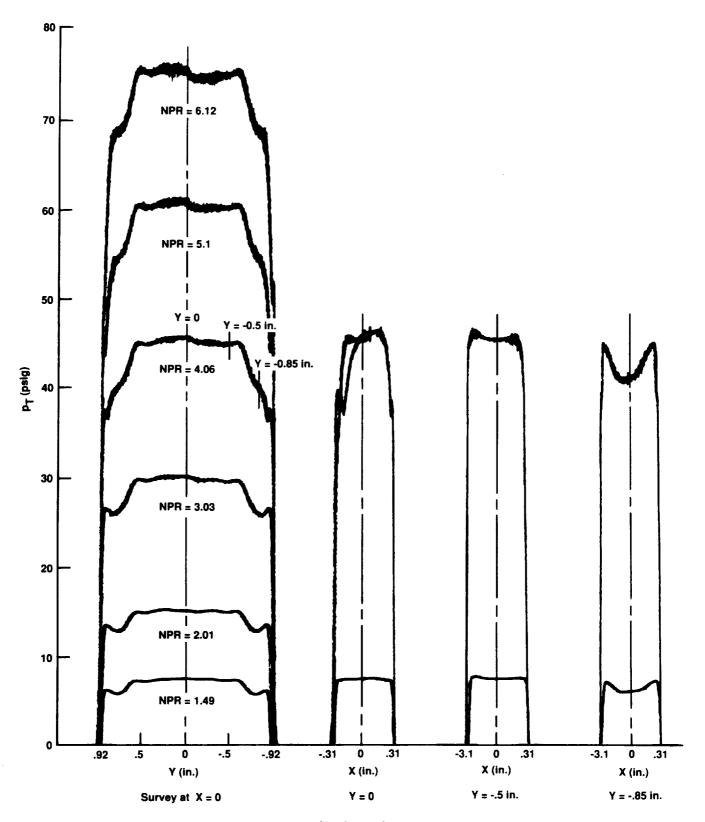


Figure 32. Exit total-pressure profiles for the forward rectangular nozzle (type 6).

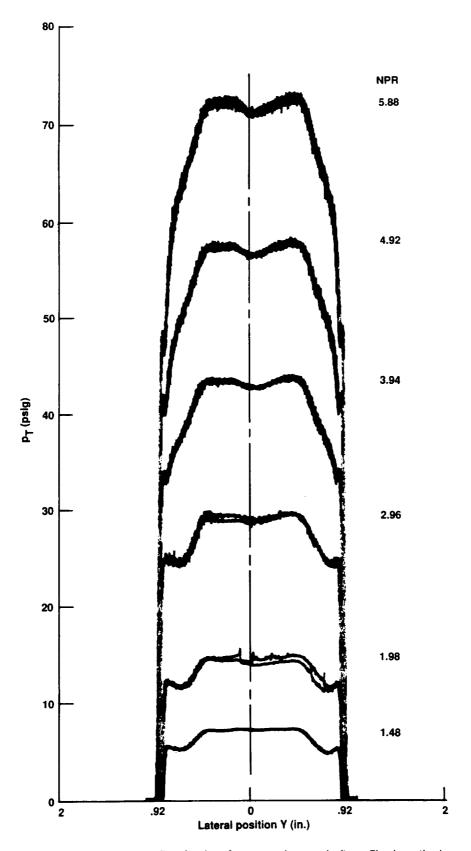


Figure 33. Exit total-pressure profiles for the aft rectangular nozzle (type 5); along the long axis.

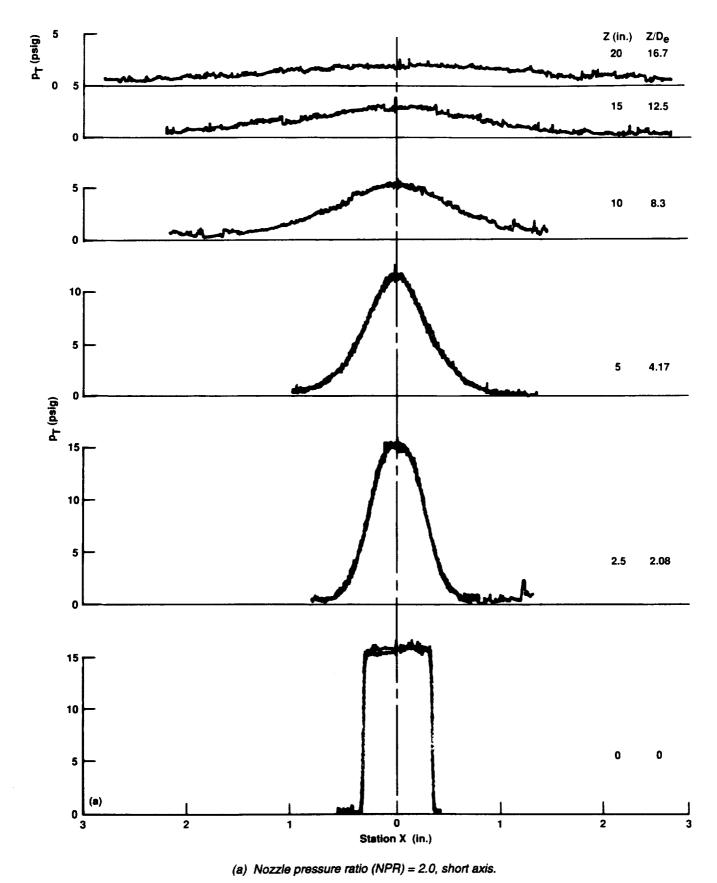
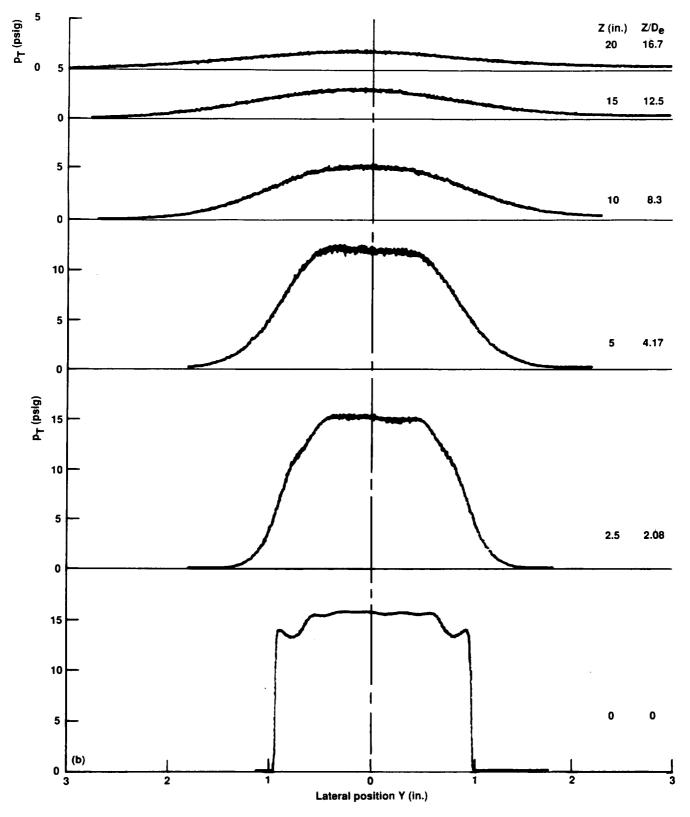
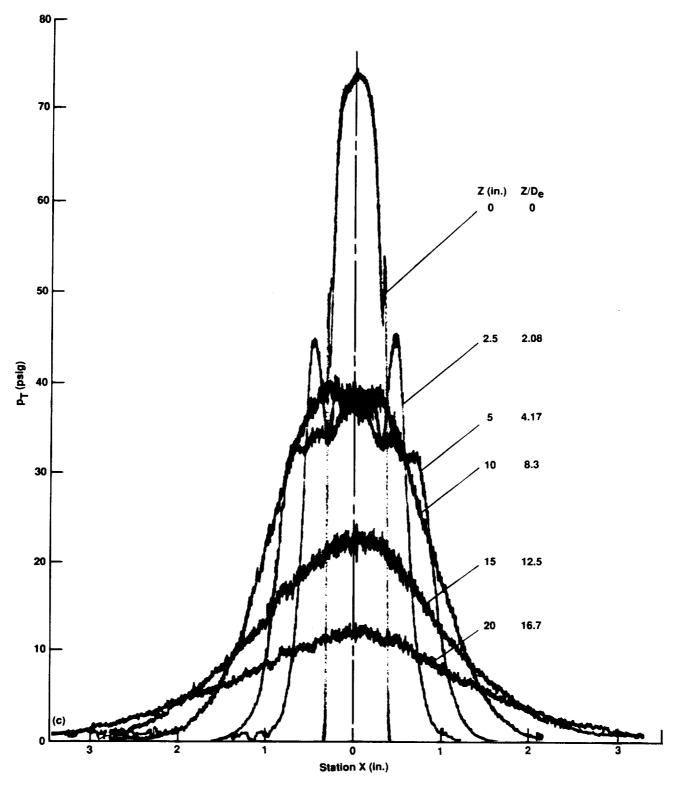


Figure 34. Total-pressure surveys at various distances downstream from the exit of the rectangular nozzles.



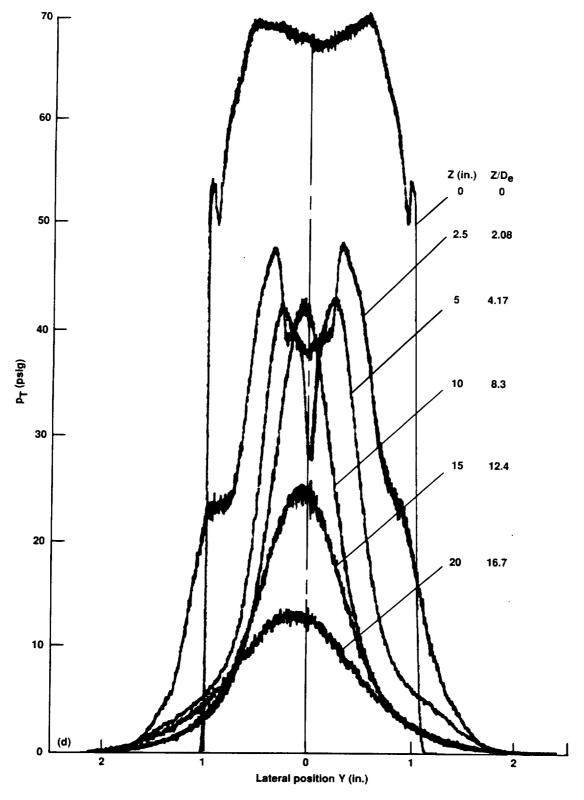
(b) Nozzle pressure ratio (NPR) = 2.0, long axis.

Figure 34. Continued.



(c) Nozzle pressure ratio (NPR) = 6.0, short axis.

Figure 34. Continued.



(d) Nozzle pressure ratio (NPR) = 5.8, long axis.

Figure 34. Concluded.

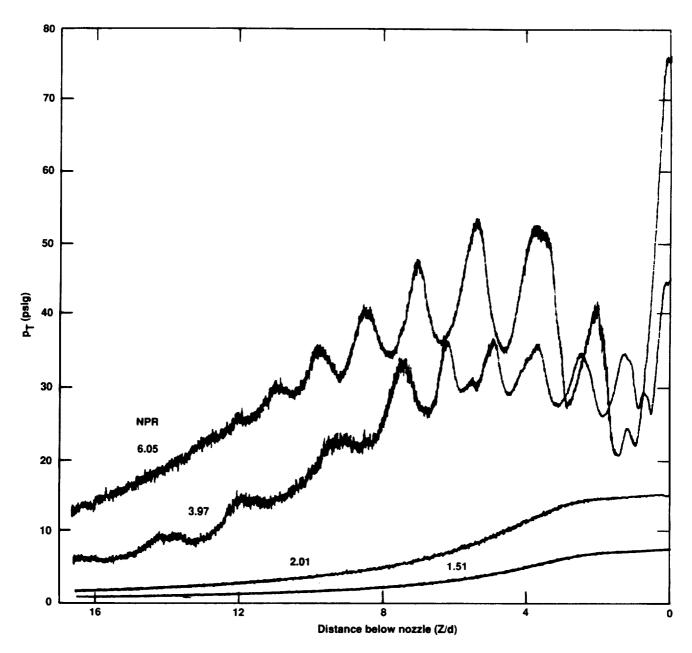


Figure 35. Jet-decay curves for the forward rectangular jet (type 6).

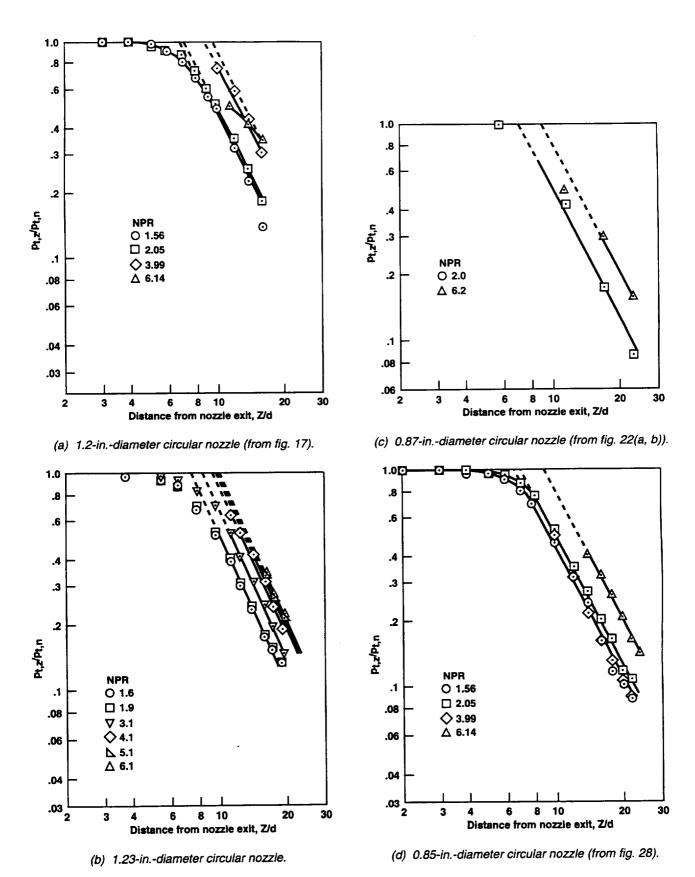
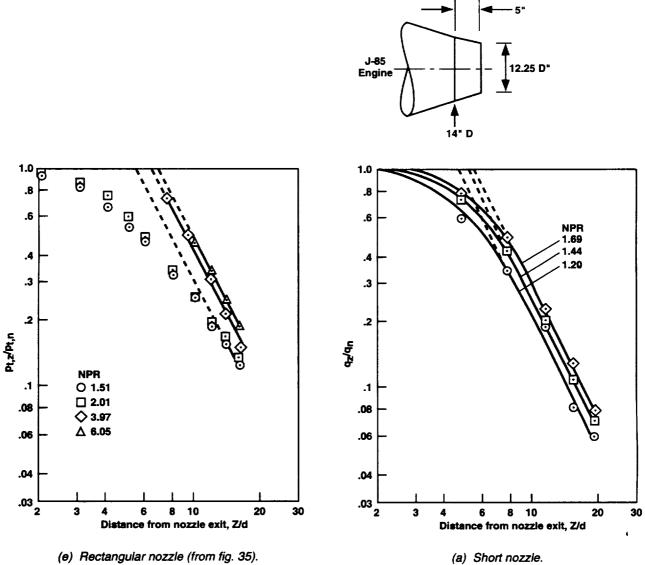


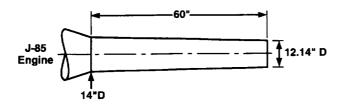
Figure 36. Log-log plots of jet decay curves.

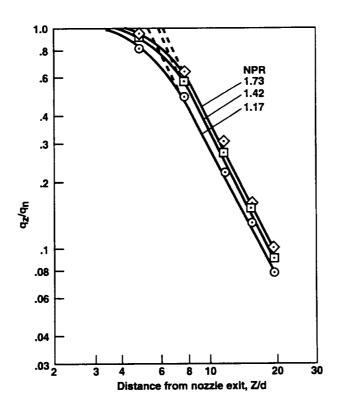


(e) Rectangular nozzle (from fig. 35).

Figure 36. Concluded.

Figure 37. Decay curves for a J-85 engine (ref. 6).

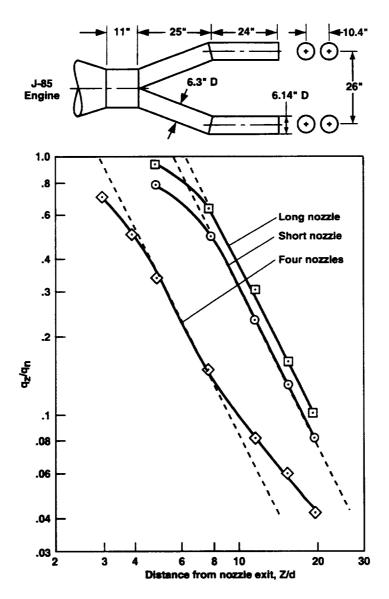




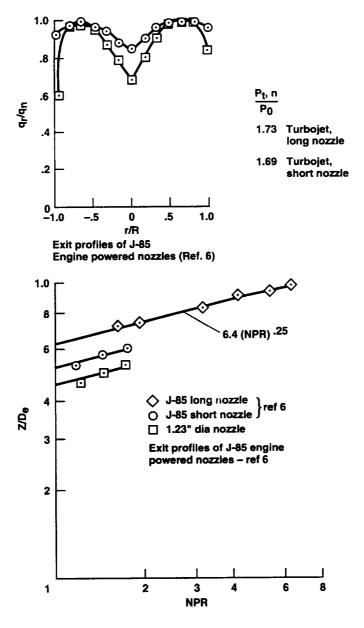
(b) Long nozzle.

Figure 37. Continued.

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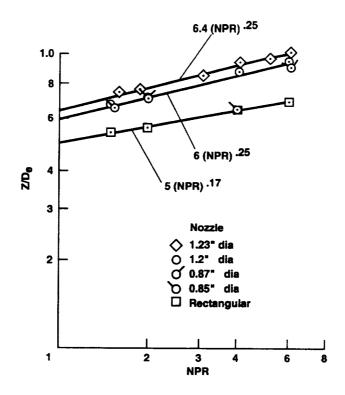


(c) Four-nozzle configuration. Figure 37. Concluded.

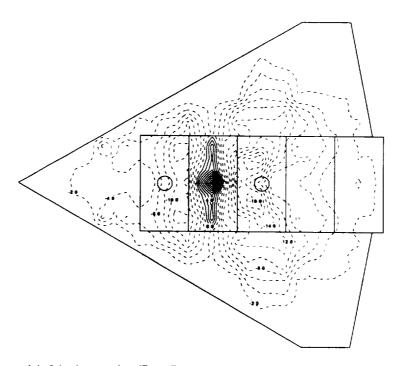


(a) Comparison of a jet engine and a small cold-air jet.

Figure 38. Effect of nozzle configuration and nozzle pressure ratio (NPR) on "effective" core length.

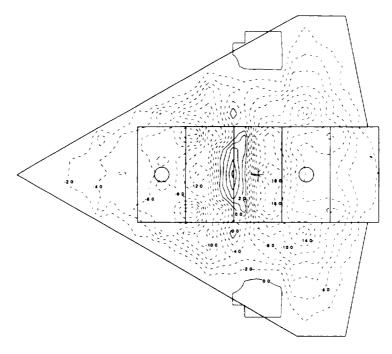


(b) Circular and rectangular cold-air jets. Figure 38. Concluded.

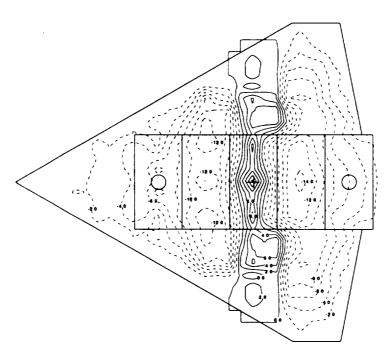


(a) 8-in.-jet spacing (R187P7),  $c_{pmax} = 0.0188$ ,  $c_{pmin} = -0.0260$ .

Figure 39. Contours of  $c_p$ \*1000 induced on the model undersurface for a two-jet delta-wing configuration showing the effect of jet spacing. Nozzle pressure ratio (NPR) = 2,  $h/D_\theta$  = 2.36 (h = 4 in.).



(b) 12-in.-jet spacing (R199P7),  $c_{pmax} = 0.0121$ ,  $c_{pmin} = -0.0227$ .



(c) 16-in.-jet spacing (R235P7),  $c_{pmax} = 0.0126$ ,  $c_{pmin} = -0.0151$ . Figure 39. Concluded.

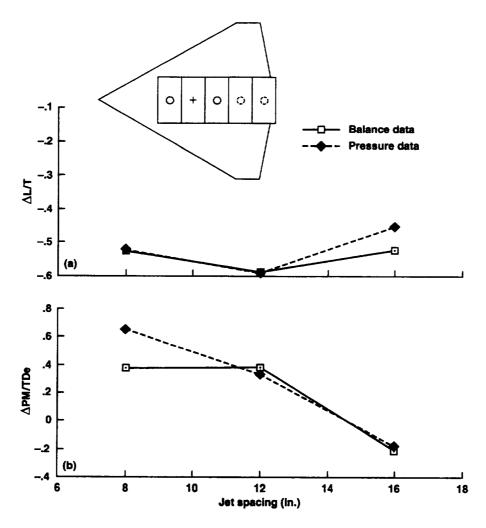


Figure 40. Balance and pressure data comparing jet spacing two-jet delta-wing configuration. Forward jet at the same location,  $h/D_{\theta} = 2.36$  (h = 4 in.). Nozzle pressure ratio (NPR) = 2. (a) Jet-induced lift increments, (b) jet-induced pitching moment increments.

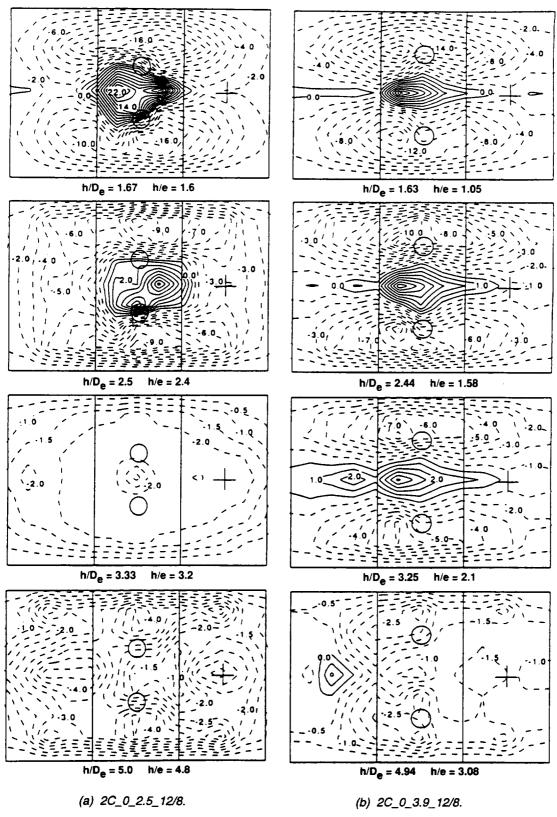


Figure 41. Contours of  $c_p$ \*1000 induced on the model undersurface by two closely spaced jets. Nozzle pressure ratio (NPR) = 2.

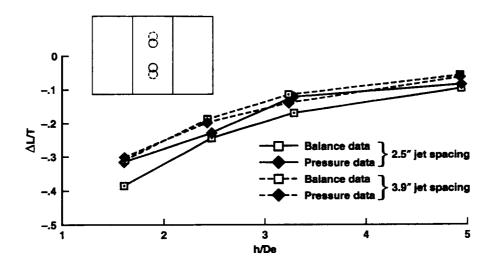


Figure 42. Balance and pressure data comparing the 2.5 in. and 3.9 in. jet spacing for the 12/8 aspect-ratio planform. Nozzle pressure ratio (NPR) = 2.

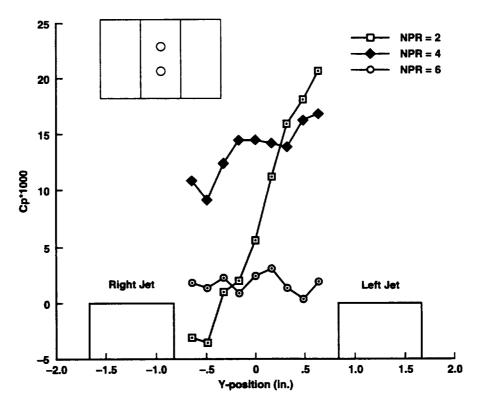


Figure 43. Pressure coefficients between the side-by-side nozzles (X = 0 in.) for the  $2C_0_2.5_12/8$  configuration at nozzle pressure ratio (NPR) = 2, 4, and 6.

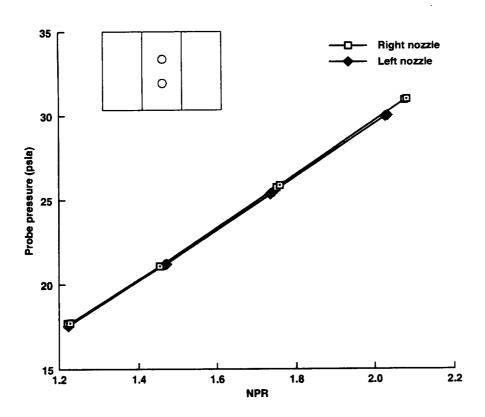


Figure 44. Comparison of nozzle exit pressure for the right and left nozzles of the 2C\_0\_2.5\_12/8 configuration.

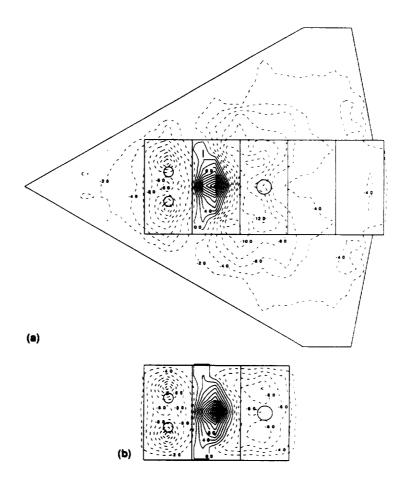


Figure 45. Contours of  $c_p$ \*1000 on the model undersurface induced by an 8 in. spaced forward/aft three-jet arrangement for two different planforms. Nozzle pressure ratio (NPR) = 2 on all jets. (a) 3C\_8\_2.5\_DW (R260P8),  $h/D_\theta$  = 2.35 (h = 4 in.),  $c_{pmax}$  = 0.0206,  $c_{pmin}$  = -0.0211, (b) 3C\_8\_2.5\_12/8 (R268P6),  $h/D_\theta$  = 2.35 (h = 4 in.),  $c_{pmax}$  = 0.0256,  $c_{pmin}$  = -0.0243.

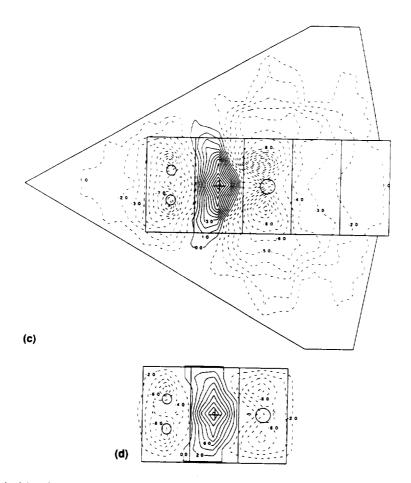


Figure 45. Continued. (c)  $3C_82.5_DW$  (R260P7),  $h/D_\theta=3.53$  (h = 6 in.),  $c_{pmax}=0.0121$ ,  $c_{pmin}=-0.0191$ , (d)  $3C_82.5_12/8$  (R268P9),  $h/D_\theta=3.53$  (h = 6 in.),  $c_{pmax}=0.0168$ ,  $c_{pmin}=-0.0245$ .

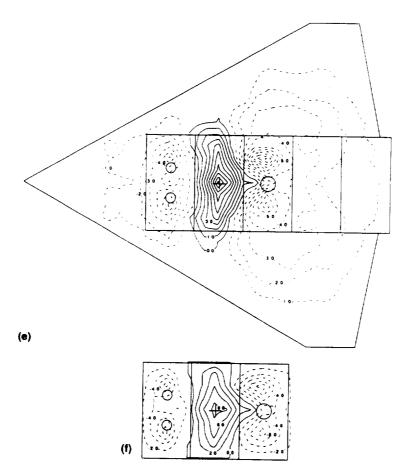


Figure 45. Continued. (e)  $3C_8_2.5_DW$  (R260P6),  $h/D_\theta=4.71$  (h = 8 in.),  $c_{pmax}=0.0093$ ,  $c_{pmin}=-0.0115$ , (f)  $3C_8_2.5_12/8$  (R268P5),  $h/D_\theta=4.71$  (h = 8 in.),  $c_{pmax}=0.0098$ ,  $c_{pmin}=-0.0184$ .

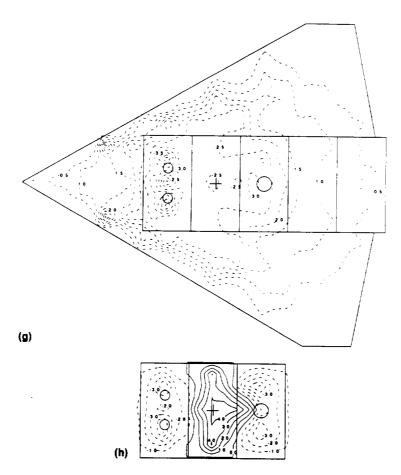


Figure 45. Concluded. (g)  $3C_8_2.5_DW$  (R260P5),  $h/D_\theta = 5.89$  (h = 10 in.),  $c_{pmax} = -0.0003$ ,  $c_{pmin} = -0.0065$ , (h)  $3C_8_2.5_12/8$  (R268P4),  $h/D_\theta = 5.89$  (h = 10 in.),  $c_{pmax} = 0.0055$ ,  $c_{pmin} = -0.0116$ .

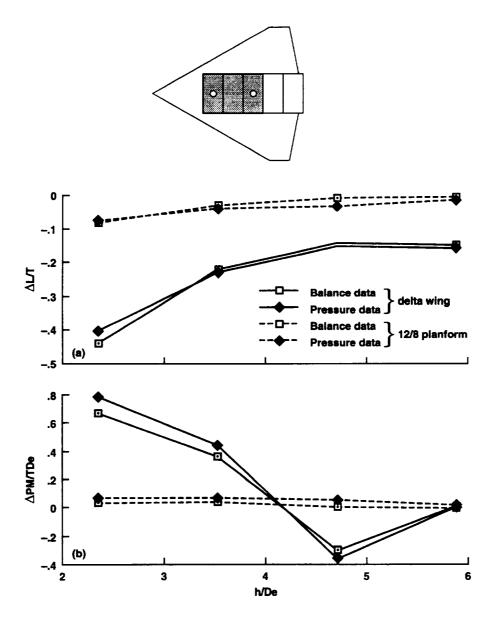


Figure 46. Balance and pressure data comparing planform shape for the three-jet, 8 in. spaced configuration. Nozzle pressure ratio (NPR) = 2. (a) Jet-induced lift increments, (b) jet-induced pitching-moment increments.

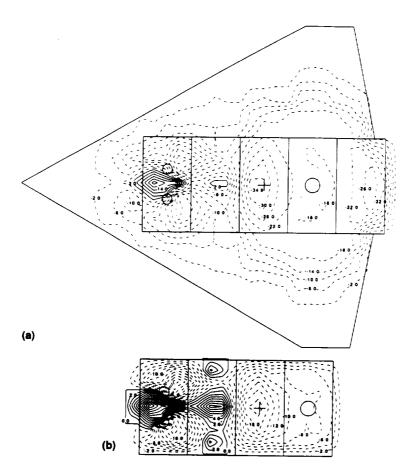


Figure 47. Contours of  $c_p$ \*1000 on the model undersurface induced by a 12 in. spaced fore/aft three-jet arrangement for two different planforms. Nozzle pressure ratio (NPR) = 2 on all jets. (a) 3C\_12\_2.5\_DW (R271P10),  $h/D_e$  = 1.18 (h = 2 in.),  $c_{pmax}$  = 0.0571,  $c_{pmin}$  = -0.0523, (b) 3C\_12\_2.5\_16/8 (R274P10),  $h/D_e$  = 1.18 (h = 2 in.),  $c_{pmax}$  = 0.0540,  $c_{pmin}$  = -0.0400.

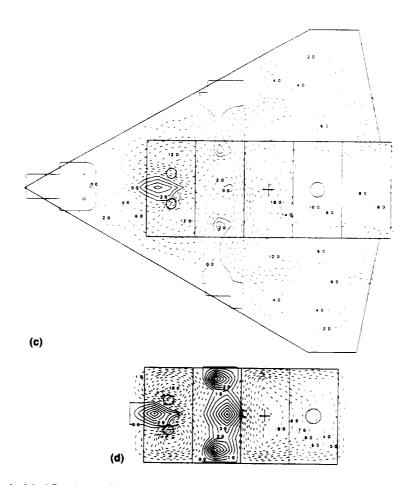


Figure 47. Continued. (c)  $3C_12_2.5_DW$  (R271P9),  $h/D_\theta=1.77$  (h = 3 in.),  $c_{pmax}=0.0149$ ,  $c_{pmin}=-0.0214$ , (d)  $3C_12_2.5_16/8$  (R274P9),  $h/D_\theta=1.77$  (h = 3 in.),  $c_{pmax}=0.0130$ ,  $c_{pmin}=-0.0166$ .

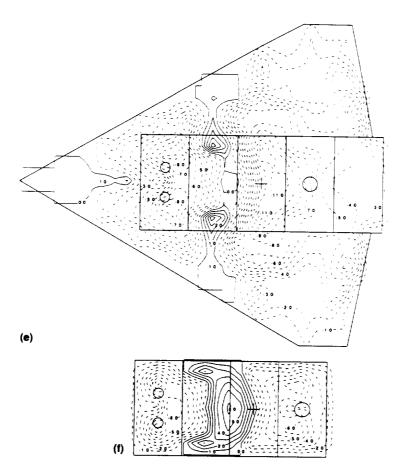


Figure 47. Continued. (e)  $3C_12_2.5_DW$  (R271P8),  $h/D_\theta=2.35$  (h = 4 in.),  $c_{pmax}=0.0046$ ,  $c_{pmin}=-0.0126$ , (f)  $3C_12_2.5_16/8$  (R274P8),  $h/D_\theta=2.35$  (h = 4 in.),  $c_{pmax}=0.0079$ ,  $c_{pmin}=-0.0104$ .

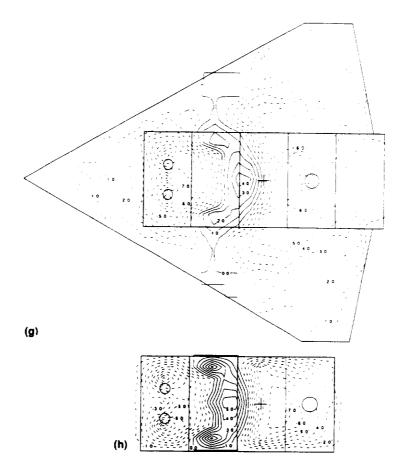


Figure 47. Continued. (g)  $3C_12_2.5_DW$  (R271P7),  $h/D_\theta=3.53$  (h = 6 in.),  $c_{pmax}=0.0041$ ,  $c_{pmin}=-0.0125$ , (h)  $3C_12_2.5_16/8$  (R274P7),  $h/D_\theta=3.53$  (h = 6 in.),  $c_{pmax}=0.0078$ ,  $c_{pmin}=-0.0101$ .

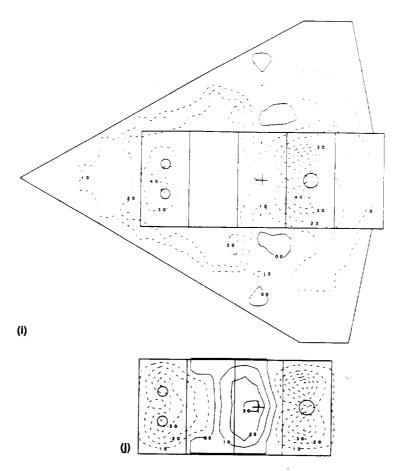


Figure 47. Concluded. (i)  $3C_12_2.5_DW$  (R271P5),  $h/D_\theta = 5.89$  (h = 10 in.),  $c_{pmax} = 0.0004$ ,  $c_{pmin} = -0.0094$ , (j)  $3C_12_2.5_16/8$  (R274P5),  $h/D_\theta = 5.89$  (h = 10 in.),  $c_{pmax} = 0.0035$ ,  $c_{pmin} = -0.0092$ .

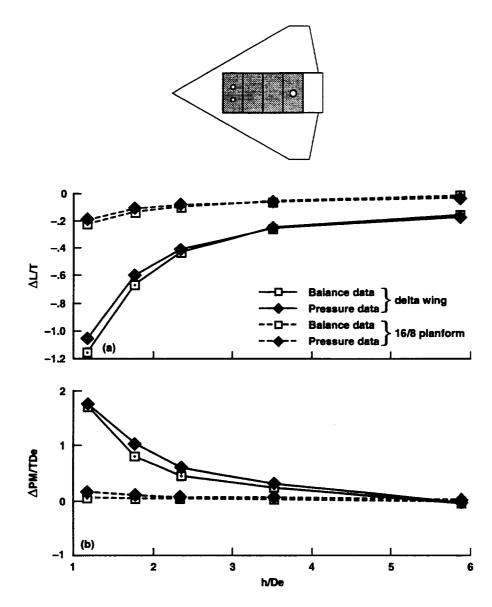


Figure 48. Balance and pressure data comparing planform shape for the three-jet, 12 in. spaced configuration. Nozzle pressure ratio (NPR) = 2. (a) Jet-induced lift increments, (b) jet-induced pitching-moment increments.

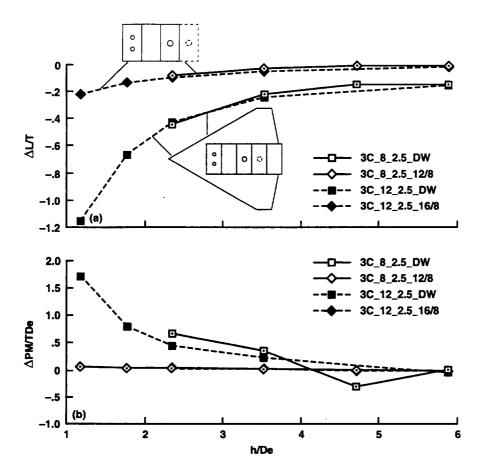
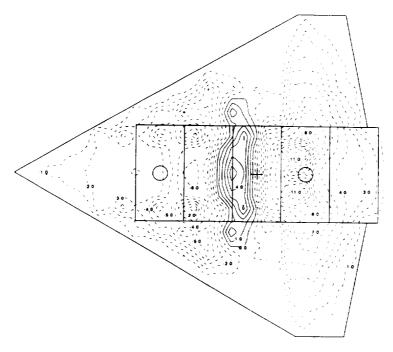
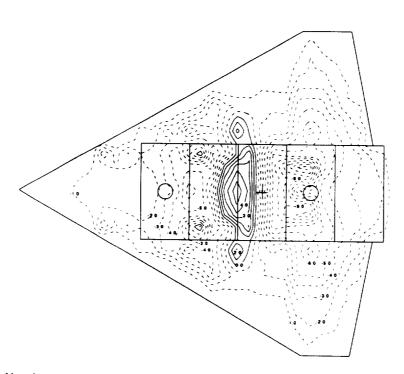


Figure 49. Balance data comparing forward/aft jet spacing and planform geometry. Nozzle pressure ratio (NPR) = 2. (a) Jet-induced lift increments, (b) jet-induced pitching-moment increments.

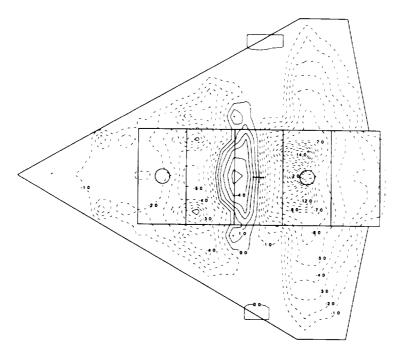


(a) Nozzle pressure ratio (NPR) = 2 (R199P6),  $c_{pmax} = 0.0085$ ,  $c_{pmin} = -0.0180$ .

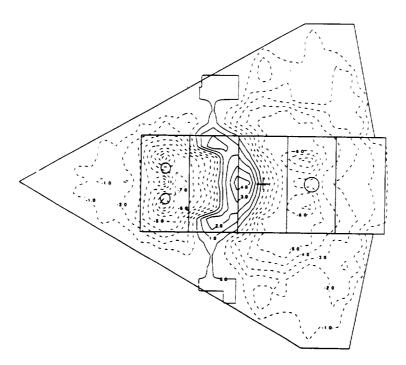


(b) Nozzle pressure ratio (NPR) = 4 (R200P6),  $c_{pmax}$  = 0.0076,  $c_{pmin}$  = -0.0161.

Figure 50. Contours of  $c_p$ \*1000 induced on the model undersurface for a two-jet delta-wing configuration showing the effect of nozzle pressure ratio (NPR). 12 in. jet spacing,  $h/D_\theta = 3.54$  (h = 6 in.).

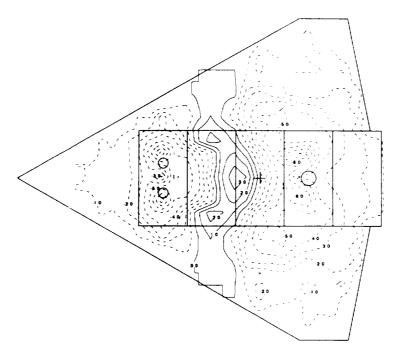


(c) Nozzle pressure ratio (NPR) = 6 (R201P6),  $c_{pmax} = 0.0073$ ,  $c_{pmin} = -0.0197$ . Figure 50. Concluded.

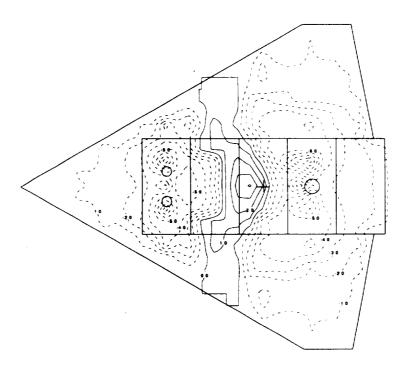


(a) Nozzle pressure ratio (NPR) = 2 (R271P7),  $c_{pmax} = 0.0075$ ,  $c_{pmin} = -0.0125$ .

Figure 51. Contours of  $c_p^*1000$  induced on the model undersurface for a three-jet delta-wing configuration showing the effect of nozzle pressure ratio (NPR). 12 in. forward/aft jet spacing,  $h/D_e = 3.53$  (h = 6 in.).



(b) Nozzle pressure ratio (NPR) = 4 (R272P7),  $c_{pmax} = 0.0047$ ,  $c_{pmin} = -0.0127$ .



(c) Nozzle pressure ratio (NPR) = 6 (R273P6),  $c_{pmax} = 0.0044$ ,  $c_{pmin} = -0.0118$ . Figure 51. Concluded.

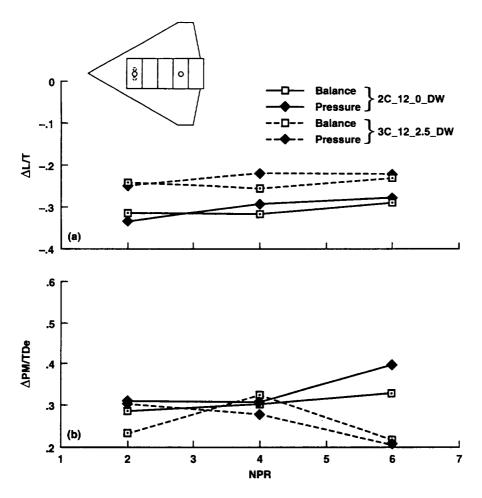


Figure 52. Balance and pressure data as a function of nozzle pressure ratio (NPR) for the  $2C_12_0$ DW and  $3C_12_2.5_0$ DW configurations;  $h/D_0 = 3.53$  (h = 6 in.). (a) Jet-induced lift increments, (b) jet-induced pitching-moment increments.

#### **Appendix**

Force and pressure data for each of the 31 configurations tested, including an extra pressure layout for the  $2C_16_012/24$  configuration (designated with an "X" at the end of the name), are grouped by configuration and are contained in this section. The configurations are presented in the order tested. Each data set (group) for a configuration has three parts. First is a 1:4 scale drawing of that configuration with pressure-tap locations shown (dots representing pressure taps show location only and do not represent their actual size). Second is a table listing each pressure-tap X and Y location, associated areas, and moment arms of those areas (for integration) for each configuration. Third are listings of pressure and balance data for each configuration. Port numbers 92 and 158

were not installed in the model and do not appear in any of the data or configuration setup listings.

Table 4 lists the run conditions for each of the configurations tested. NPR and height numbers in the table represent target set conditions. The actual test conditions are provided in the data sets located in this appendix. In some cases the forward and aft NPRs were intentionally different in order to obtain some data on how pitch control using nozzle thrust affects jet-induced lift and pitch characteristics. Some single-jet data are provided for the 2C\_8\_0\_DW, 2C\_12\_0\_DW, and 2R\_8\_0\_DW configurations. The rest of the configurations are variations on planform geometry (mainly aspect ratio), nozzle arrangements, and nozzle geometry (circular or rectangular).

Table 4. Summary of run conditions and related figures

Configuration	$NPR_f$	NPRa	Height (in.)	Runs	Figure(s)
2C_8_0_DW	-	2.0	20-4	185	
	-	4.0	30-4	186	
	2.0	2.0	30-4	187	39(a), 40
	4.0	4.0	30-4	188	
	6.0	6.0	30-4	189	
	2.0	2.0	4	190A	
	1.95	2.05	4	190A	
	1.90	2.10	4	190A	
	2.10	1.90	4-10	190B	
	1.90	2.10	10-4	190C	
	1.95	2.05	4-10	190D	
	4.0	4.0	10-4	191, P1-3	
	3.9	4.1	4-10	191, P4-6	
	4.1	3.9	10-4	191, <b>P</b> 7-9	
	3.8	4.2	4-10	191, P10-12	
	6.0	6.0	10,6	191B, P13-14	
	5.5	6.4	6,10	191B, P15-16	
	6.5	5.6	10,6	191B, P17-18	
2C_8_0_12/8	2.0	2.0	30-2	192	
	4.0	4.0	30-3	193	
	6.0	6.0	30-4	194	
2C_8_0_4/8	2.0	2.0	30-4	195	
	4.0	4.0	15-3	196	
2C_8_0_4/24	2.0	2.0	15-2	197	
	4.0	4.0	15-3	198A	
	6.0	6.0	4-10	198B	
2C_12_0_DW	2.0	2.0	30-3	199	39(b), 40, 50(a), 52
	4.0	4.0	30-4	200	50(b), 52
	6.0	6.0	30-5	201	50(c), 52
	1.9	2.15	10-4	202	
	1.78	2.25	10-4	203	
	1.98	2.07	10-4	204	
	3.68	4.4	20-4	205A, P1-6	
	4.0	4.0	15	205A, P7	
	5.67	6.45	10-5	205B	
	-	2.0	30-4	206	
	_	4.0	30-6	207	
	_	6.0	30-6	208	
	2.0	2.0	30-4	209	
2C_12_0_16/8	2.0	2.0	15-4	210	-
	4.0	4.0	15-4	211	
	6.0	6.0	15-4	212	
	2.0	2.0	15-4	213, -4 deg gr	ound plane tilt
2C_12_0_16/16	2.0	2.0	15-4	214	
	4.0	4.0	4-10	215	

Table 4. Continued

Configuration	NPRf	NPRa	Height (in.)	Runs	Figure(s)
2C_12_0_16/24	2.0	2.0	30-4	216	
	4.0	4.0	30-4	217	
	6.0	6.0	30-6	218	
2C_12_0_8/24	2.0	2.0	30-4	219	
	4.0	4.0	30-4	220	
	6.0	6.0	30-4	221	
2C_16_0_12/24	2.0	2.0	30-4	222	
2C_16_0_12/24X	2.0	2.0	30-4	223	
	4.0	4.0	30-4	224	
	6.0	6.0	30-5	225	
2C_16_0_4/24	2.0	2.0	30-4	226	
	4.0	4.0	30-4	227	
	6.0	6.0	30-6	228	
2C_16_0_8/24	2.0	2.0	30-4	229	
	4.0	4.0	30-4	230	
	6.0	6.0	15-4	231	
2C_16_0_20/8	2.0	2.0	30-2	232	
	4.0	4.0	30-4	233	
	6.0	6.0	30-4	234	
2C_16_0_DW	2.0	2.0	30-4	235	39(c), 40
	4.0	4.0	30-4	236	
	6.0	6.0	30-6	237	
2R_16_0_DW	2.0	2.0	10,4	238	
	2.0	2.0	30-4	239	
	4.0	4.0	30-4	240	
	6.0	6.0	30-10	241	
	6.0	6.0	30-6	242	
	4.0	4.0	30-4	243	
2R_12_0_DW	2.0	2.0	30-4		PM/TDe data
	4.0	4.0	4-30	245	
	6.0	6.0	30-6	246, P1-6	
	4.0	4.0	6	246, P7	
	2.0	2.0	6	246, P8	
	2.0	2.0	57.5-4	247	
	4.0	4.0	57.4-4	248	
	1.97 3.76	2.19 4.52	4-10 4-15	249 250	
		<del> </del>			
2R_12_0_16/8	2.0	2.0	57.5-2	251	
	4.0 6.0	4.0 6.0	57.5-4 4-10	252 253	
				- <del></del>	
2R_8_0_DW	2.0	2.0	57.5-4 20.4	254	
	4.0	4.0	20-4 57.5.4	255 257	
		2.0	57.5-4	257	

Table 4. Concluded

Configuration	NPR <sub>f</sub>	NPR <sub>a</sub>	Height (in.)	Runs	Figure(s)
2R_8_0_DW	-	4.0	57.5-4	258	
	_	6.0	57.5-4	259	
3C_8_2.5_DW	2.0	2.0	57.5-3	260	45(a)(c)(e)(g), 46, 49
	4.0	4.0	57.5-4	261	
	6.0	6.0	57.5-6	262	
2C_0_2.5_12/8	2.0	_	30-2	263	41, 42, 43
	4.0	-	30-3	264	43
	6.0		30-3	265	43
3C_8_2.5_12/8	2.0	2.0	30-2	268	45(b)(d)(f)(h), 46, 49
	4.0	4.0	30-2	269	
	6.0	6.0	30-3	270	
3C_12_2.5_DW	2.0	2.0	57.5-2	271	47(a)(c)(e)(g)(i), 48, 49, 51(a), 52
	4.0	4.0	57.5-3	272	51(b), 52
	6.0	6.0	30-4	273	51(c), 52
3C_12_2.5_16/8	2.0	2.0	57.5-2	274	47(b)(d)(f)(h)(j), 48, 49
	4.0	4.0	30-3	275	
	6.0	6.0	30-3.2	276	
3C_16_2.5_20/8	2.0	2.0	57.5-2	277	
	4.0	4.0	30-3	278	
	6.0	6.0	30-3	279	
4C_16_2.5/3.9_20/8	2	2	57.5-2	280	
	4	4	30-3	281	
	6	6	3-30	282	
4C_12_2.5/3.9_16/8	2	2	57.5-2	283	
	4	4	30-3	284	
	6	6	30-3	285	
4C_8_2.5/3.9_12/8	2	2	57.5-2	286	
	4	4	30-3	287	
	6	6	30-3	288	
2C_0_3.9_12/8	_	2	57.5-2	289	41, 42
_	_	4	57.5-3	290	
	_	6	30-3	291	
3C_8_3.9_12/8	2	2	57.5-2	292	
	4	4	30-3	293	
	6	6	30-3	294	
3C_12_3.9_16/8	2	2	57.5-2	295	
	4	4	30-2	296	
	6	6	30-3	297	
3C_16_3.9_20/8	2	2	57.5-2	298	
	4	4	30-2	299	
	6	6	30-3	300	

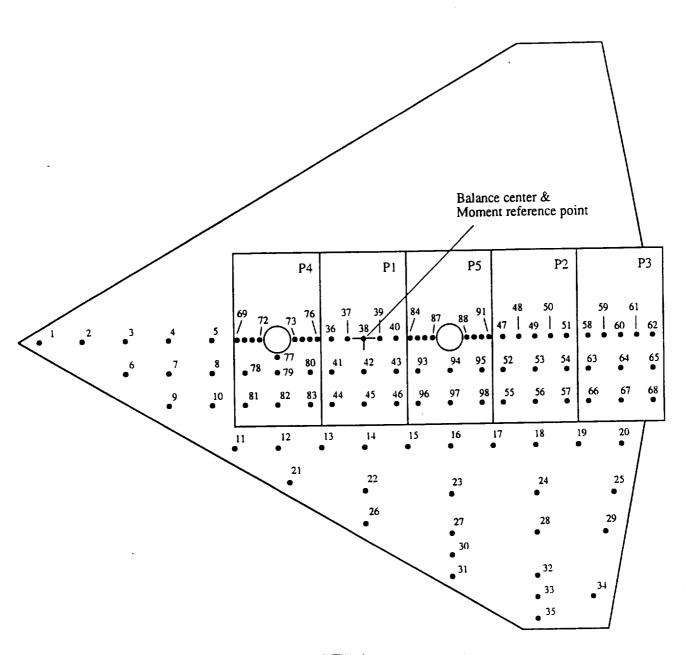


Figure 53. Configuration 2C\_8\_0\_DW;  $D_\theta$  = 1.697 in.,  $A_{jet}$  = 2.26 in.<sup>2</sup>.

### Conf. # 2C\_8\_0\_DW

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
	14.6	0 '	2.3	15
2	12.86	0	6918	13
3	11	0	3	11
4	9	Ö	3	9
5	11 9 7	Ö	3 3 3 8.546	7
6	10.9	1.5	8 546	11
1 2 3 4 5 6 7 8	10.9 9 7	1.5	6.540	11
ģ	7	1.5	6 6 7.166	9 7 9 7 6 4 2 0 -2
0	8.87	1.5	7 166	,
10	0.07	3	7.100	9
10	7	3	7 8.91	1
11	6.14	5	8.91	6
12	4 2 0	5	8	4
13	2	5	8	2
14	0	5	8	0
15	-2	5	8	-2
16	-4	1.5 1.5 3 3 5 5 5 5 5 5 5 7 7 7 7 7 8.5	8 8 8 8 8 8	-4
17	-6	5	8	-6 -8
18	-8	5	8	-8
19	-10	5	8	-10
20	-11.91	5	8.06	-12
21	3.06	6.6	7.302	3.5
22	0	7	16	0
23	-4	ż	16 16	-4
24	-8	7	16	-8
25	-11.31	7	10.484	-0 -11.6
26 26	-11.31 0.765	9.5		
20 27	-0.765	8.5	9.904	0
27	-4	9	12	-4
28	-8	9 9 9	16	-8 -11.2
29	-11.11	9	8.908	-11.2
30	-4	10	8	-4
31	-4.84	11	8.376	-4
32	-8	11	12 8	-8
33	-8	12	8	-8
34	-10.86 -8.17	12	12.005	-10.6
35	-8.17	13	6.883	-8 5.85
69	5.85	0	0.634	5 85
70	5.5	Ŏ	0.683	5.5
71	5.15	ŏ	0.683	5.15
72	4.8	Ö	0.619	4.8
73	3.2	0		3.2
			0.619	
74 75	2.85	0	0.683	2.85
75	2.5	0	0.683	2.5
76	2.15	0	0.634	2.15
77	4	0.8	1.238	4
78	5.5	1.5	3.19	5.5
79	4	1.5	3.825	4

Conf. # 2C\_8\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
80	2.5	1.5	3.19	2.5
81	5.5	3 3 3	4.375	5.5
82	4	3	5.25	4 2.5
83	2.5	3	4.375	2.5
36	1.5	0	1.313	1.5 0.75
37	0.75 0	0 0	1.125 1.125	0.73
38 39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
40	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0.
43	-1.5	1.5	3.75	0 -1.5
44	1.5	3	4.375	1 5
45	0	3 3 3 0	5.25	0
46	-1.5	3	4.375	-1.5
84	-2.15	0	0.634	-2.15
85	-2.5	0	0.683	-2.5
86	-2.5 -2.85	0	0.683	0 -1.5 -2.15 -2.5 -2.85
87	-3.2 -4.8	0	0.619	-3.2
88	-4.8	0	0.619	-4.8
89	-5.15	0	0.683	-5.15
90	-5.5 -5.85	0	0.683	-5.5
91	-5.85	0	0.634	-5.85
93	-2.5	1.5	3.19	-2.5
94	-4	1.5	5.062	-4
95	-5.5	1.5	3.19	-5.5
96 07	-2.5	3 3 3 0	4.375 5.25	-2.5 -4
97 08	-4 -5.5	3	5.25 4.375	- <del></del> -5.5
98 47	-5.5 -6.5	0	1.313	-6.5
48	-7.25	ŏ	1.125	-7.25
49	-8	ŏ	1.125	-8
50	-8 -8.75	ŏ	1.125	-8.75
51	-9.5	ŏ	1.313	-9.5
52	-6.5	1.5	3.75	-6.5
53	-6.5 -8	1.5	4.5	-8
54	-9.5	1.5	3.75	-9.5
55	-6.5		4.375	-6.5
56	-8	3 3 3 0	5.25	-8
57	-9.5	3	4.375	-9.5
58	-10.5		1.313	-10.5
59	-11.25	0	1.125	-11.25
60	-12	0	1.125	-12
61	-12.75	0	1.125	-12.75
62	-13.5	0	1.313	-13.5
63	-10.5	1.5	3.75	-10.5
64	-12	1.5	4.5	-12
65	-13.5	1.5	3.75	-13.5
66	-10.5	3 3 3	4.375	-10.5
67	-12	5	5.25 4.375	-12
68	-13.5	3	4.375	-13.5

Total ' NPR NPR X-loc	Point h/De = Thrust = Front = Aft = Y-loc	3 16.84 26.40 1.00 2.01 ACP	12.62 26.52 1.00 2.02 ACP	8.40 26.45 1.00 2.01 ACP	6.77 26.80 1.00 2.03 ACP	5.07 26.72 1.00 2.03 ACP	3.42 26.63 1.00 2.02 ACP
- o'n'n' o'n'	000000	000000	-0.00022 -0.00026 -0.00026 -0.00016	0.00053 0.00053 0.00048 0.00049	00085 00108 00096	000000	
44044	900000		-0.00010 -0.00010 -0.00010 -0.00014	0.00053	0.00103 0.00103 0.00105 0.00111		0.00265
0000000	000000		0.00011 -0.00013 -0.00014 -0.00024 -0.00024	0.00062 0.00062 0.00066 0.00064 0.00064	0.00108 0.00109 0.00102 0.00110	9955	00643
00,40000		0000000	-0.00033 -0.00033 -0.00032 -0.00032 -0.00033	000000	-0.000862 -0.000660 -0.000968 -0.000842 -0.000828	-0.001714 -0.001970 -0.003167 -0.001613 -0.001801	0.0049 0.0055 0.0054 0.0045
10.60	10.00 11.00 11.00 12.00 13.00		000000	0.000819 -0.000819 -0.000675 -0.000424 -0.000722	0.000111 0.0001111 0.00058 0.00058	000000	000351
Force an Balance Pressure Balance Pressure	Moment h/De AL/T AL/T AH/TDe	Summary 16.84 -0.039 -0.032 -0.136	12.62 -0.053 -0.044 0.158	8.40 -0.113 -0.107 0.269 0.315	6.77 -0.193 -0.183 0.450	5.07 -0.352 -0.342 0.842 1.118	3.42 -0.732 -0.719 2.166 2.622

	3.42 26.63 1.00 2.02 ACP	0.000078 0.000078 0.0001812 0.0001814 0.0001814 0.0001814 0.0001814 0.0001814 0.0001814 0.0001814 0.0001814 0.0001814 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811 0.0001811	0.00537
its 185	5.07 26.72 1.00 2.03	0.000000000000000000000000000000000000	0.001968
re Increment	6.77 26.80 1.00 2.03 ACP	0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.000935 0.0009	0.001013
ced Pressu	8.40 26.45 1.00 2.01 ACP	0.0000113	0.00041
Jet-Indu 8-0-DW	12.62 26.52 1.00 2.02 ACP	0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313 0.0001313	0.00023
ation: 2C-1	16.84 26.40 1.00 2.01 ACP	0.0000133	000147
Configure	Point h/De = Thrust = Front = Aft = Y-loc		•
	Total NPR NPR NPR X-loc	21819	9

	3.43 68.31 1.00 3.98 ACP	0.000000000000000000000000000000000000
	5.07 68.40 1.00 3.98 ACP	0.00102288 0.00102288 0.00102099999999999999999999999999999999
	68.64 1.00 3.99 ACP	4 4 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
	8.41 68.71 1.00 4.00 ACP	0.000000000000000000000000000000000000
	12.62 68.65 1.00 3.99 ACP	0.000000000000000000000000000000000000
	2 16.88 68.86 1.00 4.00	0.000000000000000000000000000000000000
	25.31 68.86 1.00 4.00	Decided to the control of the contro
	Point h/De = Thrust = R Front = R Aft = Y-loc	3 000 3 000 000 000 000 000 000 000 000
	Total T NPR NPR X-loc	
	3.43 68.31 1.00 3.98 ACP	0.000155 0.0001855 0.0001855 0.0002241 0.0002241 0.000224255 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023924 0.00023925 0.00023924 0.00023924 0.00023925 0.00023925 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392 0.0002392
	6 3.07 3.43 68.40 68.31 1.00 1.00 3.98 ACP ACP	00000000000000000000000000000000000000
its 186	200.040 000.040 000.040	0.00240 - 0.000334 - 0.000334 - 0.000335 - 0.000335 - 0.000335 - 0.000335 - 0.000335 - 0.000335 - 0.000335 - 0.000335 - 0.000355 - 0.000335 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0.000355 - 0
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Jet-Induced Pressure -0-DW	62 8.41 6.75 5.07 6.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00	0.000056 0.000011 0.000252 0.000455 0.000556 0.00000066 0.0000171 0.0000017 0.0000186 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187 0.0000187
Jet-Induced Pressure 2C-8-0-DW	6. 2 3 4 6.75 5.07 8.86 8.87 6.75 5.07 8.86 8.87 6.87 6.87 6.87 6.87 6.87 6.8	0.000199 -0.000245 -0.000240 -0.000649 -0.0001924 -0.0001924 -0.0001924 -0.0001925 -0.000640 -0.0001924 -0.0001925 -0.000640 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001926 -0.0001
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	2.38 52.62 2.01 2.05 ACP	0.000
	3.54 52.77 2.01 2.06 ACP	0.000000000000000000000000000000000000
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	8.85 51.98 2.01 2.02 ACP	0.000000000000000000000000000000000000
	11.8 52.00 52.01 2.01 ACP	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
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	Point h/De = Thrust = R Front = R Aft = Y-loc	## ## ## ## ## ## ## ## ## ## ## ## ##
	Total TI NPR I NPR	Pressure Pre
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	17.84 136.75 3.99 4.01 ACP		Summary Summar
	Point h/De =   Thrust = PR Front = PR Aft = Y-loc	00000000000000000000000000000000000000	AVORENT N/VE AL/T = A AM/TDF = AM/TDF =
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Jet-Induced Pressure Increments Configuration: 2C-8-0-DM

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Jet-Indu -8-0-DW	,	~	ះឡ	-0.00045	-0.00207	-0.00197	-0.00321	-0.00326	-0.00320	-0.00331	-0.00317	-0.00312	-0.00357	-0.00415	0.00016	0.00327	-0.00054	0.00103	0.00282	-0.00673	-0.00653	-0.00672	-0.00395	-0.00307	-0.00247	-0.00211	-0.00123	-0.00100	-0.00093	-0.00207	-0.00258	-0.00391	-0.00499	-0.00469	-0.00224	0.00292	-0.00292	-0.00611	-0.00611	-0.00194	-0.00144	-0.00114	-0.00675	-0.00557	-0.00459	-0.00502	-0.00194	-0.00761	-0.00703	-0.00/03	
uration: 2C	.3	<b>M-</b>	1.89	0.00046	0.00334	0.00356	0.00356	0.00406	0.00380	0.00503	0.01136	01659	0.01121	00230	01115	0.00796	0.02119	0.01642	0.003/4	0.00779	0.00689	0.00575	0.00683	0.00569	0.00340	0.00209	0.00111	0.00094	0.00133	0.00388	0.00462	0.00573	0.00424	0.01407	0.01267	0.02412	0.02412	0.00831	0.00831	0.00366	0.00126	0.00141	0.00957	0.00797	0.00381	0.01325	0.00165	.008	0.01838	0.00366	
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Jet-Indu 8-0-DW	3.51 136.77 1.98 4.02 ACP	0.001449 0.001445 0.001445 0.001445 0.001447 0.001447 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444 0.001444	-0.004168
Jet-Induced Pressure Configuration: 2C-8-0-DM	5.87 136.65 3.98 4.02 ACP	0.0000883 0.0000883 0.0000883 0.0000883 0.0000883 0.0000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.00088 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0.000883 0	
Configur	Point h/De = Thrust = R Front = R Aft = Y-loc		m
	Total 1 NPR NPR X-loc	8.000000000000000000000000000000000000	-6.50

	5.88 135.86 3.75 4.21 ACP	0.001521 0.001621 0.001631 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643 0.001643	5.88 -0.143 -0.145 0.288 0.326
	3.51 135.88 3.75 4.21 ACP	0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931 0.0001931	3.51 -0.276 -0.253 0.359
	2.32 135.91 3.75 4.21 ACP	0.008287 0.008287 0.008287 0.002295 0.002228 0.002328 0.002221 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281 0.002281	2.32 -0.531 -0.499 0.566
	2,32 136,88 4.08 3,92 ACP	0.009800 0.009800 0.0012800 0.0012800 0.0012800 0.000533	2,32 -0.534 -0.520 0.535 0.699
	3.51 136.94 4.08 3.92 ACD	0.0009559599999999999999999999999999999	3.51 -0.281 -0.269 0.213 0.300
2/2	5.87 136.96 4.08 3.92 ACP	0.001989 0.000989 0.000989 0.001989 0.001989 0.001989 0.001999 0.001999 0.001999 0.000998 0.000998 0.000999 0.000999 0.000999	5.87 -0.124 -0.115 0.062 0.107
Page 2/2	5.86 136.83 3.88 4.12 ACP	0.001453 0.001453 0.00158 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278 0.001278	5.86 -0.131 -0.128 0.200 0.262
ements Run 191	3.51 136.89 3.89 4.12 AOP	0.003893 0.003893 0.003893 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833 0.003833	3.51 -0.275 -0.260 0.305 0.416
Jet-Induced Pressure Increments 0-DM	2.33 136.86 3.89 4.12 A.00	0.0006818	2.33 -0.527 -0.496 0.508
iced Pressu	2.33 136.74 3.98 4.02 ACD	0.0013398888888888888888888888888888888888	2.33 -0.532 -0.505 0.533 0.692
Jet-Indu -8-0-DW	3.51 136.77 3.98 4.02 ACD	0001388	3.51 -0.285 -0.277 0.250
Jet- Configuration: 2C-8-0-DW	5.87 136.65 3.98 4.02 ACD	0.001965 0.001965 0.001965 0.001966 0.001966 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969 0.001969	Summary 5.87 -0.128 -0.124 0.116
Configu	Point h/De = Total Thrust = NPR Front = NPR Aft = X-loc Y-loc		id Moment Summary h/De = 5 AL/T = -0. AL/T = -0. AM/TDe = 0.
	Total NPR NPR	### ### ##############################	Force and Balance Pressure Balance

14 3.51 224.25 5.98 6.00 ACP	0.000000000000000000000000000000000000
224.18 224.18 5.98 6.00 ACP	A STATE OF THE PROPERTY OF THE
Point h/De = Thrust = R Front = R Y-loc	3 .00 3 .00 3 .00 3 .00 3 .00 3 .00 3 .00 5 .00 5 .00 5 .00 7 .00 7 .00 111 .00 112 .00 113 .00 114 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .00 115 .0
Total Thy NPR Fr NPR A X-loc	-8.00 -1.05.50 -1.2.00 -1.2.00 -2.00 -2.000 -1.2.00 -1.2.00 -1.2.00 -1.2.00 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1.3.50 -1
3.51 232.73 6.50 5.54 AQP	0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015 0.001015
17 5.86 231.69 6.48 5.54 6.00	0.000855 0.000865 0.000865 0.000865 0.000865 0.00130 0.00131 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136 0.00136
217.60 217.60 5.50 6.34 ACP	0.0000128 0.0000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128 0.000128
3.51 217.62 5.50 6.34 ACP	0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000898 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.000888 0.0
3.51 224.25 5.98 6.00 6.00	0.00101844 0.00101844 0.00101844 0.00101846 0.00101846 0.00101836 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846 0.00101846
224.18 5.98 5.98 6.00 ACP	0.000000000000000000000000000000000000
Point h/De = thrust = Front = Aft = Y-loc	

3.51 -0.256 -0.229 0.202 0.211

5.86 -0.107 -0.107 -0.018

5.84 -0.133 -0.139 0.272 0.327

3.51 -0.265 -0.238 0.382 0.462

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3.51 232.73 6.54 6.54 6.55 6.54 6.003314 6.003314 6.003314 6.0032314 6.003314 6.003314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.0032314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314 6.003314

16 5.84 217.60 5.50 6.34 ACP

3.51 217.62 5.50 6.34 ACP

Jet-Induced Pressure Increments Configuration: 2C-8-0-DW

0000572 0000574 0000297 00002087 0001088 0001088 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089 0001089

999999999999999999999999

001362 001382 001384 001348 001319 001319 001319 001393 001393 001393 001385 001385 001385 001385 001385 001385 001385 001385 001385 001385

003443 0003443 0001443 000154 000154 000554 000578 000578 000578 000578 000578 000578 000578 000578

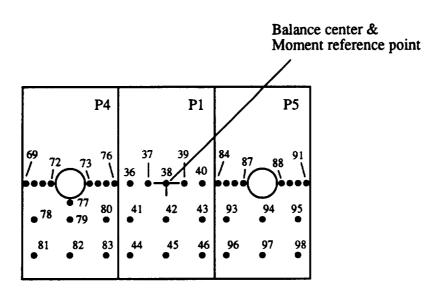


Figure 54. Configuration 2C\_8\_0\_12/8;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_8\_0\_12/8

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
69	5.85	0	0.634	5.85
70	5.5	0	0.683	5.5
71	5.15	0	0.683	5.15
72	4.8	0	0.619	4.8
73	3.2	0	0.619	3.2
74	2.85	0	0.683	2.85
75	2.5	0	0.683	2.5
76	2.15	0	0.634	2.15
77	4	0.8	1.238	4
78 70	5.5	1.5	3.19	5.5
79	4	1.5	3.825	4
80	2.5	1.5	3.19	2.5
81	5.5	3	4.375	5.5
82	4	3 3 3 0	5.25	4
83	2.5	3	4.375	2.5
36	1.5 0.75		1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3 3 3	5.25	0
46	-1.5	3	4.375	-1.5
84	-2.15	0	0.634	-2.15
85	-2.5	0	0.683	-2.5
86	-2.85	0	0.683	-2.85
87	-3.2	0	0.619	-3.2
88	-4.8	0	0.619	-4.8
89	-5.15	0	0.683	-5.15
90	-5.5	0	0.683	-5.5
91	-5.85	0	0.634	-5.85
93	-2.5	1.5	3.19	-2.5
94	-4	1.5	5.062	-4
95	-5.5	1.5	3.19	-5.5
96	-2.5	3	4.375	-2.5
97	-4	3 3 3	5.25	-4
98	-5.5	3	4.375	-5.5

	1.15 50.94 1.98 2.01 ACP		-0.347 -0.297 0.105 -0.012
	2.36 50.91 1.98 2.01 ACP	NAALUWANAUGOOLAMALANUNHUNCOONAAWACANOO K	-0.137 -0.120 0.098 -0.005
nts 1 192	3.53 50.92 1.98 2.01 ACP		-0.065 -0.057 -0.049 -0.008
ire Increments Run 192	4.70 51.00 1.98 2.01 ACP	- +0000040000400000000000000000000000000	-0.030 -0.031 0.000 -0.008
et-Induced Pressure	5.87 51.04 1.98 2.01 ACP	a nnn-co-ceann-cannaidh ann ann ann ann ann ann ann ann ann an	-0.018 -0.028 0.007 -0.007
26	8.83 51.05 1.98 2.01 ACP	0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918 0.0006918	-0.008 -0.019 0.033
ation: 2C-	111.77 51.13 1.98 2.02 ACP		-0.006 -0.020 0.088 -0.017
Configuration:	Point h/De = Thrust = ! Front = Aft = Y-loc	A Mose of the Control	AL/T = AL/T = AM/TDe = AM/TDe =
	Total NPR NPR NPR	88.81888888888888888888888888888888888	Balance Pressure Balance Pressure

	1.72 136.77 4.00 4.01 ACP	00000000000000000000000000000000000000	0.024
	2.32 136.81 4.00 4.01 ACP	0.00449 0.006221 0.006221 0.006221 0.00116141 0.0111713 0.0111713 0.011713 0.011713 0.011713 0.011713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.0171713 0.017171	0.012
	3.49 136.81 4.00 4.01 ACP	000000000000000000000000000000000000000	282
ements Run 193	4.69 136.84 4.00 4.01 ACP		-0.006
Jet-Induced Pressure Increment 0-12/8	5.86 136.84 4.00 4.01 ACP	THE TOO TOO THE TOTAL THE	900.0-
iced Pressu	8.83 136.86 4.00 4.01 ACP		-0.008
Jet-Indu -8-0-12/8	11.78 137.02 4.01 4.02 ACP	0.000010388	88
Configuration: 2C-	17.68 137.13 4.02 ACP	2	0.028
Configu	Point h/De = Thrust = Front = Aft = Y-loc	Month of the control	
	Total 7 NPR NPR X-loc	88.88.88.88.88.88.88.88.88.88.88.88.88.	Balance Pressure

	7	2.35	221.12	5.92	5.95	<b>d</b> ⊘ <b>p</b>		1000000																		-0.004905			-0.029818	ö		170510.0-				-0.008430									-0.008318			5.3	ŝ	ŝ	-0.017
	9	3	221.08	5.92	5.94	ď2ø	8		38	3:	3	8	8	8												-0.003604						-0.004420																3.53	-0.069	-0.031	-0.01
194	50		221.14	5.92	5.95	<b>Q</b> Cb	110000	-0.001374	j,	-0.002191	-0.003042	0.002438	0.000325	0.000372	0.000111	0.002164	0.003446	0.002315	0.001668	-0.000519	Ö	-0.002025	-0.001172	0.000404	-0.003368	-0.002175	-0.002167	-0.001471	-0.011651	o,	-0.004200	-0.00033	0.001037	-0.000332	-0.001869	0	-0.001909	-0.001944	-0.002917	-0.001092	0.000426	0.001845	000000	-0.002998	-0.002998			_	5	2	-0.026
re Increments Run 19	•	S	221.11	5.92	5.95	<b>Q</b> O	5	-0.000E3	?'	•	٠,	٩,	٩	۰.	٩	٠,	٦	٠,	٧,	٦	٦	٠.	٠.	۳	٠.	٠	٠.	٠.	٠,	٠·	٠,٠	0.00000	••	•	9	۹.	100.	ŝ	.0030	8	0000		1	1					-0.022	-0.020	0.029
ced Pressure		œ	220.94	5.92	5.94	Q.	3	33	3	5	0.00	š	ខ្ល	Š	Š	Š	8	훓	š	š	-0.000814	8	80000	-0.001018	-0.001874	-0.001229	-0.001033	-0.001125	ø,	ö,	-0.000487	-0.000432	ċ	# E 9000 0-			-0.001067	-0.000515	-0.003475	-0.000728	-0.000175	-0.00056	3	2000	Ò				5	2	-0.042
Jet-Induced 8-0-12/8			221.06	•		<b>₽</b> Cb		0.00000	87/000.0-	0.000/88	-0.001593	-0.000784	-0.000547	-0.000640	-0.000252	-0.000233	-0.000213	00130	-0.000200	-0.000234	-0.000156	-0.000392	-0.000402	-0.000660	-0.001628	-0.000B68	-0.000718	-0.000758	-0.001797	-0.000977	-0.000745	-0.000462	-0.000161	00010	500000-0-	-0.00000	-0.000622	-0.000507	-0.003439	-0.000347	-0.000388	-0.000412	2000.0	00000	-0.000489			÷	۰,	۰.	-0.042
ation: 2C-8		~	221.14	5.93	5,95	QQ PQ	,,,,,	-0.000646	9000	.0000	.00131	.00063	.0003	.00034	.0003	.0000	۰.	٩	.0000	٣.	۳.	۳.	۳.	۳.	٣,	٦.	٣.	3	٣.		3	٠,				-0.00000	.0010	. 0003	.0038	0.003	0.000	0.000			200			۲.	5	5	0.049
Configuration:	Point	h/De #	Thrust =	Front	Aft	Y-10																										1.50															Moment	h/De n	<b>A</b> L/1	<b>₹</b> /.	
			Total 1	MPR	ad.	X-10c			0.0	5.15	8.	3.20	2.85	2.50	2.15	1.50	0.75	0.0	-0.75	-1.50	~		-2.85	-3.20	9.		-5.50	-5.85	00· <b>+</b>	5.50	0.4	2.50	1.50		2.50		-5.50	5.50	00· <del>†</del>	2.50	1.50	00.0	25.	200	2	3	Force and		Balance	Pressure	Balance

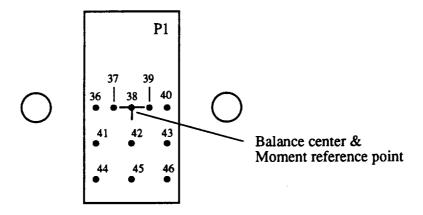


Figure 55. Configuration 2C\_8\_0\_4/8;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_8\_0\_4/8

Orif. #	Mom. arm	Sta. y	$\Delta$ . Area	Sta. x
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0 -0.1
38 39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0 -0.1
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3	5.25	0 -0.1
46	-1.5	3	4.375	-1.5

	7			•		<b>₽</b>	22	55	582	799	150	93	36	7.4	24	0	41		12	5		52	010
		-	1 2	; `	9 -	. `	-0.030422			-0.014	-0.031450	-0.0300		-0.032774			•		-	9		9	0.010
	٠	2.4	7.7	200	-	Ş	0.001667	0.021418	0.023500	0.012379	-0.005042	0.001652	0.022905	-0.005168	-0.003194	0.017104	-0.005710		2.34	0.040	0.044	-0.049	0.010
Run 195	2	3 52	51.67	50	-	<b>₽</b> Cb	0.002818			0.005086					-0.000350				3.52	0.019	0.020	-0.018	0.001
0-4/8 Run 19	•	17.7	52.14	2.05	-	₽ ¶	0.002206	0.002575	0.003855	0.002575	0.002057	0.000837	0.004906	0.000782	0.000359	0.003486	-0.000359		4.71	0.00	0.014	-0.039	0.001
	•	5.89	52.27	2.05	2.00	₽Ç₽	0.000457	0.001256	0.001704	0.002558	0.000531	-0.000045	0.002474	0.000323	-0.000025	0.000263	0.000273		5.89	0.004	0.005	-0.016	-0.001
8-0-4/8	ď	8.83	52.54	2.06	2.00	δ	-0.000450	-0.000148	-0.000035	0.000049	0.000232					-0.000292	-0.000178		8.83	-0.001	-0.001	-0.010	-0.001
Configuration: 2C-8-0-4/8	-	17.67	52.25	2.07	1.98	Ş	-0.000278	-0.000268	-0.000179	-0.000209	-0.000268	-0.000199	-0.000238	-0.000422	-0.000139	-0.000283	-0.000258	Summary.	17.67	-0.003	-0.002	-0.010	0.00
Configur	Point	h/De =	È			Y-10c						1.50						d Moment Summary	h/De =	AL/T =	<b>∆L</b> /T #		AM/TDe
			Total	AP.	NPR	X-10c	1.50	0.75	0.0	-0.75	-1.50	1.50	0.00	-1.50	1.50	0.0	-1.50	Force and		Balance	Pressure	Balance	Pressure

	Config	Configuration: 2C-	Jet-Indu 2C-8-0-4/8	Jet-Induced Pressure 0-4/8	Incr	ements Run 196		
	Point	-	~		-	S	•	
	P/15	8.8	5.90	4.73	3.54	2.35	1.76	
Total	Thrust =	137.44	137.40	137.37	137.32	137.34	137.32	
adv	Pront .	00.7	4.00	4.00	• 00	00.	4.00	
A	NPP Aft	70.7	4.04	4.04	4.03	4.03	4.03	
X-loc	Y-10c	Ş	Q.	Q	Q	₽CD	<b>Q</b>	
1.50	0.00		0.000599	0.000796	0.002159	0.003926	-0.002804	
0.75	0.00	-0.000204	0.001136	0.001851	0.005735	0.018354		
0	00.0		0.001143	0.002000	0.005820	0.025093		
-0.75	0.00	0.000085	0.000491	0.001616	0.004519	0.014229	0.015793	
-1.50	00.0	-0.000202	0.000140	•	-0.000100	-0.000514	-0.010077	
1.50	1.50	-0.000300	0.000338	0.000497	0.001055	0.001891	-0.004629	
00.0	1.50	-0.000091	-0.000015	0.002493	0.005451	0.020524	0.043018	
-1.50	1.50	-0.000338	0.000019	-0.000070	-0.000406	-0.001087	-0.010604	
1.50	3.00		0.000057	0.000267	0.001673	-0.001743	-0.008852	
00.0	3.00		0.000302	0.001705	0.003429	0.013798	0.033135	
-1.50	3.00		-0.000735	-0,000355	-0.000208	-0.003743	-0.011609	
Force and	d Moment	Summary						
		8.84	5.90	4.73		2.35		
Balance	<b>L</b> /1	= -0.002	0.00	0.003	0.012	0.042	0.057	
Pressure		-0.001	0.001	900.0		0.047		
Balance	8	= -0.013	-0.030	-0.041		-0.046		
Pressure		000.00 =	0.001	0.001		0.005		

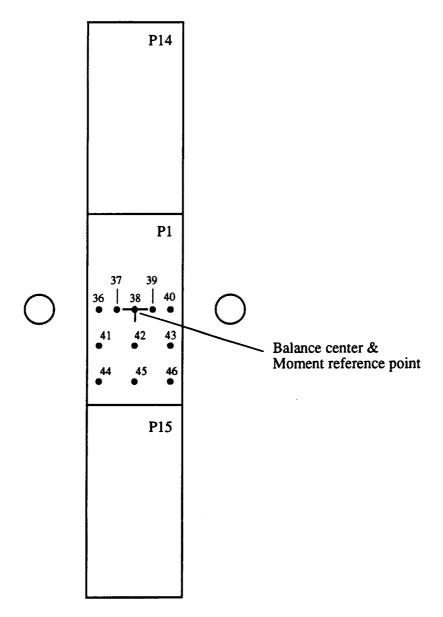


Figure 56. Configuration 2C\_8\_0\_4/24;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_8\_0\_4/24

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3	5.25	0
46	-1.5	3	4.375	-1.5

	Config	Jet-In Configuration: 2C-8-0-4/24	Jet-Indu -8-0-4/24	ced Pressu	Jet-Induced Pressure Increments 0-4/24 Run 19	ements Run 197		
	Point	7	ď	•	~	ю	9	7
	h/De =	8.85	5.87	4.68	3.52	2.36	1.76	1.17
Total	Total Thrust =		52.27	52.19	52.11	52.11	52.13	52.11
NPR	Front =		2.04	2.04	2.04	2.04	2.04	2 0 4
MPR	Aft =	2.01	2.01	2.01	2.01	2.01	2.01	2.01
X-10c	Y-loc		₽ÇĐ	Ş.	βÇ	QQ Q	₽	₽CD
1.50	0.00		0.000845	0.000796	0.000065	-0.006318	-0.022618	-0.046229
0.75	0.0		0.001321	0.003170	0.004754	0.012673		-0.01335
00.0	0.00	0.000392	0.000929	0.003353	0.008172	0.026910	0.043202	0.063914
-0.75	0.0	0.000298	0.001724	0.002816	0.006009	0.017387	0.019110	-0.002576
-1.50	0.0	Ť	0.000745	0.001125	0.001694	-0.003039	-0.018895	-0.047367
1.50	1.50	•	0.000899	0.001139	0.001056	-0.006941	-0.021612	-0.047601
0.00	1.50		0.001406	0.002831	0.007524	0.024853	0.041796	0.064444
-1.50	1.50	•	0.000626	0.000164	0.000334	-0.004983	-0.021403	-0.046255
1.50	3.00		0.000223	0.001179	0.001081	-0.005102	-0.019416	-0.042705
0.00	3.00	'	0.000705	0.003268	0.006767	0.022049	0.037136	0.056743
-1.50	3.00	-0.000511	-0.000134	0.000229	-0.000384	-0.008142	-0.020857	-0.041116
Force and	1 Moment	Summery						
	h/De	± 8.85	5.87	4.68	3.52	2.36	1.76	
Balance	<u> </u>	-0.005	0.010	0.016	0.028	0.067	0.044	-0.082
Pressure	<b>A</b> L/1	-0.001	0.005	0.012	0.022	0.039	0.015	
Balance		. 0.101	0.081	0.077	0.087	0.054	0.054	
Pressure		≥ 0.000	000.0	0.001	0.001	-0.000	-0.001	

	Configu	Jet-Induced Pressure Increments Configuration: 2C-8-0-4/24	Jet-Indu 8-0-4/24	ced Pressu	re Increme	ints 1 198A	
	Po (a)	-	~	~	7	ın	٠
	1	8.84	8	17.7	3.54	2.34	1.76
10101	1		135.94	136.50	136.58	136.64	136.60
	Property of		3.06	85			6
202	1		7	7	00.4	4.00	90.4
X-loc Y-loc	Y-10c	ð	ΦCD	Q	Q.	₽	₽
1.50	00.00	-0.000101	0.000246	0.000871	0.000523	-0.001908	-0.020204
75	00	-0 000005	ı	0.002713	0.004107	0.013173	0.014829
00	00.0	-0.000013		0.002547	0.006075	0.024946	
-0.75	00.0	-0.000329		0.001541	0.005200	0.015752	
-1.50	00.0	0.000185	0.000122	0.000304	0.000578	0.000110	•
1.50	1.50	-0.000335		0.000748	0.000392	-0.001720	-0.020055
00.0	1.50	-0.000181	0.000988	0.001959	0.004336	0.023757	0.050034
-1.50	1.50	-0.000051		0.000251	0.000766	-0.003206	-0.020234
1.50	3.00	-0.000369	-0.000621	0.000015	-0.000837	-0.004335	-0.019005
00.00	3.00	000181	-0.000225	0.001200	0.003196	0.018397	0.043211
-1.50	3.00	-0.000369	-0.000260	0.000354	0.000015	-0.004609	-0.019214
Force and	Moment	Moment Summary					
	h/De	8.8	5.88	4.71	3.54		1.76
Balance	AL/T	-0.005	0.00	900.0	0.014		0.070
Pressure	AL/T	-0.001	0.001	0.007	0.012	0.045	0.038
Balance	AM/TDe	0.024	0.018	0.018	0.012		0.004
Dragging AN/The	AW/The	000 0-	000	0000	-0.001		-0.000

Increments Run 198B	10	5.89	221.93	5.94	5.95	₽ÇЪ	0.000050	.001247	. 000668	0.000735	-0.000252	.000401	0.001597	.000124	.000488	.000170	.000357		5.89	-0.001	0.001	0.012	-0.000
Jet-Induced Pressure Increments 0-4/24 Run 19	Φ.	4.70	222.04	5.95	5.95	<b>₽</b> CÞ	0.0000777 0	0.001884 0		.002389		.000526	.002211		.00000	.001727	.000267		4.70	0.010	0.007	800.0	0.000
Jet - Indu 8-0-4/24	•	3.52	222.10	5.95	5.95	₽Çb	0.002236	0.007125	0.008644	0.005833	0.001997	0.002383	0.008440	0.001672	0.000493				3.52	0.032	0.026	0.001	0.001
Jet-In Configuration: 2C-8-0-4/24	7	2.34	222.10	5.95	5.95	₽Ç	-0.002917	0.017576	0.032142	0.017140	-0.002868	-0.004178	0.035279	-0.004127	-0.005186	0.029901	-0.004492	Summarry	2.34	0.118	0.069	-0.001	-0.001
Configu	Point	h/De =	Thrust =	ь,	<	Y~10c	0.00	0.0	0.0	0.0	0.0	1.50	1.50	1.50	3.00	3.00	3.00	Moment	h/De =	AL/T =	AL/T =		AM/TDe =
			Tote]	MPR MPR	MPR	X-10c	1.50	0.75	0.00	-0.75	-1.50	1.50	0.00	-1.50	1.50	0.00	-1.50	Force and		Balance	Pressure	Balance	Pressure

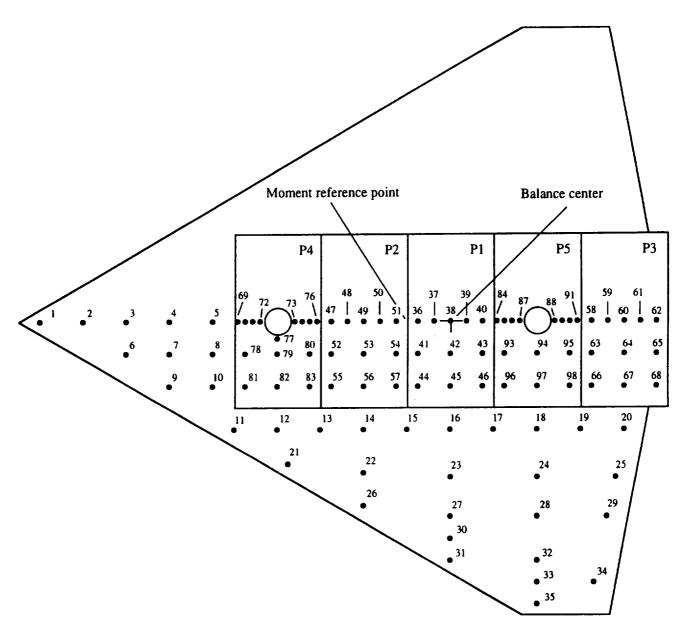


Figure 57. Configuration 2C\_12\_0\_DW;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_12\_0\_DW

Orif.#	Mom. arm	Sto. v	Δ.Area	Sto. v
1	16.6	Sta. y 0	2.3	Sta. x 17
2	14.86	0	6.918	15
2	13	0	0.710	13
3	11	0	3	11
4	11	0	2	
5	9	1.5	3 3 3 8.546	9
0	13	1.5	8.340	13
2 3 4 5 6 7 8 9	11 9 10.87 9 8.14	1.5	6 6	11
8	10.07	1.5	0	9
9	10.87	3	7.166	11
10	9	3	7 8.91	9 8
11	8.14	2	8.91	8
12	6	5	8	6
13	4	5	8	4
14	2	5	8	2
15	0	5	8	0
16	6 4 2 0 -2 -4 -6 -8	5	8 8 8 8 8 8	6 4 2 0 -2 -4
17	-4	5	8	-4
18	-6	5	8	-6 -8
19	-8	1.5 3 3 5 5 5 5 5 5 5 7 7 7 7 7 8.5	8	-8
20	-9.91	5	8.06 7.302	-10
21	5.06	6.6	7.302	5.5
22	2	7	16	2
23	2 -2 -6	7	16	-2
24	-6	7	16	-6
25	-9.31	7	10.484	-9.6
26	1.235	8.5	9.904	2
27	-2	9	12	-2
28	-2 -6	9	16	-6
29	-9.11	9	8.908	-9.2
30	-2	9 9 9 10	8	-2
31	-2.84	11	8.376	-2
32	-6	11	12	-6
33	-6 -6	12	12 8	-6
34	-8.86	12	12.005	5.5 2 -2 -6 -9.6 2 -2 -6 -9.2 -2 -6 -6 -8.6
35	-6.17	13	6.883	-6
69	7.85	0	0.634	-6 7.85
70	7.5	Ŏ	0.683	7.5
71	7.15	Ö	0.683	7.15
72	6.8	ŏ	0.619	6.8
73	5.2	ŏ	0.619	5.2
74 74	4.85	ŏ	0.683	4.85
75	4.5	ŏ	0.683	4.5
76	4.15	ŏ	0.634	4.15
70 77	6	0.8	1.238	6
77 78	7.5	1.5	3.19	7.5
78 <b>7</b> 9		1.5	3.825	
19	6	1.3	3.823	6

Conf. # 2C\_12\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
80	4.5	1.5	3.19	4.5
81	7.5	3 3 3 0	4.375	7.5
82	6	3	5.25	6
83	4.5	3	4.375	4.5
47	3.5		1.313	3.5
48 49	2.75 2	0	1.125	2.75
50	1.25	0 0	1.125 1.125	2.75 2 1.25
51	0.5	0	1.123	0.5
52	3.5	1.5	3.75	3.5
53	3.5 2	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5	3	4.375	3.5
56	2	1.5 3 3 3 0	5.25	2
57	0.5	3	4.375	0.5
36	-0.5	0	1.313	-0.5
37	-1.25	0	1.125	-1.25
38	-2	0	1.125	-2
39	-2.75	0	1.125	-2.75
40	-3.5	0	1.313	-3.5
41	-0.5	1.5	3.75	-0.5
42	-2	1.5	4.5	-2
43	-3.5	1.5	3.75	-3.5
44 45	-0.5 -2	3 3 3 0	4.375	-0.5
43 46	-3.5	3	5.25 4.375	-2 -3.5
<del>4</del> 0 84	-3.3 -4.15	0	0.634	-3.3 -4.15
85	-4.5	Ŏ	0.683	-4.1 <i>5</i>
86	-4.85	ŏ	0.683	-4.85
87	-5.2	Ŏ	0.619	-5.2
88	-6.8	Ö	0.619	-6.8
89	-7.15	0	0.683	-7.15
90	-7.5	0	0.683	-7.5
91	-7.85	0	0.634	-7.85
93	-4.5	1.5	3.19	-4.5
94	-6	1.5	5.062	-6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3 3 3 0	4.375	-4.5
97	-6	3	5.25	-6
98 50	-7.5 8.5	3	4.375	-7.5
58 50	-8.5 0.25	Ü	1.313	-8.5
59 60	-9.25	0 0	1.125	-9.25
61	-10 -10.75	0	1.125 1.125	-10 -10.75
62	-11.5	0	1.313	-10.73
63	-8.5	1.5	3.75	-8.5
64	-10	1.5	4.5	-10
65	-11.5	1.5	3.75	-11.5
66	-8.5		4.375	-8.5
67	-10	3 3 3	5.25	-10
68	-11.5	3	4.375	-11.5

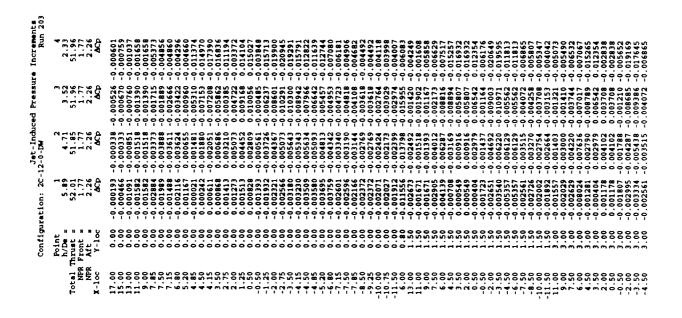
	1.75 52.59 2.08 1.99 ACP	-0.009913 -0.009913 -0.005913 -0.005913 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782 -0.00782	
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	Total T NPR NPR X-loc	7.50 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10 1.10
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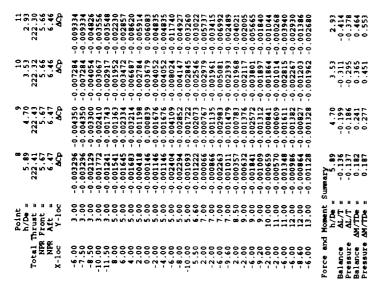
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Jet-Induced Pressure: 2C-12-0-DM	17.67 11.80 8.86 5.90 4.73 3.54 2.22 2.22 2.22 2.22 2.22 2.22 2.22 2	0.000101

5.90 5.20 2.18 2.18 2.18 2.18 2.18 2.18 ACP 

2.33 51.96 1.77 2.26 ACP	<b>プラきちゅうアフラ目のアウシニゅうちのファルチグラクルアクラウものアファブログログラウンファブログログラグアファログログラグアファログログラグラグラグラグラグラグラグラグラグラグラグラグラグラグラグラグラグラ</b>	2.33 -0.582 -0.617 0.517
3.52 51.96 1.77 2.26 ACP	148880901954548898964949019444	3.52 -0.340 -0.338 0.424 0.496
4.71 51.85 1.77 2.26 ACP		4.71 -0.231 -0.235 0.303
5.89 52.01 1.77 2.26 ACP	440000000000000000000000000000000000000	5.89 -0.165 -0.189 0.237 0.232
Point h/De = Thrust = Front = Aft = Y-loc	## 1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000   1000	h/De = AL/T = AL/T = AM/TDe =
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Jet-Induced -12-0-DW	7	7.	•	1.3	٥.	Ą	8000	0.000	0.0000	0.0011	0.00111	0.0011	0.00099	0.00170	0.0021	0.0025	0.00416	0.00484	0.00511	0.00467	0.00298	0.00099	00182	00444	.00461	.003275	0.000461	0.002765	0.005099	0.006467	0.005931	0.004484	0.002671	1140000	0.003334	0.003840	002716	0.002716	0.002631	0.002131	0.002111	0.005333	0.001039	0.000093	20000	0.003452	0.004782	3.004549	0.004549	9600	004336	00.00262	0.014038	0.014038	0.003904	0.002661	0.002671	0.002280	0.00100.0	001208	0.001155	0.004727	103600	0.001219	0.001219	0.003474	0.00173	0.004841	0.00390
ration: 20	1	5.8	52.45	3	۰.	<b>Q</b> C	.000	0.0007	0.0007	0.00085	0.00085	0.00103	0.00085	0.00127	0.00182	0.00206	0.00308	0.00344	0.00416	0.00316	0.00180	0.00074	96000	.00324	00298	.00282	0.00030	0.00066	0.00337	0.00359	0.00382	0.00348	0.001		0000	0.00353	00276	0.00276	0.00196	0.00160	0.00143	0.00547				0.00326	0.00345	0.00300	0.00300	00167	8/700	00000	01097	0.01097	0.00371	0.00321	0.00200	77100.0	20100	7000	00000	00360	00167	0.00094	0000	0.00248	00010	-0.002644	00371
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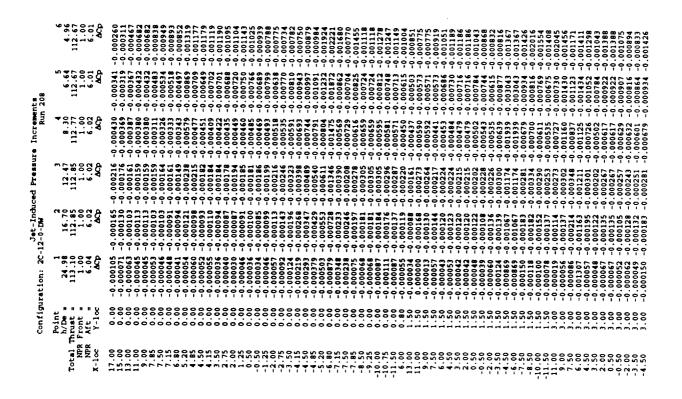


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Jet-Induced Pressure Inc: -12-0-DW	25.05 16.68 21.46 8.37 6.69 5.03 25.73 25.67 25.65 25.00 25.58 25.57 2 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.	0000070 -0.000136 -0.000146 -0.000377 -0.000567 -0.000187 -0.000056 -0.000186 -0.000187 -0.000367 -0.000186 -0.000186 -0.000312 -0.000499 -0.000817 -0.000186 -0.000186 -0.000312 -0.000499 -0.000817 -0.000186 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.000187 -0.00018	\$5

4.97 67.44 1.00 3.92 ACP	0.001346 0.001346 0.001346 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340 0.001340	4.97 -0.309 -0.312 0.394 0.599
6.66 67.55 1.00 3.93 ACP		6.66 -0.193 -0.191 0.081 0.271
8.30 67.59 1.00 3.93 ACP	0.000522 0.0007222 0.0007224 0.0008534 0.0008534 0.0008534 0.0008536 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0.0008526 0	8.30 -0.133 -0.137 -0.011 0.137
12.47 67.79 1.00 3.94 ACP	0.000099	12.47 -0.059 -0.039 -0.094 0.080
16.67 67.95 1.00 3.95 ACP	0.000183 0.000183 0.000182 0.000182 0.000182 0.000182 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.000183 0.0001	16.67 -0.035 -0.031 -0.098 0.069
25.05 68.18 1.00 3.96 ACD	0.000188	Summary 25.05 = 0.020 = 0.021 = 0.020
Point h/De = Thrust = Front = Aft = Y-loc		Moment N/De AL/T AK/TDe
Total NPR NPR NPR X-loc		Force and Balance Pressure Balance Pressure



4.96 112.67 1.00 6.01	-0.001190 -0.001190 -0.001455 -0.001456 -0.001431 -0.001101 -0.001108	0.00112 0.00112 0.00107 0.00106 0.00139 0.00107	0.00136 0.00084 0.00105 0.00143 0.00143 0.00170 0.00170	4.96 -0.272 -0.279 0.321
6.64 112.67 1.00 6.01 ACP	000755 000136 00184 000698 001168 001329 001226 001226	0.000777 0.000846 0.000997 0.001120 0.001055 0.000949	0000000000	6.64 -0.181 -0.186 0.085 0.215
8.30 112.77 1.00 6.02 ACP	.000641 .000641 .000674 .000587 .000948 .001092 .0010884 .00008884	0.000745 0.000765 0.000628 0.000825 0.000841 0.000822	0.0007 0.0007 0.0007 0.0006 0.0006 0.0006	8.30 -0.125 -0.144 0.013
112.47 112.85 1.00 6.02 ACP	000288 000228 000229 000297 000397 00309	000288 000283 000275 000269 000269 000273 000273	0.000257 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 - 0.000258 -	12.47 -0.056 -0.058 -0.048 0.053
16.70 112.85 1.00 6.02 ACP	0000000000	00015 00015 00015 00015 00015 00016 00015	71111111111	16.70 -0.033 -0.035 -0.066 0.034
24.98 113.10 1.00 6.04 ACP	0.000069 - 0.00069 - 0.000069 - 0.000066 - 0.00066 - 0.00066 - 0.00066 - 0.000066 - 0.000013 - 0.00013 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.0000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.0000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.0000000000000000000000000000000000	0.000093 - 0.000093 - 0.000093 - 0.000093 - 0.000993 - 0.000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.0000993 - 0.00000993 - 0.00000993	0.000057 0.0000573 0.0000573 0.0000681 0.0000683 0.0000683 0.0000683 0.0000684	'ummary 24.98 24.98 -0.019 -0.021 -0.080 0.025
Point h/De = Thrust = Front = Aft = Y-loc	•••••	888888888	80.00 0.00 0.00 0.01 0.00 0.00 0.00 0.00	Moment S h/De = AL/T = AL/T = M/TDe = M/TDe =
Total 1 NPR NPR X-loc	AL 00-100-4400	0000000000	444444466	Force and Balance Pressure Balance /



	2.32 52.06 2.01 2.00 ACP	0.000000000000000000000000000000000000
	3.52 52.12 2.01 2.01 ACP	0.008324 0.008324 0.008324 0.0083267 0.0083267 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.00832824 0.
	4.69 52.12 2.01 2.01 ACP	0.000000000000000000000000000000000000
	3.52 3.52 52.18 2.01 2.01 ACP	0.000000000000000000000000000000000000
	8.84 52.20 2.02 2.01 ACP	0.000000000000000000000000000000000000
	3 17.68 52.12 2.01 2.01	0.000000000000000000000000000000000000
	2.11.81 52.18 2.02 2.01 2.01	0.000012 0.000012 0.000012 0.000012 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.0000
	17.64 51.92 2.00 2.01 ACP	10.000256 10.000256 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.0002576 10.00025
	Point h/De = Thrust = R Front = R Aft = Y-loc	3 000 000 000 000 000 000 000 000 000 0
	Total T NPR NPR X-loc	8 1 5 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6
	2.32 2.06 2.01 2.00 ACP	0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238 0.001238
	3.52 52.12 2.01 2.01 AC	0.00010138800000000000000000000000000000
	22.12 22.12 2.01 2.01 ACD	0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.000951 0.0
1t. 209	3.52 52.18 2.01 2.01 ACP	0.00009454
e Increments Run 209	52.20 2.02 2.02 2.03 AC	0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344 0.0000344
ced Pressure	17.68 52.12 2.01 2.01 ACP	0.000000000000000000000000000000000000
Jet-Induced 2C-12-0-DW	11.81 52.18 2.02 2.01 2.01	
	17.64 51.92 2.00 2.01 ACP	10000000000000000000000000000000000000
Configuration:	Point h/De = Thrust = r Front = r Aft = r-loc	
	Total T NPR NPR X-loc	######################################

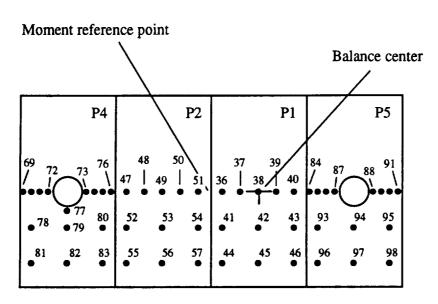


Figure 58. Configuration 2C\_12\_0\_16/8;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_12\_0\_16/8

69       7.85       0       0.634       7.85         70       7.5       0       0.683       7.5         71       7.15       0       0.683       7.15         72       6.8       0       0.619       6.8         73       5.2       0       0.619       5.2         74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       7.5         84       2.75       0       1.313       3.5         47       3.5       0       1.313       3.5         49       2       0       1.125       2.5	Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
70       7.5       0       0.683       7.5         71       7.15       0       0.683       7.15         72       6.8       0       0.619       6.8         73       5.2       0       0.619       5.2         74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.5         51       0.5       0       1.313       0.5					
71       7.15       0       0.683       7.15         72       6.8       0       0.619       6.8         73       5.2       0       0.619       5.2         74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.5         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5					
72       6.8       0       0.619       6.8         73       5.2       0       0.619       5.2         74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         49       2       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5					
73       5.2       0       0.619       5.2         74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         49       2       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2 <t< td=""><td></td><td>6.8</td><td></td><td></td><td></td></t<>		6.8			
74       4.85       0       0.683       4.85         75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         50       1.25       0       1.313       0.5         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5    <		5.2			5.2
75       4.5       0       0.683       4.5         76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         50       1.25       0       1.313       0.5         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5					
76       4.15       0       0.634       4.15         77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         50       1.25       0       1.313       0.5         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5		4.63	ñ		
77       6       0.8       1.238       6         78       7.5       1.5       3.19       7.5         79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.313       0.5         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5					4.15
79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5		4.13			6
79       6       1.5       3.825       6         80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5		7.5		2.10	7.5
80       4.5       1.5       3.19       4.5         81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5			1.5	2.17	1.5
81       7.5       3       4.375       7.5         82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5			1.5		4.5
82       6       3       5.25       6         83       4.5       3       4.375       4.5         47       3.5       0       1.313       3.5         48       2.75       0       1.125       2.75         49       2       0       1.125       2         50       1.25       0       1.125       1.25         51       0.5       0       1.313       0.5         52       3.5       1.5       3.75       3.5         53       2       1.5       4.5       2         54       0.5       1.5       3.75       0.5			1.5		4.5
48     2.75     0     1.125     2.75       49     2     0     1.125     2       50     1.25     0     1.125     1.25       51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5			3	4.373	1.5
48     2.75     0     1.125     2.75       49     2     0     1.125     2       50     1.25     0     1.125     1.25       51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		6	3	5.25	6
48     2.75     0     1.125     2.75       49     2     0     1.125     2       50     1.25     0     1.125     1.25       51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		4.5	3		
50     1.25     0     1.125     1.25       51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		3.5		1.313	3.5
50     1.25     0     1.125     1.25       51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		2.75			2.75
51     0.5     0     1.313     0.5       52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		2	0		2
52     3.5     1.5     3.75     3.5       53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5		1.25	0		1.25
53 2 1.5 4.5 2 54 0.5 1.5 3.75 0.5		0.5			
53     2     1.5     4.5     2       54     0.5     1.5     3.75     0.5       55     3.5     3     4.375     3.5       56     2     3     5.25     2		3.5	1.5	3.75	3.5
54     0.5     1.5     3.75     0.5       55     3.5     3     4.375     3.5       56     2     3     5.25     2	53	2	1.5	4.5	
55     3.5     3     4.375     3.5       56     2     3     5.25     2	54	0.5	1.5	3.75	
56 2 3 5.25 2	55	3.5	3	4.375	3.5
	56	2	3	5.25	2
57 0.5 3 4.375 0.5		0.5	3	4.375	0.5
36 -0.5 0 1.313 -0.5		-0.5	0	1.313	-0.5
37 -1.25 0 1.125 -1.25				1.125	-1.25
38 -2 0 1.125 -2					-2
39 -2.75 0 1.125 -2.75					-2.75
40 -3.5 0 1.313 -3.5				1 313	
41 -0.5 1.5 3.75 -0.5				3.75	-0.5
42 -2 1.5 4.5 -2		-2			-2
43 -3.5 1.5 3.75 -3.5			1.5		-3 5
44 -0.5 3 4.375 -0.5			3		
44 -0.5 3 4.375 -0.5 45 -2 3 5.25 -2		20.5	3		
		2 5	2		2 5
			0		
85 -4.5 0 0.683 -4.5					
86 -4.85 0 0.683 -4.85					
87 -5.2 0 0.619 -5.2					
88 -6.8 0 0.619 -6.8		-6.8			
89 -7.15 0 0.683 -7.15					
90 -7.5 0 0.683 -7.5					
91 -7.85 0 0.634 -7.85					
93 -4.5 1.5 3.19 -4.5	93	-4.5	1.5	3.19	-4.5

Conf. # 2C\_12\_0\_16/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
94	-6	1.5	5.062	-6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3	4.375	-4.5
97	-6	3	5.25	-6
98	-7.5	3	4.375	-7.5

	~	٠.	•	? •	٠;	J.	324	306	0338	0456	0479	0984	1287	1370	1461	1366	97.0		17.	0568	0675	1249	1319	1366	121	0000	0000	0349	0303	931	1160	071	1341	2	775	200	9068	140	125	200	0033	9060	200	0142	008	0115	000	0112	700	.006463	~	138	: 🖺	2
							ò	ę	ç	q	o	ę	ę	ė,	ė,	ė	ė,			0	ė.	ė	o P	ė.	ė,	۹	9	Ģ	ę	ę.	ڄڄ	ė	ę	o.	o c	•	ę	o	o o	9	9	9	ę,	0 0	9	0	0	9 9	,	٩				
•	4	3	•	? •	50.7	9	0.00227	0.00278	00000	0 00412	0.00278	0.00630	0.00753	0.00880	0.00819	0.00625	0.00151	200	200	00470	0.00167	0.00555	0.00863	0.00894	0.00821	0.00612	0003	0.00353	000	0.0008	0.01446	0.0066	0.0084	0.0083	0.0083(		0.0017	0.0083	0117	7110.0	0.0028	0.0065	0.0068	0.0072	000	0.0073	0.0021	0.0064	0.0023	-0.004259	ď		9	3
•	4 73		24.34	70.7	2.03	d Sc	0.9100 0	0 001979	000517	000000	0 001934	0.004050	0.005085	0.005781	0.004626	0.00294	0.000064	77500		00315	001305	0.003199	0.004744	0.005058	0.004744	0.004116	0.001604	0.002492	001992	0.001330	0.012109	0.002032	0.005576	0.005142	0.005142	9000		0.0045	0110	0110	0024	0.0077	0.0042	0.0056		0035	9000	903	0020	-0.003773	٢		2	5
•	•		?	٠.	2.03	<b>6</b>	000752	001447	1733	79000	01210	198C00	003726	003097	002854	00110	000499	00147		00281	00119	0.000930	0.002506	0.002672	0.003138	0.002927	0.001464	0.00366	0.001278	0.000568	0.009168	0.001219	0.003555	0.002388	0.002388		000	0.002066	0.008671	0.008671	0.001943	0.006278	0.003101	.003367	000	0032	0.0003	0.0020	0.0014	0.002716	•	'n.	3 2	5
~	•		7	٥.	2.01	Q Q	- 179000	000760	99600	446.00	100101	100.00	001483	0.000604	- 568000.0	000378 -	0.000129	001010	00100	001000	000110	0.000572	088000	0.001045 -	0.001188 -	0.001571	0.002134	001/40	000522	0.000512	0.004841	0.000714	0.001297	0.000438	0.000438	07.6000	000572	0.000974	.005247	0.005247	7.0000	0.006067	0.001284	.000970	00000	000448	.000398	.000632	.000870	-0.001288	•	∞,	7:	70.0
Doint					Aft =		5	2 6	38	38	38	38	3 2	28	00	8	8	•	0 4	<b>&gt;</b> <	, c		0	0	0	0	0 0	9 0	, 0		ш,	31 W			•	•:•	•••	:-:	-:	<b>-:</b> :	•:•			٦.	٠, ٠	•		٠.	٦.	8.6	Moment		- t	
			Total T	Z Z	Ē	X-10c		в ы	n ,	→ 1				7 -		,,,	•				: .			3		3	٠; ·			::	9	•••	-		-		-: -		-	٠	٠,								•	9.9	Force and	,	200	ressure

	2.33 136.70 3.95 ACP	00000000000000000000000000000000000000	0.031 0.027
crement: Run 2	5.52 6.73 3.98 5.98	1218 8 24 25 11 10 5 25 0 4 20 4 20 12 12 12 12 12 12 12 12 12 12 12 12 12	976
ssure Inc	E	0.000000000000000000000000000000000000	
Induced Press	4.70 136.74 3.95 3.98 ACP	0.000	0.015
Jet-Ind 12-0-16/8	5.90 136.88 3.95 3.98 A.Op	0.000000000000000000000000000000000000	0.019
guration: 2C-	8.85 137.10 3.97 3.98 ACD		0.018
Configu	Point h/De = Thrust = Front = Aft = Y-loc	MA WAS A CONTRACT OF THE PROPERTY OF THE PROPE	AW/170
	Total NPR NPR	8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Pressure Balance Pressure

nts _ 212	2.32 226.33 2.95 6.02 ACP	A PARAMENTA OF THE PROPERTY OF THE PARAMENT OF	-0.101 -0.086 0.041 0.035
re Increment	3.52 226.30 5.95 6.02 ACP		-0.064 -0.064 0.005
ced Pressure	4.70 226.45 5.95 6.03 ACP		-0.043 -0.046 0.012
Jet-Induced 12-0-16/8	5.95 6.03 ACD	2004/3004/3004/3004/3004/3004/3004/3004/	-0.030 -0.036 0.012
Ŕ	8.85 226.26 5.95 6.03 ACP	NEWS COMMENSOR OF THE COMENSOR OF THE COMMENSOR OF THE CO	0.016 0.021 0.008
Configuration:	Point h/De = Thrust = r Front = r Aft = r-loc	Month of the control	AE/T7 AE/T76 100 100 100 100 100 100 100 100 100 100
	Total T NPR NPR X-loc	7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7. 7	Balance Pressure Balance Pressure

## Moment reference point

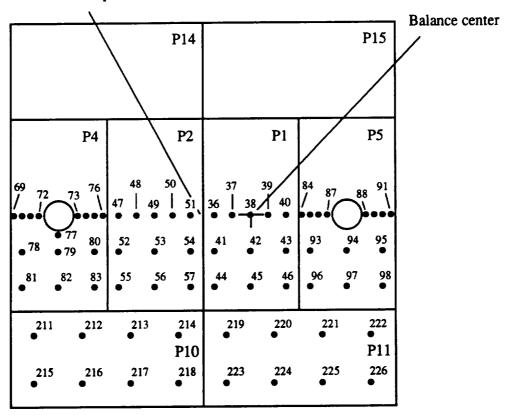


Figure 59. Configuration 2C\_12\_0\_16/16;  $D_{\theta} = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

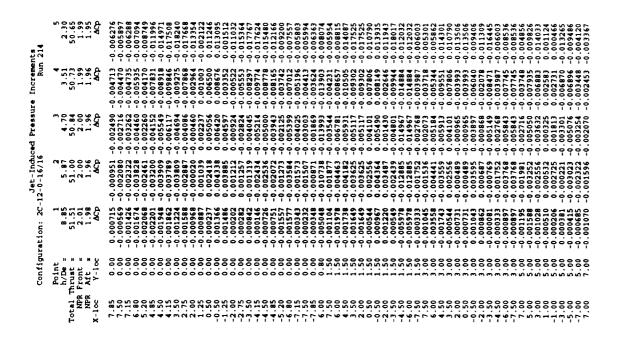
### Conf. # 2C\_12\_0\_16/16

O * C * #		_		_
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
69	7.85	0	0.634	7.85
70	7.5	0	0.683	7.5
71	7.15	0	0.683	7.15
72	6.8	0	0.619	6.8
73	5.2	0	0.619	5.2
74	4.85	0	0.683	4.85
75	4.5	Ō	0.683	4.5
76	4.15	Ŏ	0.634	4.15
77	6	0.8	1.238	6
<del>7</del> 8	7.5	1.5	3.19	7.5
79	6	1.5	3.825	6
80	4.5	1.5	3.19	4.5
81	7.5	1.5 3 3 3 0	4.375	7.5
82	6	3	4.373 5.35	
83		3	5.25	6
0.3	4.5	3	4.375	4.5
47	3.5	0	1.313	3.5
48	2.75	0	1.125	2.75 2
49	2	0	1.125	2
50	1.25	0	1.125	1.25
51	0.5	0	1.313	0.5
52	3.5	1.5	3.75	3.5
53	2	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5	3 3 3 0	4.375	3.5
56	2	3	5.25	2
57	0.5	3	4.375	0.5
36	-0.5	Õ	1.313	-0.5
37	-1.25	Ŏ	1.125	-1.25
38	-2	ŏ	1.125	-2
39	-2.75	ŏ	1.125	-2.75
40	-3.5	ŏ	1.313	-3.5
41	-0.5	1.5	3.75	-3.3 0.5
42	-0.5 -2	1.5	4.5	-0.5 -2
43	-3.5			-Z
		1.5	3.75	-3.5
44	-0.5	3 3	4.375	-0.5
45	-2		5.25	-2
46	-3.5	3 0	4.375	-3.5
84	-4.15	0	0.634	-4.15
85	-4.5	0	0.683	-4.5
86	-4.85	0	0.683	-4.85
87	-5.2	0	0.619	-5.2
88	-6.8	0	0.619	-6.8
89	-7.15	0	0.683	-7.15
90	-7.5	0	0.683	-7.5
91	-7.85	0	0.634	-7.85
93	-4.5	1.5	3.19	-4.5
	_		= - = -	•••

Conf. # 2C\_12\_0\_16/16, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
94	-6	1.5	5.062	-6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3	4.375	-4.5
97	-6	3	5.25	-6
98	-7.5	3	4.375	-7.5
211	7	5	8	7
212		5	8	5
213	5 3	3 3 5 5 5 5	8	5 3
214	1	5	8	1
215	7	7	8	7
216	5	7	8	5 3
217	3	7	8	3
218	1	7	8	1
219	-1	5	8	-1
220	-3	5	8	-3
221	-5	5	8	-5
222	-7	5	8	-7
223	-1	7	8	-1
224	-3	7	8	-3
225	-5	7	8	-5
226	-7	7	8	-7

	Point h/De =	8.85	5.87	4.70	3.51	2.30
Total T		51.51	51.00		50.73	
NPR	Aft =	1.98	1.96		1.96	
X-10c	Y-10c	ФСР	ΦCÞ		ďζ	
9.00	7.00	-0.001323	-0.002305	-0.003453	9	-0.005652
3.00	7.00	-0.001499	-0.001047	-0.002898	Ŷ	-0.009317
1.00	7.00	-0.000364	0.000476	0.000078	0	-0.000183
-1.00	7.00	0.00000.0	0.001072	0.000664	0.000770	0.002086
-3.00	7.00	0.000163	-0.000619	-0.001783	Ŷ	-0.008336
-5.00	7.00	0.000021	-0.002115	-0.003132	9	-0.005475
-7.00	7.00	-0.000343	-0.001349	-0.001996	٥	-0.002953
Force and	Moment	Summary				
	h/De a	8.85	5.87	4.70	3.51	2.30
Balance	ΔL/T =	-0.034	-0.077	-0.132	-0.222	-0.388
Pressure	ΔL/T =	-0.046	-0.085	-0.149	-0.220	-0.372
Balance	AM/TDe =	-0.039	0.004	0.014	0.046	0.070
Pressure	AM/TDe =	-0.046	0.018	0.052	0.049	0.031



e Increments Run 215		'n۲		٠.	8	0.00127	0.00205	00349	0.00138	0.00067	0.00137	28100.	0.00056	.00214	.00398	86500.	0000	0.00102	0.00162	86700.0	00311	0.00282	0.00120	0.00325	16100.0	.00160	0.01115	0.00203	0.00264	0.00050	0.00050	.00177	0.00132	.00288	0.00867	0.00156	0.00172	0.00433 0.00287	0.00288	.00127	7100	0.00153	0.00286	0.00156	00298	0.00200	0.00248	0.00083	0.00018	0.00201	0.00321	-0.001925 -0.001383	
ced Pressure		٦,		٠,	8	0.001825	0.002720	858700	0.001082	0.001508	0.003017	675753	0.000632	.00341	.00561	.00558	.00126	0.001853	0.003115	0.004957	004914	0.003571	0.001832	0.004395	0.003039	.002447	0.017281	0.002954	0.004825	0.003089	0.003089	0.00000	0.002202	.005189	0.011129	0.002512	0.002653	0.004478	0.006053	.00180	.00180	0.001972	0.004435	0.002512	004382	0.003430	0.004957	0.002598	0.002301	0.004041	0.004259	-0.002416	
Jet-Indu -12-0-16/16		ų a		Ö	₹.	0.00377	.00465	70000	0.00015	0.00468	0.00626	.00974	0.00346	0.00105	.00723	.00800.	0.00128	0.00418	0.00669	0.00781	0.00883	0.00596	0.00344	0.00510	0.00419	.00356	0.01768	0.00410	90600.0	0.00694	0.00694	00452	0.00497	.00827	70600.0	0.00344	0.00367	0.00451	0.00616	.00036	. 00036	0.00531	0.00865	0.00344	00537	0.00364	0.00755	0.00553	0.0021	.00646	0.00631	-0.002814	
ration: 2C		٠.	9 0	•	¥	0.00541	0.00475	100000	0.00400	0.00933	0.01456	.01633	0.01441	0.00773	.00511	.01552	77100.0	0.01027	0.01452	0.01514	0.01434	0.00836	0.00463	0.00550	0.00525	.00498	0.01189	0.00551	0.00938	0.01691	0.01691	01329	0.01195	0.01484	0.00751	0.00514	0.00494	0.00358	0.01329	.00708	0.00708	0.01276	0.01408	0.00514	00621	0.00452	0.01084	0.01212	0.005/1	0.01142	0.00712	-0.003644	
Configu	Point	2 1	-	Aft	Y-10	ĕ	ō, c	ة ج	Ò	Ö	ē	ē	9	Ö	٠	ه ه	Õ	•	•	٠, ٥	• •	9	•	ō,	90	9	•	'n	نەن	ini	٦ċ٠	ٺم	ir.	ĸ	بن	į	۰.	9.0	? 0	0,1	9.0	. •	۰	0,0	? =	٠.	۰,	۰,	? •	۰.	٥,	2.00 7.00	
		i de la constante de la consta	Ž	N. N.	X-10c	•	'n.	- •	9 19		ŝ	ન •	٦.	۰.	ď	9	2.5	2	7	~ 	Ξ,	-	2.5	9.	7.1	, 00	9	٠į٠	ی د	j	۰,		٠.	5.5	4.0	: .	ζ.	o, v	9	9	0.0		.5	A. (	<u> </u>	::	٩	۰,			۰,	7.00	

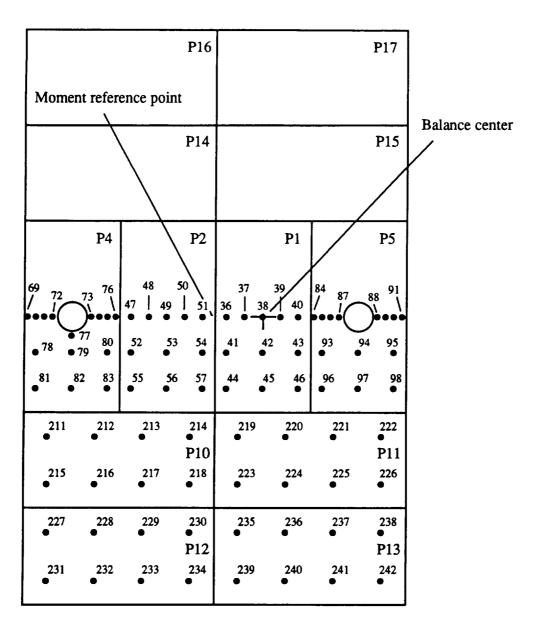


Figure 60. Configuration 2C\_12\_0\_16/24;  $D_{\Theta} = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

## Conf. # 2C\_12\_0\_16/24

0.10.11		0.		α.
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
69	7.85 7.5	0 0	0.634 0.683	7.85 7.5
70 71	7.3 7.15	0	0.683	7.3 7.15
72	6.8	0	0.619	6.8
73	5.2	Ŏ	0.619	5.2
73 74	4.85	Ŏ	0.683	4.85
75	4.5	Ŏ	0.683	4.5
76 76	4.15	ŏ	0.634	4.15
77	6	<b>0</b> .8	1.238	6
<b>78</b>	<b>7</b> .5	1.5	3.19	7.5
79	6	1.5	3.825	6
80	4.5	1.5	3.19	4.5
81	7.5		4.375	7.5
82	6	3 3 3	5.25	6
83	4.5	3	4.375	4.5
47	3.5	0	1.313	3.5
48	2.75	0	1.125	2.75
49	2	0	1.125	2
50	1.25	0	1.125	1.25
51	0.5	0	1.313	0.5
52	3.5	1.5	3.75	3.5
53	2	1.5	4.5	2
54	0.5	1.5	3.75 4.375	0.5 3.5
55 56	3.5 2	3 3 3 0	5.25	3.3
50 57	0.5	3	4.375	2 0.5
36	-0.5	0	1.313	-0.5
37	-1.25	ŏ	1.125	-1.25
38	-2	ŏ	1.125	-2
39	-2.75	ŏ	1.125	-2.75
40	-3.5	Ŏ	1.313	-3.5
41	-0.5	1.5	3.75	-0.5
42	-2	1.5	4.5	-2
43	-3.5	1.5	3.75	-3.5
44	-0.5	3 3	4.375	-0.5
45	-2		5.25	-2
46	-3.5	3 0	4.375	-3.5
84	-4.15		0.634	-4.15
85	-4.5	0	0.683	-4.5
86	-4.85	0	0.683	-4.85
87	-5.2	0	0.619	-5.2
88	-6.8	0	0.619	-6.8
89	-7.15	0	0.683	-7.15 7.5
90	-7.5 7.85	0	0.683	-7.5 7.85
91	-7.85 -4.5	0 1.5	0.634 3.19	-7.85 -4.5
93	-4.3	1.5	2.17	-4.3

Conf. # 2C\_12\_0\_16/24, continued

Orif. # 94	Mom. arm	Sta. y 1.5 1.5 3 3 5 5 7 7 7 7 7 7 7 7 7 7	Δ.Area 5.062	Sta. x -6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3	4.375	-4.5
97	-6	3	5.25	-6
98	-7.5	3	4.375	-7.5
211	7	5	8 8	7
212	5	5	8	5
213	3	5	8	-4.5 -6 -7.5 7 5 3
214	1	5	8	1
215	7	7	8 8 8	7 5 3
216	5	7	8	5
217	3	7	8	3
218	1	7	8	1
219	-1	5	8	-1
219 220 221 222 223	-3	5	8	-3
221	-5	5	8	-5
222	-7	5	8	-7
223	-1	7	8	-1
224	-3	7	8 8 8 8 8 8	-3
225	-5	7	8	-5
226	-7	7	8	-7
227	7	9	8	7
228	5	9	8	5
229	3	9	Ř	3
230	ĺ	9	Ř	-1 -3 -5 -7 -1 -3 -5 -7 5 3
231	-7.5 7 5 3 1 7 5 3 1 -1 -3 -5 -7 7 5 3 1 -1 -3 -5 -7	11	Ř	
232	5	11	8	7 5 3
233	3	11	Ř	3
234	ĺ	11	· 8	ĺ
235	<u>-</u> 1	9	8	-1
236	-3	9	8	-3
237	-5	ģ	8	-5
238	<u>-</u> 7	9 9	8	-7
239	- <b>1</b>	11	8	-1
240	-3	11	8	-3
241	-5 -5	11	8	-5
242	-1 -3 -5 -7	11	8 8 8 8 8 8 8 8 8 8 8	-3 -5 -7 -1 -3 -5
272	- /	11	U	-,

	2.33 50.83 2.03 1.95 ACP	0.001875 0.006604 0.006679 0.001310 0.001310 0.001310 0.001310 0.001310 0.001305 0.001305 0.001305	0.0161 0.0161 0.0161
	3.51 50.88 2.03 1.95 ACP	1280 120 120 130 130 131 131 131 131 131	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	4.73 50.88 2.03 1.95 ACD	-0.001877 -0.003052 -0.003053 -0.001080 -0.0011080 -0.0011080 -0.0011080 -0.0011080 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.001173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0.00173 -0	0.107
	5.90 50.77 2.02 1.95		0 . 1080 - 0 . 098 0 . 0109 0 . 0109
	8.85 50.80 2.02 1.95 ACP	0198041889418444	8 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	11.79 50.95 2.02 2.02 1.96 ACP		0.0.329 0.0025 0.0030 0.0030 0.0030
	2 17.70 51.34 2.03 1.97 ACP	00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00.00 00	0.00.00 0.00 0.00 0.00 0.00 0.00 0.00
	Point h/De = Thrust = R Front = R Aft = Y-loc	9.00 9.00 9.00 9.00 9.00 11.00 11.00 11.00 11.00	AV/BA AL/TA AL/TA TA TA T
	Total T NPR NPR X-loc	7.00 5.00 1.00 -1.00 -1.00 -7.00 7.00 1.00 -1.00 -7.00 -7.00	Balance Pressure Balance Pressure
	2.33 50.83 2.03 1.95 ACP	0.007598 0.00720 0.00724 0.00823 0.010899 0.01791 0.012956 0.012956 0.012959 0.012959 0.012959 0.012959 0.012959 0.012979	0.01895 0.018935 0.012601 0.012601 0.012601 0.016100 0.018396 0.018396 0.018396 0.018396 0.018396 0.018396 0.019650 0.018396 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.019669 0.01969
	3.51 2.33 50.88 50.83 2.03 2.03 1.95 ACP	00046651 00076831 00076831 00084664 00084664 00097650 00097660 0007660 0007660 0007660 0007660 0007660 0007660	0.009234 - 0.018760 0.003255 - 0.016935 0.003256 - 0.016915 0.004617 - 0.006413 0.003751 - 0.006413 0.003751 - 0.006413 0.003751 - 0.006413 0.003751 - 0.006413 0.003751 - 0.01326 0.003751 - 0.01326 0.003752 - 0.01326 0.003752 - 0.01326 0.003762 - 0.01366 0.003762 - 0.01366 0.003762 - 0.01366 0.003762 - 0.01366 0.003762 - 0.014657 0.003763 - 0.014657 0.003763 - 0.014657 0.003763 - 0.014657 0.003763 - 0.014657 0.003763 - 0.014657 0.003763 - 0.014657 0.003764 - 0.014657 0.003764 - 0.01366 0.003764 - 0.014657 0.003764 - 0.014657 0.003764 - 0.014657 0.003764 - 0.01366 0.003764 - 0.01366 0.003393 - 0.003744 0.003393 - 0.003744 0.003394 - 0.003394 0.003395 - 0.003395 0.003395 - 0.001396 0.003395 - 0.001396 0.003395 - 0.001396 0.003395 - 0.001396 0.003395 - 0.001396 0.003395 - 0.001396 0.003395 - 0.001396
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	3.54 137.72 4.01 4.01 ACP	0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.0005555 0.000555 0.000555 0.000555 0.000555 0.00055 0.00055 0.00055 0.00055 0.00055 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.0005 0.
	4.72 137.58 4.01 4.00 ACP	0.0023469 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349 0.0003349
	5.90 137.58 4.01 4.00 ACP	-0.001558 -0.00019234 -0.0001924 -0.00019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254 -0.0019254
	8.85 137.69 4.01 ACD	0.0000484 0.00001844 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184 0.0000184
	11.81 137.20 4.00 4.00 ACP	0.00005550 0.00005550 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.00005530 0.000005530 0.000005530 0.000005530 0.000005530 0.000005530 0
	17.68 137.43 4.00 4.00 ACP	-0.000462 -0.0003339 -0.0003319 -0.0003319 -0.0003319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319 -0.000319
	Point h/De = Thrust = R Front = R Aft = Y-loc	9 00 9 00 9 00 9 00 11 00 10 0
	Total T NPR NPR X-loc	7.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
	2.35 137.64 4.01 4.01 ACp	0.005551 0.005551 0.005541 0.0105541 0.0105541 0.0115217 0.0115217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.01155217 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011552 0.011
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Jet-Induced Pressure 2-0-16/24	3 4 5 6 2 3.54 2 3.54 2 4.72 13.74 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 137.72 13	000043 - 0.000492 - 0.001303 - 0.00395 - 0.0044713 - 0.000431 - 0.000495 - 0.001896 - 0.003969 - 0.003969 - 0.004713 - 0.000721 - 0.000986 - 0.001896 - 0.003969 - 0.003969 - 0.000916 - 0.000896 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.000996 - 0.
Jet-Induced Pressure 2C-12-0-16/24	2 3 4 5 6 6 2 8 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1 8 1	0.00434 0. 0.00492 0. 0.01303 0. 0.00355 0. 0.044713 1. 0.00731 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0. 0.00396 0.
Jet-Induced Pressure -12-0-16/24	17.68 11.81 8.85 5.90 4.72 3.54 2 3.43 137.20 137.69 137.58 137.58 137.72 137 4.00 4.00 4.01 4.01 4.01 4.01 4.01 4.01	100131 - 0.000131 - 0.000130 - 0.001305 - 0.001313   1001347 - 0.000131 - 0.000130 - 0.001305 - 0.001313   1001347 - 0.000131 - 0.000132 - 0.001305 - 0.001313   1001347 - 0.000131 - 0.000132 - 0.000130 - 0.001305 - 0.001313   100135 - 0.000131 - 0.000132 - 0.000130 - 0.001305 - 0.001313   100135 - 0.000131 - 0.000132 - 0.000130 - 0.001305 - 0.001313   100031 - 0.000131 - 0.000132 - 0.000130 - 0.001305 - 0.001313   100031 - 0.000131 - 0.000132 - 0.000130 - 0.001311 - 0.000131   100031 - 0.000131 - 0.000132 - 0.000130 - 0.00131   100031 - 0.000131 - 0.000131 - 0.000130 - 0.00131   100031 - 0.000131 - 0.000131 - 0.000131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.00131   100031 - 0.000131 - 0.000131 - 0.000131   100031 - 0.000131 - 0.000131 - 0.000131   100031 - 0.000131 - 0.000131 - 0.000131   100031 - 0.000131 - 0

3.53 225.40 5.97 6.03	-0.002193 -0.004319 -0.004315 -0.001335 -0.001833 -0.001833 -0.001833 -0.001830 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841 -0.001841	3.53 -0.284 -0.265 0.099 0.053
4.73 225.32 5.97 6.03 ACP	-0.001883 -0.001883 -0.001854 -0.001854 -0.001854 -0.001854 -0.001854 -0.001878 -0.001919 -0.001919 -0.001919 -0.001919 -0.001919 -0.001919 -0.001919 -0.001919 -0.001919	4.73 -0.157 -0.168 0.056 0.055
5.91 225.54 5.97 6.04 ACP	-0.001304 -0.001510 -0.0016510 -0.001664 -0.001163 -0.001647 -0.001634 -0.000618 -0.000618 -0.000618 -0.000619 -0.000619 -0.000619 -0.000619 -0.000619 -0.000619 -0.000619	5.91 -0.091 -0.095 0.065 0.065
8.87 225.59 5.97 6.04 ACp	-0.000421 -0.000386 -0.000386 -0.000255 -0.000264 -0.000683 -0.000683 -0.000152 -0.000162 -0.000163 -0.000163 -0.000163	8.87 -0.037 -0.046 0.068 0.058
11.81 225.65 5.97 6.04 ACP	-0.000175 -0.000240 -0.0003610 -0.000375 -0.000450 -0.000245 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00024610 -0.00	11.81 -0.026 -0.032 0.060 0.017
17.72 225.61 5.97 6.04 ACP	-0.000205 -0.000106 -0.0001111 -0.0001111111111111111111111	Summary 17.72 = -0.013 = -0.028 = 0.028
Point h/De = Thrust = Front = Aft = Y-loc	99.00 99.00 99.00 99.00 111.00 111.00 111.00 111.00	Moment h/De AL/T AL/T W/TDe
Total 1 NPR NPR X-loc	7.00 3.00 13.00 -1.00 -7.00 -7.00 3.00 -1.00 -7.00	Force and Balance Pressure Balance /

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Total State | Configuration: 26.12-0-16.74 | Part |
```

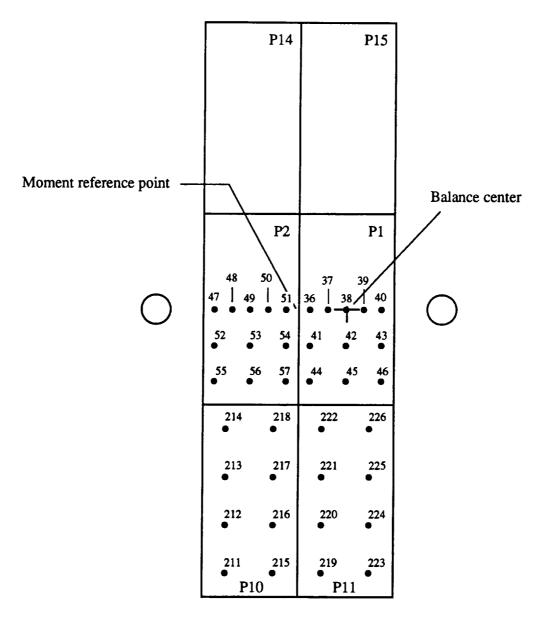


Figure 61. Configuration 2C\_12\_0\_8/24;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_12\_0\_8/24

Orif. # 47 48 49 50 51 52 53 54 55 56 57 36 37	Mom. arm 3.5 2.75 2 1.25 0.5 3.5 2 0.5 3.5 2 0.5 -0.5 -1.25 -2	Sta. y 0 0 0 0 1.5 1.5 1.5 3 3 0 0	Δ.Area 1.313 1.125 1.125 1.125 1.313 3.75 4.5 3.75 4.375 5.25 4.375 1.313 1.125 1.125	Sta. x 3.5 2.75 2 1.25 0.5 3.5 2 0.5 3.5 2 -0.5 -1.25 -2 -2.75
39 40 41	-2.75 -3.5 -0.5	0 0 1.5	1.125 1.313 3.75	-3.5
42 43 44 45	-2 -3.5 -0.5	1.5 1.5 1.5 3	4.5 3.75 4.375 5.25	-2 -3.5 -0.5
46 211 212	-0.5 -2 -3.5 -0.5 -2 -3.5 3 3 3	3 3 3 11 9 7	4.375 8 8 8	-3.5 3 3
213 214 215	3 3 1 1	7 5 11 9	8 8 8 8	-0.5 -2 -3.5 -0.5 -2 -3.5 3 3 1 1 1
216 217 218 219	1 1 -1	7 5 11	8 8 8	-1
220 221 222 223	-1 -1 -1	9 7 5 11	8 8 8 8	-1 -1 -1
223 224 225 226	-3 -3 -3	9 7 5	8 8 8	-3 -3 -3

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	3.55 52.15 2.03 2.00 ACD		0.015
ements Run 219	4.71 52.22 2.03 2.00	4.0000000000000000000000000000000000000	0.029
Incr	5.89 51.96 2.02 2.00 AQD	0.000000000000000000000000000000000000	0.052
Jet-Induced Pressure -0-8/24	8.85 52.08 2.02 2.00 2.00 ACD	0.0003088	0.026
Jet-Indu -12-0-8/24	11.79 52.37 2.03 2.01 ACP	-0.000223 -0.00022422 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.0002228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.000228 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -0.00028 -	
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	Total 1 NPR NPR X-loc	7 Porce and 100 100 100 100 100 100 100 100 100 10	Balance Pressure

	Configuration:	X	Jet-Induced -12-0-8/24	ced Pressure	re Increments Run 220	ints 1 220		
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Y. Joe	× 1,2	ξ	Q V	Ş	Q	Q	Q	Q Q
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Par Cad	# E E	500.0-	-0.005	'	0.013		-0.025	-0.124
Pressure	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \			-0.00	0.011	6	-0.021	-0.111
Halance H		6	-0.026	-0.01	-0.008	ė	-0.009	0.002
Pressure	# (P/)		6	0.0	0.007	Ö	0.019	0.039

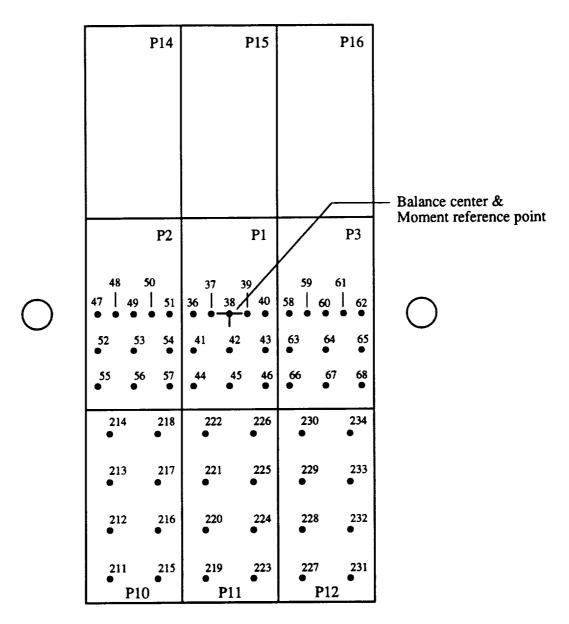


Figure 62. Configuration 2C\_16\_0\_12/24;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

#### Conf. # 2C\_16\_0\_12/24

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
47	5.5	0	1.313	5.5
48	4.75	ő	1.125	4.75
49	4	ŏ	1.125	4.73
50	3.25	ŏ	1.125	3.25
51	2.5	ŏ	1.313	2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4
54	2.5	1.5	3.75	2.5
55	5.5	3	4.375	5.5
56	4	3	5.25	4
57	2.5	3 3 3 0	4.375	2.5
36	1.5	Õ	1.313	1.5
37	0.75	ŏ	1.125	0.75
38	0	Ŏ	1.125	0
39	-Ŏ.75	ŏ	1.125	-0.75
40	-1.5	ŏ	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5		4.375	1.5
45	0	3	5.25	0
46	-1.5	3 3 3 0	4.375	-1.5
58	-2.5	Ō	1.313	-2.5
59	-3.25	Ö	1.125	-3.25
60	-4	Ö	1.125	-4
61	-4.75	Ō	1.125	-4.75
62	-5.5	0	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1.5	4.5	-4
65	-5.5	1.5	3.75	-5.5
66	-2.5		4.375	-2.5
67	-4	3 3 3	5.25	-4
68	-5.5	3	4.375	-5.5
211	-4 -5.5 5 5	11	8 8	5 5 5
212	5	9 7	8	5
213	5	7	8	5
214		5	8	5
215	3	11	8	3
216	3	9	8	3
217	3	7	8	3
218 219	3 3 3 3 1 1	.5	8	3
219	1	11	8	1
220		9	8	1
221	1	7	8	1
222	1	5 11 9 7 5 11 9 7 5	8 8 8 8 8 8 8	5 3 3 3 1 1 1 1 1
220 221 222 223	-1	11	8	-1

Conf. # 2C\_16\_0\_12/24, continued

Orif.#	Mom. arm	Sta. y	∆.Area	Sta. x
224	-1	9 *	8	-1
225	-1	7	8	-1
226	-1	5	8	-1
227	-3	11	8	-3
228	-3	9	8	-3
229	-3	7	8	-3
230	-3	5	8	-3
231	-5	11	8	-5
232	-5	9	8	-5
233	-5	7	8	-5
234	-5	5	8	-5

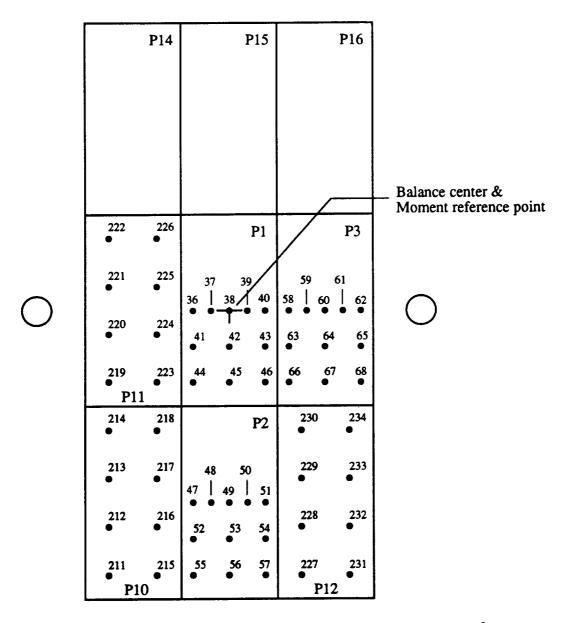


Figure 63. Configuration 2C\_16\_0\_12/24X;  $D_{\Theta} = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_16\_0\_12/24X

Orif. # 219 220 221 222 223 224 225 226 36 37 38 39	Mom. arm 5 5 5 5 3 3 3 1.5 0.75 0 -0.75	Sta. y 3 1 -1 -3 3 1 -1 -3 0 0 0	Δ.Area 8 8 0 0 0 8 8 0 1.313 1.125 1.125	Sta. x 5 5 5 5 3 3 1.5 0.75 0 -0.75
40 41 42 43 44 45 46 58 59 60 61 62 63 64 65 66 67 68 211	-1.5 1.5 0 -1.5 1.5 0 -1.5 -2.5 -3.25 -4 -4.75 -5.5 -2.5 -4 -5.5 -2.5	0 1.5 1.5 1.5 3 3 3 0 0 0 0 0 1.5 1.5 1.5 3 3	1.125 1.313 3.75 4.5 3.75 8.125 9.75 8.125 1.313 1.125 1.125 1.313 3.75 4.5 3.75 4.375 5.25 4.375	-1.5 1.5 0 -1.5 1.5 0 -1.5 -2.5 -3.25 -4 -4.75 -5.5 -2.5 -4 -5.5 -5.5
212 213 214 215 216 217 218 47 48 49 50 51 52 53 54	-2.5 -4 -5.5 5 5 5 5 0 -0.75 0 -1.5	9 7 5 11 9 7 5 8 8 8 8 8 9.5 9.5 9.5	8 8 8 8 8 8 8 5.69 4.875 4.875 4.875 5.69 3.75 4.5 3.75	-2.5 -4 -5.5 5 5 5 5 3 3 1.5 0.75 0 -0.75 -1.5 1.5

Conf. # 2C\_16\_0\_12/24X, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
55	1.5	11	4.375	1.5
56	0	11	5.25	0
57	-1.5	11	4.375	-1.5
227	-3	11	8	-3
228	-3	9	8	-3
229	-3	7	8	-3
230	-3	5	8	-3
231	-5	11	8	-5
232	-5	9	8	-5
233	-5	7	8	-5
234	-5	5	8	-5

Confidence Point P	17.70 51.68 51.68 5.03 1.99 ACP ACP 0.00026 0.00026 0.000271 0.00021 0.000201 0.000201 0.000201 0.000100 0.000100 0.000100	11 11 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	51 8 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	71.000000000000000000000000000000000000	233 223 223 223 223 223 223 223 223 223	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	999999999999
20000000000000000000000000000000000000				9999999999999		0.000000000000000000000000000000000000	01126 000586 000586 0003131 000403 00068 00068 001332 001312
5.50 5.00 5.00 5.00 5.00 5.00 5.00 5.00 5.00 7.00 1.50 8.00 1.50 8.00 1.50 8.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.00 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 9.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50 1.50	0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013 0.000013	0.000000000000000000000000000000000000	0.000124	0.0013992	0.00125341 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541 0.0012541	0.0031986 0.0031986 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988 0.0031988	0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131 0.0013131

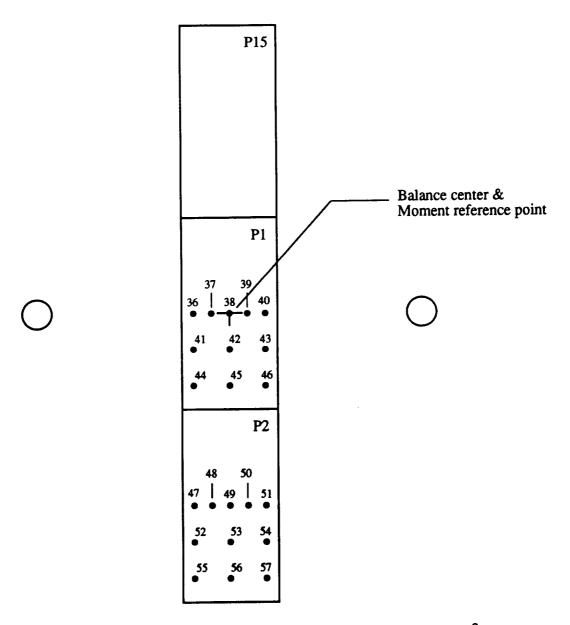


Figure 64. Configuration 2C\_16\_0\_4/24;  $D_{\theta} = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

## Conf. # 2C\_16\_0\_4/24

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5		8.125	1.5
45	0	3	9.75	0
46	-1.5	3	8.125	-1.5
47	1.5	3 3 3 8 8	5.69	1.5
48	0.75	8	4.875	0.75
49	0	8	4.875	0
50	-0.75	8 8 8	4.875	-0.75
51	-1.5	8	5.69	-1.5
52	1.5	9.5	3.75	1.5
53	0	9.5	4.5	0
54	-1.5	9.5	3.75	-1.5
55	1.5	11	4.375	1.5
56	0	11	5.25	0
57	-1.5	11	4.375	-1.5

Configuration: Point h/De = 17. Thrust = 51 8 Aft = 1. Y-10c 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0

	Configu	Jet-Ind Configuration: 2C-16-0-4/24	Jet-Ind -16-0-4/24	Jet-Induced Pressure Increments -0-4/24 Run 22	re Increme Run	ements Run 227		
	Point	1	a	m	~	¥0	•	7
	h/De n	17.71	11.80	8.83	5.88	4.71	3.52	2.34
Total Thrust	hrust =	138.23	138.28	138.13	138.01	137.97	138.03	138.03
NPR	Front .	4.02	4.02	4.01	4.00	4.00	4.01	4.00
MPR	Aft =	4.03	4.03	4.03	4.03	4.03	4.03	4.02
X-10c	2	βÇ	₽Ç	Ş	Ş	<b>QC</b> b	Ş	₽
1.50	0.00	0.000011	٩	0.000053	0.001988	0.004323	0.003696	0.001501
0.75	0.0	0.000000		0.001053	0.003112	0.005680	0.008569	0.011717
00.0	0.0	-0.000045	0	0.000643	0.003571	0.005710	0.009497	0.015715
-0.75	0.0	0.000028	-0.000118	0.000032	0.003499	0.006247	0.008756	0.011372
-1.50	0.00	0.000058	-0.000203	0.000274	0.002162	0.003588	0.004105	0.001917
1.50	1.50	-0.000056	-0.000101	0.000305	0.002267	0.002949	0.003827	0.000707
0.00	1.50	-0.000022	0.000216	•	0.004364	0.005979	0.009523	0.014414
-1.50	1.50	-0.000043	-0.000022	ö	0.001693	0.003336	0.003735	0.001678
1.50	3.00	-0.000090	0.000086	ö	0.001561	0.003213	0.002607	-0.000410
0.0	3.00	-0.000051	-0.000220	0.000583	0.002820	0.006939	0.009104	0.014263
-1.50	9.00 8	-0.000034	0.000105	0.000462	0.001605	0.002590	0.002965	0.000683
1.50	8.00	-0.000053	-0.000038	0.000423	0.000649	0.001907	0.001439	-0.000231
0.75	8.00 8	-0.000051	-0.000054	0.000665	0.001430	0.002422	0.004607	0.004804
0.0	8 OO	-0.000028	-0.000024	0.000626	0.001936	0.003565	0.005544	0.007649
-0.75	8.00 8	-0.000043	-0.000004	0.000641	096000.0	0.002411	0.005033	0.005234
-1.50	8.00	-0.000030	-0.000017	-0.000087	0.000978	0.001272	0.001985	0.000152
1.50	9.50	-0.000071	-0.000026	0.000282	0.000230	0.000941	0.001975	-0.000008
0.0	9.50	-0.000071	-0.000026	0.000282	0.000230	0.000941	0.001975	-0.000008
-1.50	9.50	-0.000045	-0.000045	0.000077	0.000152	0.000992	0.000978	0.000196
1.50	11.00	-0.000045	-0.000045	0.000077	0.000152	0.000992	0.000978	0.000196
0.00	11.00	-0.000019	-0.00000-	0.000485	0.001082	0.001553	0.003417	0.003913
-1.50	11.00	-0.000019	-0.000004	0.000485	0.001082	0.001553	0.003417	0.003913
Force and	Moment	Summery						
	h/De	17.71	11.80	8.83	5.88	4.71	3.52	2.34
Bal ance	<b>∆L</b> /T =	-0.001	-0.001	0.001	0.033	0.058	0.087	0.087
Pressure	<u>*</u> '-	-0.001	-0.000	0.00	0.033	0.063	0.088	0.086
Balance	AM/TDe =	-0.011	-0.008	-0.009	-0.007		-0.00	-0.00\$
Pressure	AM/TDe =	-0.000	-0.000	-0.001	-0.001	0.001	-0.003	-0.006

	Config	Configuration: 2C-	Jet-Indu 16-0-4/24	ced Pressu	Jet-Induced Pressure Increments 2C-16-0-4/24	nts 228	
	Podar	1	N	•	4	s	
	h/De a	17.71	11.79	8.85	00	•	
Total		225.09	225.07	225.28	-	225.12	
6		26.5	S	5.98	5.97	5.97	5.97
Z Z	Aft.	6.9	6.01	6.01	6.01	9.00	9.00
X-10c	Y-10c	₽C.P	ď,	Ş	<b>Q</b>	ĝ	₽ P
1.50		-0.000045	0.000100	0.000325	0.001123	0.002762	ö
	00		00042			0.004862	Ö
•		-0.000081				0.006202	ö
-0.75	00.0		-0.000003	0.000233	0.002353	0.004217	Ö
	00.0	0	-0.000025			0.002826	ö
	1 50	ė	0.000015			0.002338	ö
	1.50	9	0.000031			0.005095	Ö
	1.50	þ	0.000216			0.003115	Ö
1.50	00	Ģ	0.000130	ö		0.002565	Ö
00.0	3.00	0	0.000013	Ö		0.004968	Ö
-1.50	3.00	0	-0.000115	Ö		0.002426	Ö
1.50	8.00	9	-0.000030	ö		0.000795	Ö
0.75	8.00	ę	-0.000091	Ö		0.002338	Ö
0.00	8.00	Ö	0.000053	ö		0.002428	Ö
-0.75	8.00	0	0.000125	ö		0.002181	Ö
-1.50	8.00	0	0.000015	Ö		0.001346	Ö
1.50	9.50	0	0.000018	Ö		0.000724	Ö
00.0	9.50	٩	0.000018	ö	0.000423	0.000724	Ö
-1.50	9.50	Ö	-0.000249	ė		0.001153	Ö
	11.00	0	-0.000249	-0.00000-	69000	0.001153	Ö
	-	0	0.000156	ö		0.001045	
-1.50	11.00	ė	0.000156	ö	.0007	0.001045	0.0033
Force and	Money						
			11.79	8.85	5.88	4.70	3.52
Relance	Y 1.	-0.001	-0.001	0.005	0.026	0.051	0.091
Pressure	1/1	-0.001	0.00	0.007	0.028	0.051	0.093
Ralance	AW/TDe	-0.005	-0.003	-0.001	0.001	-0.001	0.001
Pressure	AM/TDe	-0,000	0.000	-0.000	0.001	-0.001	900.0-

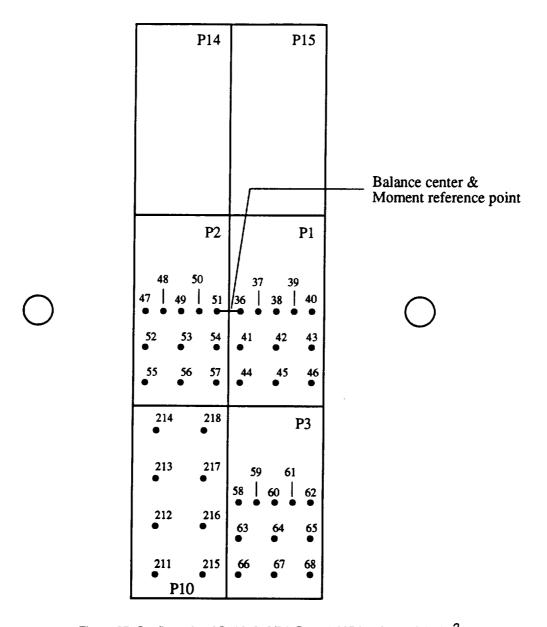


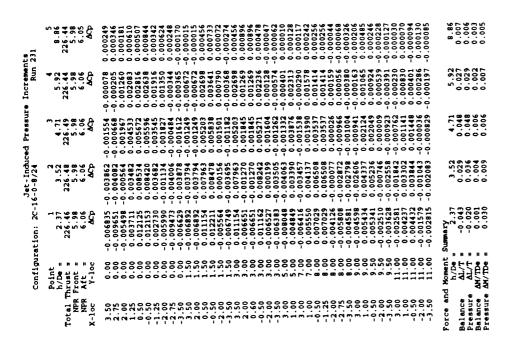
Figure 65. Configuration 2C\_16\_8\_8/24;  $D_{\Theta} = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

### Conf. # 2C\_16\_0\_8/24

Orif. # 47 48 49 50 51 52 53 54 55 56 57 36 37 38	Mom. arm 3.5 2.75 2 1.25 0.5 3.5 2 0.5 3.5 2 0.5 -0.5 -1.25 -2	Sta. y 0 0 0 0 1.5 1.5 1.5 3 3 0 0	Δ.Area 1.313 1.125 1.125 1.125 1.313 3.75 4.5 3.75 4.375 4.375 1.313 1.125 1.125	Sta. x 3.5 2.75 2 1.25 0.5 3.5 2 0.5 3.5 2 0.6 -0.5 -1.25 -2 -2.75
39 40 41 42 43 44 45 46 211 212 213 214 215 216 217 218 58 59 60 61 62 63 64 65 66 67	-2.75 -3.5 -0.5 -2 -3.5 -0.5 -2 -3.5 3 3 3 1 1 1 -0.5 -1.25 -2 -2.75 -3.5 -0.5 -2 -3.5 -0.5 -2	0 0 1.5 1.5 1.5 3 3 3 11 9 7 5 11 9 7 5 8 8 8 8 8 9.5 9.5 9.5 9.5	1.125 1.313 3.75 4.5 3.75 8.125 9.75 8.125 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 7.69 4.875 4.875 4.875 4.5 3.75 4.5 3.75 4.5	-2.75 -3.5 -0.5 -2 -3.5 -0.5 -2 -3.5 3 3 1 1 1 -0.5 -1.25 -2 -2.75 -3.5 -0.5 -2 -3.5 -0.5 -2 -3.5

	Configuration:	ĸ	Jet-Induced -16-0-8/24	ced Pressure	re Increment Run 2	nts 1 229		
	Point	1		•	-	<b>•</b>	•	
	h/De =	17.69	11.79	8	5.90	•	m.	2.3
Total T	284	ᆏ		51.99	51.93	51.91		
	Front *			2.05	7.0	5	٠	
A A				1.98	1.98	1.98	٠	
X-10c	•	₽ P	ď	₽G	Q Q	₽Cp	Q Q	₹
		0000	•	0.00014		-0.001	-0.004	٩
		80000		0.0000		-0.001	-0.005	P
		00001	۰.	0.00052		0.001	-0.002	Ŷ
		00001		0.00142		0.00	0.00	9
		00013	۰.	0.00210		0.00	0.008	0
0		0000	٠.	0.00219		0.00	0.010	0
		.0000	٠.	0.00059		0.0	0.005	0
4		.0000	٠.	0.00142		0.00	-0.00	٩
ri		.00014	٩	96000.0		-0.000	-0.00	9
ë.		.00010	٠.	0.00051		-0.001	-0.004	9
		0.00019	۹.	0.00003		-0.00	-0.00	9
		0.00019	٠.	0.00003		-0.00	-0.00	o o
		0.00018	٠,	0.00168		0.00	0.08	0
ö		0000	٧.	0.00177		0.00	0.00	0
		.00017	٠,	0.00144		0.00	-0.00	o e
mi,		0.00007	٠,٠	0.00063		9.0	90.0	9 0
		# T000 .	٠,٠	0.00168				9
			••	0000				9
				0.00129		00	000	0
		0.00005	٠.	0.00108		0.001	-0.001	9
m.		.0000	۳.	0.00031		-0.003	-0.004	Ŷ
		0.00015		ė,	-0.000374	-0.001487	9 9	٩°
		0.00013	٠,٠	0.00				9
			: `	0000			0	•
ic		50000	: -:	0.00136		0.00	0.007	0
		0.0000	٠.	0.00136		0.003	0.007	0
		.0000	۲.	0.00067		0.00	0.00	o.
'n.		.00012	۳.	0.00076		-0.00	-0.003	9
mi,		0.0000	٠,٠	0.00017		9.00	9	P
			: `	-0.0003				9 0
ic		0000	: 4	0.00073		00.0	0.005	0
		.00017	. ~	0.00052		0.00	-0.000	P
m	è.	.00027	۳.	0.00033		-0.00	-0.003	P
	÷.	0000	٠.	-0.00013		-0.00	-0.00	o o
	≓,	.0000	٠.	0.00028		9 6	2 2	> <
j٠	٠,		••	0000				000
-3.50	11.00		-0.000030	0.00014	-0.000415	-0.001	-0.002	-0.003
Porce and	Komen	S. Carrier						
	),D	17.6	_	8.83	5.90	~	3.52	
Balance	A! /T #	00.0	۰.		.05	ŝ	۰.	7
ssure		ė	0.008	0.026	0.055	0.054	0.032	٢
	AM/TDe =	8	۹.		9	8	٩	۲
Pressure	AM/TDe =	9.0	٩.		ŝ	ş	۰.	

		~	138	7	4.02		٠ 9	-0.01150	-0.00747	0.00268	0.01254	0.01392	0.00368	-0.00596	-0.01043	-0.00	00.00	0.01262	0.01347	-0.00590	-0.00799	0.01262	-0.00782	-0.00782	0.01209	o e	-0.00		9	0	0.0		9	ò	0	9 6	9 9	ę	9	0	0.0	-0.003097	:	•	7	10.0	0	
		~	138	•	4.02		9	٩	9	0	0	0	•	9 9	? 9	? 9	9	0	0	Ŷ	٩	0	٩	ę,	0		9	0	ę		989	0.003984			-0.002132			8	8	8	60	-0.000619				0.037		
ants n 230	5	•	138.00	00. •	4.02		ò	o o	0	0	0	0		5 6	7 9	,			0	0	9	0	0	0		,			٠.	8		38	8	8	-0.000209	8		8	90	8	000	-0.000905		•		0.057	8	
ire Increments Run 23		5	138	•			-0.000431																				000	8	.000	8		35	8	8	8	5 5	3	8	00024	8		-0.000446			3.88	0.042		١
Jet-Induced Pressure -0-8/24	•	-	138.03	0. <del>*</del>	4.02	d d																				0.000442					0.000617								0.000136			-0.000252	•	•		0.013	8	3
16		Ξ	•	0 •	2.6	3	۰.	00013	8	8	۰,	8	0000		100	? <		8	8	8	8	ŝ	8	8	800	Э С	8	8	ŝ	٠.	9,6	•		٠.		. c	, 0		•	000	.00016	-0.000002			11.80	? 0	9	•
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Configuration:	Point	h/De =	Frust =	Front	¥,																					9.5					8 8	8 8	8.				05.0		ä	∹.	∴.	11.00		Moment	# F	\	AH/TO	AM / TEL
			Total	Z.	2 Z	7					o (		٠,	'n٠	i٠					ri					ġ,	9.5	. m															-3.50		Force and	Balance	ressure		



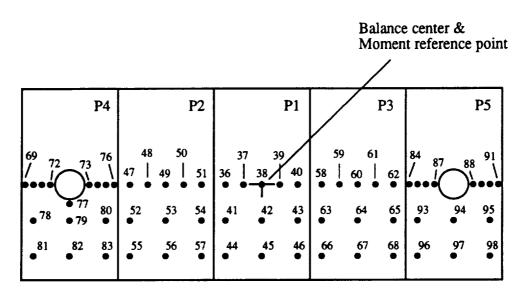


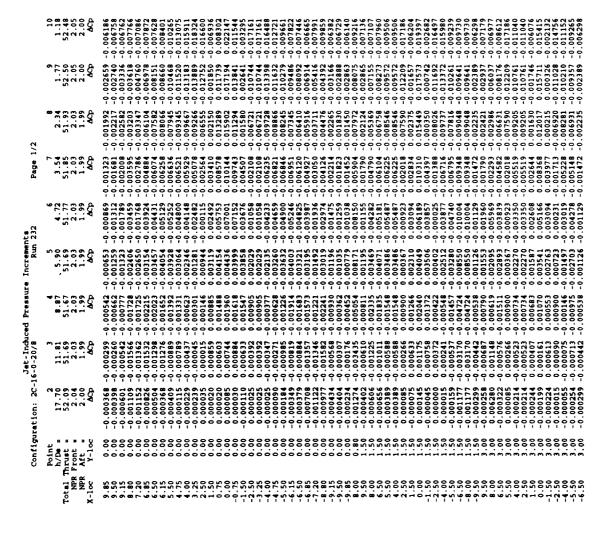
Figure 66. Configuration 2C\_16\_0\_20/8;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

## Conf. # 2C\_16\_0\_20/8

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
69	9.85	0	0.634	9.85
70	9.5	0	0.683	9.5
71	9.15	0	0.683	9.15
72	8.8	0	0.619	8.8
73	7.2	0	0.619	7.2
74	6.85	0	0.683	6.85
75	6.5	0	0.683	6.5
76	6.15	0	0.634	6.15
77	8	0.8	1.238	8
78	9.5	1.5	3.19	9.5
79	8	1.5	3.825	8
80	6.5	1.5	3.19	6.5
81	9.5	3	4.375	9.5
82	8	3	5.25	8
83	6.5	3 3 3 0	4.375	6.5
47	5.5	0	1.313	5.5
48	4.75	0	1.125	4.75
49	4	0	1.125	4
50	3.25	0	1.125	3.25
51	2.5	0	1.313	2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4
54	2.5	1.5	3.75	2.5
55	5.5	3 3 3	4.375	5.5
56	4	3	5.25	4
57	2.5		4.375	2.5
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3 3 3	4.375	1.5
45	0	3	5.25	0
46	-1.5		4.375	-1.5
58	-2.5	0	1.313	-2.5
59	-3.25	0	1.125	-3.25
60	-4	0	1.125	-4
61	-4.75	0	1.125	-4.75
62	-5.5	0	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1.5	4.5	-4
65	-5.5	1.5	3.75	-5.5
66	-2.5	3	4.375	-2.5

Conf. # 2C\_16\_0\_20/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
67	-4	3	5.25	-4
68	-5.5	3	4.375	-5.5
84	-6.15	0	0.634	-6.15
85	-6.5	0	0.683	-6.5
86	-6.85	0	0.683	-6.85
87	-7.2	0	0.619	-7.2
88	-8.8	0	0.619	-8.8
89	-9.15	0	0.683	-9.15
90	-9.5	0	0.683	-9.5
91	-9.85	0	0.634	-9.85
93	-6.5	1.5	3.19	-6.5
94	-8	1.5	5.062	-8
95	-9.5	1.5	3.19	-9.5
96	-6.5	3	4.375	-6.5
97	-8	3	5.25	-8
98	-9.5	3	4.375	-9.5



	Configu	ration: 2C-	Jec-1nox 2C-16-0-20/8	nced Press	ire increments Run 23	232	Page 2/2	7,5			
	Point	7	•	•	ın	•	7	•	•	10	
	h/De	17.70	11.81	8.87	5.90	4.72	3.54	2.34	1.77	1.18	
Total 1	Thrust =	52.09	51.69	51.67	51.69	51.77	51.85	51.93	52.50	52.48	
N. N.	Front =	2.04	2.03	2.03	2.03	2.03	2.03	2.03	2.05	2.05	
Z Z	Aft =	2.00	1.99	1.99	1.99	1.99	1.99	1.99	2.00	2.00	
X-1∞	Y-10c	đ	₽Ç	φÇβ	₽Ç	₽ PC	ď ₽	₽ P	ď ď	<b>₽</b> Cb	
. B.	3.00	-0.000204	-0.000839	-0.001422	-0.002492	-0.003050	-0.003811	-0.004865	-0.005544	-0.005972	
-9.50	3.00	-0.000204	-0.000839	-0.001422		-0.00000-	-0.003811	-0.004865		-0.0039/2	
Force and	d Moment	Summery		!	;		i	;		:	
	~	17.70		8.87	5.90	4.72	4. E	2.34	1.7	81. T	
Balance	•	-0.006		-0.014	-0.035	-0.052	-0.075	-0.123	-0.185	-0.335	
Pressure	-	-0.002		-0.019	-0.04	-0.067	-0.081	-0.138	-0.192	-0.255	
Bel ence	-	-0.001	-0.003	0.003	800.0	0.007	0.010	0.001	0.035	0.033	
Pressure	-	0.036		0.024	0.029	0.012	0.041	0.024	-0.003	-0.021	

	2.36 136.85 4.01 3.97 ACP	-0.003566	38. 6	-0.099	0.011	900.0																																	
	3.51 136.86 4.02 3.98 Acp	-0.003303	5	-0.069	0.005	0.013																																	
	4.71 136.89 4.02 3.98 ACP	-0.002801 -0.002801		-0.044	•	0																																	
	5.89 136.88 4.02 3.98 ACP	-0.002189 -0.002189	5	0.030	0.001	0.020																																	
	8.86 136.59 4.01 3.97 ACP	-0.001057		-0.014																																			
	11.80 136.74 4.01 3.98 ACP	-0.000596	11.80	-0.008	0.00	0.000																																	
	17.69 137.04 4.02 3.99 ACP	-0.000155 -0.000155	Summary 17.69	-0.004	0.007	-0.005																																	
	Point h/De = Thrust = R Front = R Aft = Y-loc	3.00	and Moment :	14.4	AH/TDe	Ø#/TDe ::																																	
	Total T NPR NPR X-loc	-8.00 -9.50	Force ar	Balance Pressure	Balance	Pressure																																	
	7 2.36 136.85 4.01 3.97 ACP	0.001710	0.002741	0.004290	0.006633	0.007090 0.008396	0.008478	0.005579	0.011492	0.015591 0.011912	0.005082	0.004945	0.008452	0.007341	0.006925	0.004373	0.001918	0.002186	0.001571	0.007182	0.001628	0.004326	0.007315	0.007315	0.001079	0.014275	0.006204	0.008763	0.007388	0.001526	0.001992	0.005169	0.005814	0.007639	0.001154	0.002571	0.007718	0.006161 0.001526	
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2.3 3.53 2.35 24 226.17 226.19 39 6.08 6.08 30 ACP ACP	52 -0.002915 -0.003322 52 -0.002915 -0.003322	12 3.53 2.35 14 -0.057 -0.094 12 -0.061 -0.084 13 -0.010 -0.023 14 -0.010 -0.0084
4.72 226.24 5.99 6.08 ACP	-0.002452	4.72 -0.044 0.002
5.89 226.28 5.99 6.08 6.08	-0.002086	5.89 -0.031 -0.040 0.000
8.84 226.36 5.99 6.09 ACD	-0.001084	8.84 -0.013 -0.021 0.006
11.81 226.33 5.99 6.09 ACP	-0.000537	Summary 11.81 -0.007 -0.017 -0.005
Point h/De = Thrust = I Front = I Aft = Y-loc	3.00	Moment h/De AL/T AL/T AM/TDe
Total 1 NPR NPR X-loc	-8.00 -9.50	Force and Balance Pressure Balance

```
Configuration: 2C-16-0-20/8 | Pan 234 | St. 19 |
```

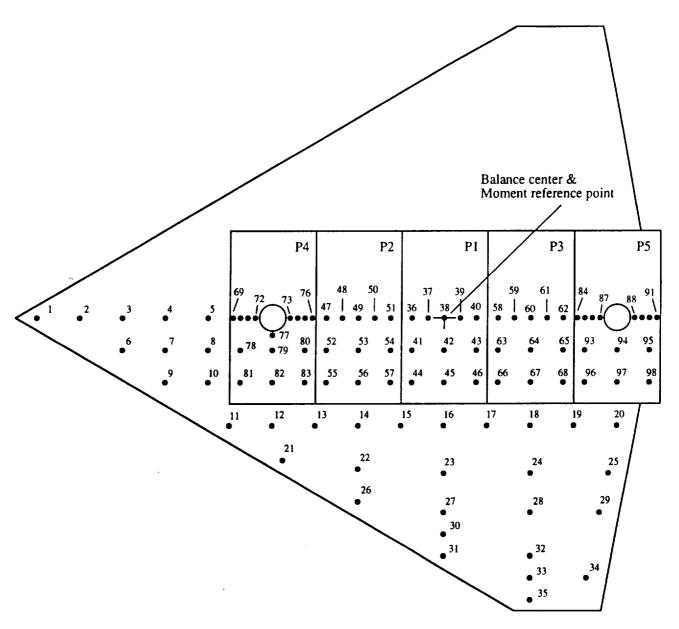


Figure 67. Configuration 2C\_16\_0\_DW;  $D_e = 1.697$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

#### Conf. # 2C\_16\_0\_DW

Orif. #	Mom. orm	Sto	A A===	C40
	Mom. arm 18.6	Sta. y 0	Δ.Area 2.3	Sta. x 19
2	16.86	0	6.918	17
2	15.86	0	0.710	15
3	13	0	3	
4			3	13
2	11	0	3 3 3 8.546	11
0	15	1.5	8.340	15
1 2 3 4 5 6 7 8	13	1.5	6 6	13
8	11	1.5	0	11
9	12.87	1.5 3 3 5 5 5 5 5 5 5 5 5	7.166	13
10	11	3	7	11
11	10.14	5	8.91	10
12	8 6	5	8	8
13	6	5	8	6
14	4	5	8	6 4 2 0
15	2	5	8	2
16	4 2 0 -2	5	8	0
17	-2	5	8	-2
18	-4	5	8 8 8 8 8 8	-4
19	-6	5	8	-6
20	-7.91	5	8.06	-8 7.5
21	7.06	6.6	7.302	7.5
22	4	7	16	4
23	0	7	16	0
24	-4	7 7	16	-4
25	-7.31	7	10.484	-7.6
26	3.235	8.5	9.904	0
27	0		12	Ō
28	-4	9 9 9	12 16	-4
29	-7.11	á	8.908	-7.2
30	0	10	8	0
31	-0.84	11	8 376	ŏ
32	-4	11	12	-4
33	-4	12	8.376 12 8 12.005	-4
34	6 86	12	12 005	-6.6
35	-6.86 -4.17	12 13	6.883	-0.0 -4
69	9.85	0	0.634	9.85
	7.0J			9.63
70 71	9.5	0	0.683	9.15
71	9.15	0	0.683	
72	8.8	0	0.619	8.8
73	7.2	0	0.619	7.2
74 75	6.85	0	0.683	6.85
75 76	6.5	0	0.683	6.5
76	6.15	0	0.634	6.15
77	8	0.8	1.238	8
78	9.5	1.5	3.19	9.5
79	8	1.5	3.825	8

Conf. # 2C\_16\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
80	6.5	1.5	3.19	6.5
81	9.5		4.375	9.5
82	8	3 3 3	5.25	8
83	6.5	3	4.375	6.5
47	5.5	0	1.313	5.5
48	4.75	0	1.125	4.75
49	4	0	1.125	4
50	3.25	0	1.125	3.25
51	2.5	0	1.313	2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4
54	2.5	1.5	3.75	2.5
55	5.5	1.5 3 3 3 0	4.375	5.5
56	4	3	5.25	4
57	2.5	3	4.375	2.5
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3 3 3 0	5.25	0
46	-1.5	3	4.375	-1.5
58	-2.5		1.313	-2.5
59	-3.25	0	1.125	-3.25
60	-4	0	1.125	-4
61	-4.75	0	1.125	-4.75
62	-5.5	0	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1.5	4.5	-4
65	-5.5	1.5	3.75	-5.5
66	-2.5	3	4.375	-2.5 -4
67	-4	3 3 3	5.25	-4
68	-5.5	_	4.375	-5.5
84	-6.15	0	0.634	-6.15
85	-6.5	0	0.683	-6.5
86	-6.85	0	0.683	-6.85
87	-7.2	0	0.619	-7.2
88	-8.8	0	0.619	-8.8
89	-9.15	0	0.683	-9.15
90	-9.5	0	0.683	-9.5
91	-9.85	0	0.634	-9.85
93	-6.5	1.5	3.19	-6.5
94	-8	1.5	5.062	-8
95	-9.5	1.5	3.19	-9.5
96	-6.5	3	4.375	-6.5
97	-8	3 3 3	5.25	-8
98	-9.5	3	4.375	-9.5

	2.33 51.70 2.04 1.98 ACP	0.013756 0.013756 0.004375 0.0043139 0.0043139 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0.007863 0
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	4.72 51.77 2.04 1.98 ACP	0.000000000000000000000000000000000000
	5.90 51.79 2.04 1.98	0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.001816 0.0018
	8.86 51.74 2.04 1.98	0.0000119 0.0000119 0.00001115 0.00001115 0.00001115 0.00001115 0.00001115 0.00001115 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119 0.00001119
	2 11.79 51.18 2.01 1.98 ACP	0.000000000000000000000000000000000000
	17.68 51.65 2.02 1.99 ACP	0.0000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.000075 0.
	Point h/De = 1 Thrust = PR Front = PR Aft *	33.00 3.00 5.00 5.00 5.00 5.00 5.00 5.00 6.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00 7.00
	Total T NPR NPR X-loc	7. 10. 10. 10. 10. 10. 10. 10. 10. 10. 10
	2.33 51.70 2.04 1.98 ACP	0.001118 0.001118 0.001512 0.004611 0.0046111 0.004937 0.004939 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568 0.0011568
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Jet-Induced Pressure 6-0-DW	8.83 5.88 4.70 3.51 7.17 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.2	0.000434 - 0.000252 - 0.000588 - 0.0006653 - 0.000589 - 0.0000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000589 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599 - 0.000599
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Jet-Induced Pressure -16-0-DW	11.80 8.83 5.88 4.70 3.51 137.21 137.21 137.21 137.21 137.21 137.21 137.21 137.20 4.02 4.02 4.02 4.02 4.02 4.02 4.02 4	0000214 - 0.000647 - 0.000427 - 0.000647 - 0.000687 - 0.000881 - 0.000174 - 0.000241 - 0.000242 - 0.000586 - 0.000581 - 0.000684 - 0.000174 - 0.000244 - 0.000241 - 0.000241 - 0.000244 - 0.000241 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000244 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.000241 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00044 - 0.00

		9999999999999999999999999
	11.76 226.91 6.01 6.10	0.000000000000000000000000000000000000
	17.67 226.84 6.01 6.10 ACP	Age and a second
	Point h/De = Thrust = R Front = R Aft = Y-loc	ALA TT P S S S S S S S S S S S S S S S S S
	Total T NPR NPR X-loc	Pressure Pre
	3.51 226.89 6.01 6.09 ACD	0.0001333884
nts 237	4.70 226.94 6.01 6.09 ACP	0.000000000000000000000000000000000000
ire Increments Run 237	5.87 226.84 6.03 6.09 AQP	0.000124
ced Pressur	8.82 226.83 6.01 6.09 ACP	0.000000000000000000000000000000000000
Jet-Indu 16-0-DW	11.76 226.91 6.01 6.00	0.000000000000000000000000000000000000
Jet-Induced Configuration: 2C-16-0-DW	17.67 226.84 6.01 6.10 ACP	0.000001000000000000000000000000000000
Configur	Point h/De = Thrust = R Front = R Aft = Y-loc	
	Total T NPR NPR X-loc	911999999977977979797979797979797979797

3.51 -0.260 -0.215 0.009

4.70 -0.165 -0.146 -0.005

5.87 -0.109 -0.107 -0.037

8.82 -0.052 -0.053 -0.034

5.87 226.84 6.01 6.09 ACP

8.82 226.83 6.01 6.09 ACP

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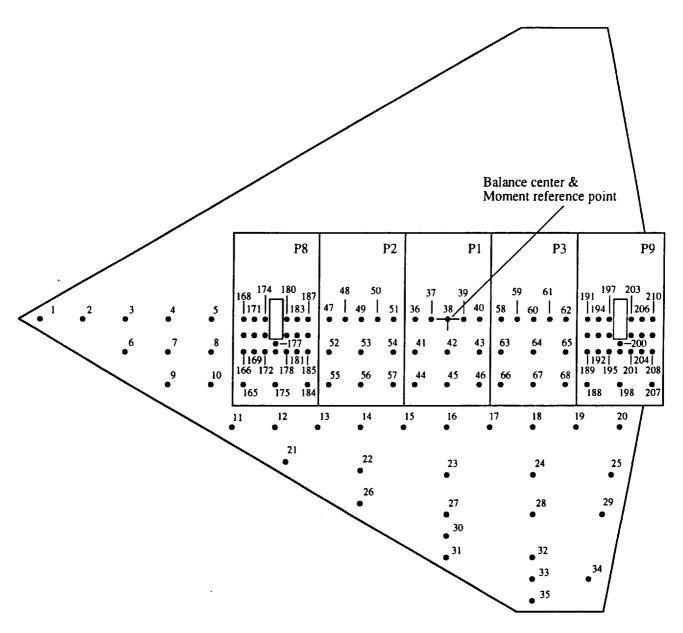


Figure 68. Configuration 2R\_16\_0\_DW;  $D_{\Theta}$  = 1.695 in.,  $A_{jet}$  = 2.26 in.<sup>2</sup>.

#### Conf. # 2R\_16\_0\_DW

		_		_
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
1	18.6	0	2.3	19
2	16.86	0	6.918	17
3	15	0	3	15
4	13	0	3	13
5	11	0	3 3 3 8.546	11
6	15	1.5	8.546	15
ž	13	1.5	6	13
Ý	11	1.5	6 6	11
0	12.87	3	7.166	13
2 3 4 5 6 7 8 9	11	3	7.100	11
10	10.14	<i>5</i>	8.91	10
11	10.14	5	0.71	10
12 13	8 6	5	ð	8 6
13	6	5	8	6
14	4 2 0	5	8	4
15	2	5	8	2
16	0	5	8	0
17	-2	5	8	-2
18	-4	5	8 8 8 8 8 8	-4
19	-6	5	8	4 2 0 -2 -4 -6 -8 7.5
20	-7.91	5	8.06	-8
21	7.06	6.6	7.302	7.5
22	4	7	16	4
23	0	1.5 3 3 5 5 5 5 5 5 5 7 7 7 7	16	0
24	-4	7	16	-4
25	-7.31	7	10.484	-7.6
26	3.235	8.5	9.904	0
27	0		12	Ŏ
28	-4	ģ	16	-4
29	-7.11	9 9 9	8.908	-7.2
30	0	10	Q.200	0
31	-0.84	11	8 8.376	Ö
32	-0.64 -4	11	12	-4
33	-4 -4	12	12 8	-4 -4
33 34		12	12.005	-4
34	-6.86 -4.17	12 13 3	12.005	-6.6
35	-4.1/	13	6.883	-4
165	9.5	3	5.313	9.5
166	9.5	1.5	1.125	9.5
167	9.5	0.75	1.125	9.5
168	9.5	0	0.563	9.5
169	9 9	1.5	0.75	9 9
170	9	0.75	0.75	9
171	9	0	0.375	9
172	8.5	1.5	0.625	8.5
173	8.5	0.75	0.578	8.5
174	8.5	0	0.295	8.5
175	8	3	6.375	8

Conf. # 2R\_16\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
176	8	1.5	0.625	8 8
177	8	1.125	0.62	
178	7.5	1.5	0.625	7.5
179	7.5	0.75	0.578	7.5
180	7.5	0	0.295	7.5
181	7	1.5	0.75	7 7
182	7	0.75	0.75	/
183	7	0	0.375	7
184	6.5	3	5.313	6.5
185	6.5	1.5	1.125	6.5
186	6.5	0.75	1.125	6.5 6.5
187	6.5	0	0.563	5.5
47	5.5	0	1.313	3.3 4.75
48	4.75	0	1.125	4.73
49	4	0	1.125 1.125	3.25
50	3.25	0	1.123	
51	2.5	0		2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4 2.5
54	2.5	1.5	3.75 4.375	2.3 5.5
55	5.5	3	4.373 5.25	3.3 4
56 57	4	3 3 3 0	3.23 4.375	2.5
57	2.5	3	1.313	1.5
36	1.5	0	1.313	0.75
37	0.75	0	1.125	0.73
38	0	0	1.125	-0.75
39	-0.75	0	1.123	-0.73
40	-1.5 1.5	1.5	3.75	1.5
41 42	0	1.5	4.5	0
42	-1.5	1.5	3.75	-1.5
43	1.5		4.375	1.5
45	0	3	5.25	0
46	-1.5	3 3 3 0	4.375	-1.5
58	-2.5	ő	1.313	-2.5
59	-3.25	ŏ	1.125	-3.25
60	-3.23 -4	ŏ	1.125	-4
61	-4.75	ŏ	1.125	-4.75
62	-5.5	ŏ	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1.5	4.5	-4
65	-5.5	1.5	3.75	-5.5
66	-2.5		4.375	-2.5
67	-4	3	5.25	-4
68	-5.5	ž	4.375	-5.5
188	-6.5	3 3 3 3	5.313	-6.5
189	-6.5	1.5	1.125	-6.5
190	-6.5	0.75	1.125	-6.5
191	-6.5	0.73	0.563	-6.5
192	-7	ĭ.5	0.75	-7
193	- <del>'</del> 7	0.75	0.75	-7
	•	<del>-</del>	*	

Conf. # 2R\_16\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	$\Delta$ . Area	Sta. x
194	-7	0	0.375	-7
195	-7.5	1.5	0.625	-7.5
196	-7.5	0.75	0.578	-7.5
197	-7.5	0	0.295	-7.5
198	-8	3	6.375	-8
199	-8	1.5	0.625	-8
200	-8	1.125	0.62	-8
201	-8.5	1.5	0.625	-8.5
202	-8.5	0.75	0.578	-8.5
203	-8.5	0	0.295	-8.5
204	-9	1.5	0.75	-9
205	-9	0.75	0.75	-9
206	-9	0	0.375	-9
207	-9.5	3	5.313	-9.5
208	-9.5	1.5	1.125	-9.5
209	-9.5	0.75	1.125	-9.5
210	-9.5	0	0.563	-9.5





	2.34 52.92 2.14 2.11 ACP	-0.007623 -0.007565 -0.004801 -0.003986	-0.003093 -0.001638	-0.004285	-0.009064	-0.010264	-0.012540	0.011314	-0.004947	-0.011875	-0.009993	-0.005961 -0.002486	-0.001930	-0.004030	-0.010689	0.005853	0.001244	-0.008967	-0.003932	0.007102	-0.006140	-0.003495 -0.003418	0.000306	-0.003000	0.000267	-0.001308	-0.001221		2.34	-0.349	-0.197	-0.412							
	3.52 3.52 51.65 2.10 2.09 ACP	-0.009932 -0.011784 -0.006898 -0.004629	.002888	003535	005463	.004341	.000948	906700.	.001313	.006567	.008333	.006128	.002560	.003133	006967	.006041	.003556	007262	.002152	003392	.004128	.003531	.001509	.003157	001110	002859	002127		3.52	-0.252	-0.059	-0.015							
	4.71 51.64 2.10 2.09 ACP	-0.008579 -0.012403 -0.007442 -0.005112	999	999	? ? ?	99	90	000	90	99	٠,	99	9.	77	99	,	30	99	7	ې د	γ,	۲۲	0.	۲۲	0	٠,	-0.001		4.71	-0.166	-0.057	-0.005							
	5.89 51.55 2.10 2.08 ACP	-0.007873 -0.010849 -0.007497	999	99	99.	9	00	0	0	99	9	99	9	99	90	00	9 0	99	? ?	00	9	99	0	? ?	0 0	9	99	•	5.89	-0.116	-0.089	-0.025							
	8.86 51.63 2.11 2.08 ACP	-0.003306 -0.005066 -0.002488 -0.001913	999	999	90	00	00		- 9	99	? ?	99	99	99	99	, 0	- 0	99	77	٥,	, 0	٥٠		۲۲		ېد	۲۲	•	8.	90.0	-0.015	0.0							
	2.11 51.74 51.74 2.09 ACP	-0.003333 -0.003490 -0.002924 -0.001403	-0.001025	-0.001211	-0.001594	0.000706	0.000636	0.000996	0.000611	-0.000696	-0.001517	-0.001378	-0.000840	-0.000815	-0.000597	-0.000557	-0.00055/	-0.001492	-0.001034	-0.000353	-0.001412	-0.001178 -0.000388	0.000249	-0.000835	-0.000174	-0.000119	-0.000959		-	٥٩	-0.022	•							
	17.71 52.40 2.13 2.10 ACP	-0.001251 -0.001310 -0.000874 -0.000554	000529	000298	000269	000208	000321	000148	000178	000213	000512	000726	000319	000201	000162	000260	000260	000299	000260	000305	000299	000584	000265	000869	000368	000432	000422		Summar.	o o	-0.011	0							
	Point h/De = Thrust = R Front = R Aft = Y-loc	1.50																											h/De	<b>1</b> /1	W/T/W	<b>₩</b> /±							
	Total T NPR NPR X-loc	-7.50 -8.00 -9.50	13.00	9.50	6.50	5.50	2.50	0.0	-1.50 -2.50	9	-6.50	9 9	10.00	00.9 9	9.6	00.0	7.00	9.00	7.50	2.6	90.4	-7.60	0.00	-4.00	0.0	00.	9.9		Force and	Balance	Balance	Pressure							
	22.34 52.92 22.14 2.11 ACP	-0.000870 -0.000875 -0.001104 -0.002105	-0.002105 -0.004498	0.005429	-0.005129 -0.008476	-0.010249 -0.012105	-0.012753	-0.011611	-0.008113 0.004218	0.013718	0.008211	-0.001252	-0.010537	-0.012685 -0.012276	-0.011841	-0.007025	-0.003908	-0.003367	-0.002594	-0.005196	-0.006277	-0.008321	-0.009533	-0.007419	-0.007029	-0.003267 -0.002935	-0.008962	-0.001468	-0.001838 -0.001579	-0.004452	-0.005952	-0.006368	-0.008359	-0.011730	-0.011730 -0.010264	0.000871	0.003939	-0.011943	-0.011909 -0.009533 -0.008255
	તાતાતાતા	-0.000862 -0 -0.000748 -0 -0.000797 -0	-0.001245 -0 -0.002491 -0	-0.002164 -0	-0.002815 -0 -0.003990 -0	-0.006371 -0 -0.007530 -0	-0.008121 -0	-0.006592 -0	0.000838 0	0.006106	0.009780	0.008463 -0	-0.000301	-0.007430 -0	-0.008312 -0	-0.004204 -0.004207 -0	-0.000079	-0.003960 -0	-0.002730 -0	-0.002721 -0	-0.003709 -0	-0.003858 -0	-0.008040	-0.006584 -0	-0.009818	-0.004757 -0	-0.004407	-0.001170	-0.001165 -0 -0.001369 -0	-0.002125 -0	-0.002509 -0	-0.003130	-0.002653 -0	-0.006562 -(	-0.006562 -0.004341 -0	0.001885	0.007389	-0.006462 -0	-0.008/23 -0.008632 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.008585 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.00855 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -0.0085 -
239	525 1165 1165 1165 1165 1165 1165 1165 1	-0.000713 -0.000862 -0 -0.000578 -0.000748 -0 -0.000633 -0.000797 -0 -0.000488 -0.001245 -0	-0.000488 -0.001245 -0	-0.001750 -0.001997 -0	-0.001031 -0.002815 -0 -0.002999 -0.003990 -0	-0.005103 -0.006371 -0 -0.005376 -0.007530 -0	-0.005731 -0.008121 -0	-0.004127 -0.006592 -0	-0.002427 -0.004332 -0	0.004955 0.006106	0.007482 0.009780 0	0.006615 0.008463 -0	0.003245 -0.000301 -0	-0.002934 -0.007430 -0.007430 -0.008733 -0	-0.005155 -0.008312 -0	-0.004626 -0.00/504 -0-0.00/207 -0	0.000494 -0.000779 -0	-0.003868 -0.003960 -0	-0.002079 -0.002730 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 -0.002521 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4.73 220.49 6.16 6.14 ACP	0.005044 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.001518 0.0015	4.73 -0.184 -0.178 0.008 0.010
5.89 220.53 6.16 6.14 ACP	0.0012545 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835 0.00121835	5.89 -0.127 -0.115 -0.011
8.87 220.43 6.17 6.14 6.04	0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.000383 0.0003	8.87 -0.055 -0.063 -0.017
219.75 219.75 6.18 6.10 ACP	0.000133	11.79 -0.040 -0.042 -0.006 -0.010
17.68 220.39 6.20 6.11 ACP	0.000000000000000000000000000000000000	Summary 17.68 -0.024 -0.018 -0.018
Point h/De = Thrust = I Front = Y-loc	441414	nd Moment is h/De = AL/T = AL/T = AM/TDe = e AM/TDe =
Total 7 NPR NPR X-10c		Force an Balance Pressure Balance Pressure

3.55 220.74 6.17 6.14 ACP	0000918 00000918 00000918 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109 0000109	0000 0000 0000 0000 0000 0000 0000 0000 0000
		,00 <b>0</b> 000
4.73 220.49 6.16 6.14 6.24	000045 0000768 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 00000144 0000144 0000144 0000144 0000144 0000144 0000144 00000144 0000144 0000144 0000144 0000144 0000144 0000144 00000144 0000144 0000144 0000144 0000144 0000144 0000144 00000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 00000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144 0000144	00.00 00.00 00.00 00.00 00.00 00.00
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5.89 220.53 6.16 6.14 ACP	00000000000000000000000000000000000000	0000000
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220.43 6.17 6.14 6.00	000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 0000027 0000027 0000027 0000027 0000027 0000027 00000027 00000027 0000000000	
66.1732 66.138 66.138 67.038		1 1 1 1
11.79 219.75 6.18 6.10 ACP		80000000000000000000000000000000000000
7		~~~~
220.3 220.3 6.2 6.1	0.000000000000000000000000000000000000	0.00014 0.00014 0.00016 0.00016
ere C		
Point h/De = Thrust = Front = Aft = Y-loc		ທ່ານ ຄູ່ ຄູ່ ຄູ່ ຄູ່
Total T NPR NPR X-loc	<b>் ஆட்ஸுயு அஅரட்டு நெடிக்கு யுரு ஒரு நடிக்கு நிக்கு நிக்கு நித்திக்கு நடிக்கு நிக்கு நிக்கு நிக்கு நடிக்கு குக்கு</b>	

2.35 138.20 4.13 4.21 ACP	0.00538 0.00438 0.00545 0.005134 0.005134 0.00558 0.00558 0.00558 0.00558 0.00596	001534 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184 00003184	0.00396 0.00550 0.00550 0.00093 0.00093 0.00190 0.00191 0.00191 0.00191 0.00191 0.00191 0.00191 0.00191 0.00191
3.53 138.06 4.13 4.21 ACP	00000000000000000000000000000000000000	0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579 0007579	00000000000000000000000000000000000000
4.72 138.08 4.13 4.20 ACP	0.00468 0.00594 0.00275 0.00275 0.00275 0.00286 0.00286 0.00286 0.00286 0.00286 0.00286	0.004542 0.00454342 0.0050454343434343434343434343434343434343	0.00181 0.00011 0.00128 0.00128 0.00181 0.00283 0.00283 0.00218 0.00218 0.00218 0.00218
8.86 137.86 4.12 4.20 ACP	0.002597 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557 0.001557	0.001188 0.001173 0.00173 0.00173 0.00173 0.00173 0.00173 0.00173 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0.00174 0	0.00023 0.00018 0.00019 0.00022 0.000125 0.00022 0.00022 0.00022 0.00022 0.00022 0.00022 0.00022 0.00022 0.00022
11.81 137.29 4.11 4.18 ACP	0.001830 0.001701 0.001701 0.000891 0.000564 0.000564 0.000564 0.000569 0.000168 0.000168 0.000168	0.0000841 0.0000841 0.0000841 0.0000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841 0.000841	0.000000000000000000000000000000000000
17.71 138.16 4.13 4.21 ACP	0.000398 0.000598 0.00029 0.00029 0.00030 0.00030 0.00030 0.00030 0.00030 0.00030 0.00030	0000153	0.000000000000000000000000000000000000
Point h/De = Thrust = t Front = t Aft = Y-loc	nininininio o o o o o o o o o o o	, m m m m m m m m m m m m m m m m m m m	9.09 9.09 10.00 11.00 11.00 12.00 13.00 Momen Momen Momen MV De- MV TDe- MV TDe- MV TDe-
Total NPR NPR NPR X-loc		44 N d d d d d d d d d d d d d d d d d d	



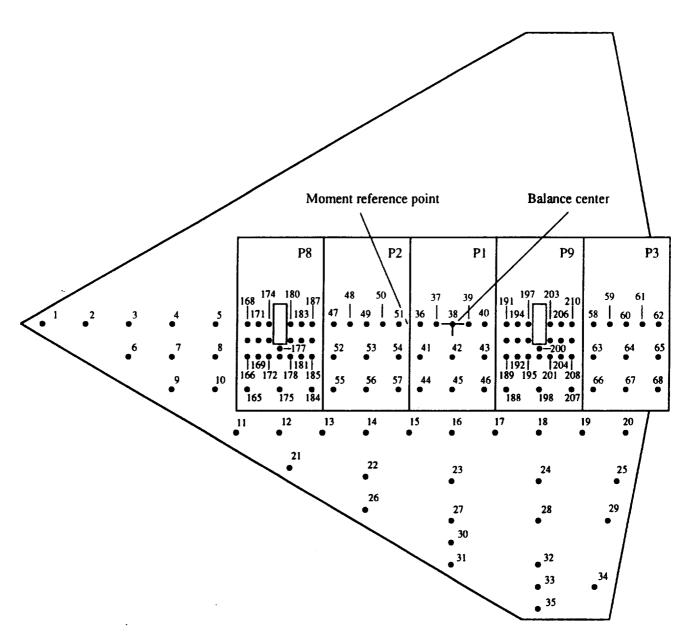


Figure 69. Configuration 2R\_12\_0\_DW;  $D_e = 1.695$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

#### Conf. # 2R\_12\_0\_DW

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
1	16.6	0	2.3	17
2	14.86	ŏ	6.918	15
2 3 4 5 6 7 8 9	13	ŏ	6.918 3 3 3 8.546	13
1	11	Ö	2	
<del>4</del>	11		2	11
2	9	0	3	9 13
5	13	1.5	8.546	13
7	11	1.5	6 6	11
8	9 10.87	1.5		9 11
9	10.87	3	7.166	11
10	9 8.14	3	7 8.91	9
11	8.14	5	8.91	8
11 12	6	5	8	Ğ
13	4	5	Ŷ.	4
14	2	5	Q .	7
15	0	5	0	2
15	0	2	Ŏ O	ŭ
16	-2	5	8	-2
17	4 2 0 -2 -4 -6 -8 -9.91	1.5 3 3 5 5 5 5 5 5 5 5	8 8 8 8 8 8	9 8 6 4 2 0 -2 -4 -6 -8
18	-6	5	8	-6
19	-8	5	8	-8
20	-9.91	5	8.06	-8 -10 5.5 2 -2
21	5.06	6.6	7.302	5.5
22	-9.91 5.06 2 -2 -6	6.6 7 7 7 7	16 16	2
23	-2	7	16	-2
24	-6	7	16	-6 -9.6 -2 -2
25	-9.31	'n	10.484	-0.6
26	1.235	.5 8.5	9.904	-5.0 1
20 27	1.233	0.5	9.904	-2
20	-2 -6	9	12 16	-2
28	-0	9	10	-6
29	-9.11	9	8.908	-9.2
30	-2 -2.84	10	8 8.376	-6 -9.2 -2 -2
31	-2.84	11	8.376	-2
32	-6	11	12	-6
33	-6 -6	12	12 8 12.005	-6 -8.6 -6 7.5
34	-8.86 -6.17 7.5	12	12.005	-8.6
35	-6.17	13 3	6.883	-6
165	7.5	3	5.313	7.5
166	7.5	1.5	1.125	7.5
167	7.5	0.75	1.125	7.5
168	7.5 7.5	0.75	0.563	7.5
169		1.5		7.3
	7		0.75	7
170	7	0.75	0.75	7
171	7	0	0.375	7
172	6.5	1.5	0.625	6.5
173	6.5	0.75	0.578	6.5
174	6.5	0	0.295	6.5
175	6	3	6.375	6

Conf. # 2R\_12\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
176	6	1.5	0.625	6
177	ő	1.125	0.62	6
178	5.5	1.5	0.625	5.5
179	5.5	0.75	0.578	5.5
180	5.5	0	0.295	5.5
181		1.5	0.75	5
182	5	0.75	0.75	5
183	5 5 5	0	0.375	5 5 5
184	4.5	0 3	5.313	4.5
185	4.5	1.5	1.125	4.5
186	4.5	0.75	1.125	4.5
187	4.5	0	0.563	4.5
47	3.5	0	1.313	3.5
48	2.75	0	1.125	2.75
49	2	0	1.125	2.75 2
50	1.25	0	1.125	1.25
51	0.5	0	1.313	0.5
52	3.5	1.5	3.75	3.5
53	2	1.5	4.5	3.5
54	0.5	1.5	3.75	0.5
55	3.5	3	4.375	3.5
56	2	3	5.25	3.5 2
57	0.5	3 3 3	4.375	0.5
36	-0.5	0	1.313	-0.5
37	.1 25	0	1.125	-1.25 -2 -2.75
38	-2	0	1.125	-2
39	-2.75	0	1.125	-2.75
40	-3.5	0	1.313	-3.5
41	-0.5 -2	1.5	3.75	-0.5 -2
42	-2	1.5	4.5	-2
43	-3.5	1.5 1.5 3 3 3	3.75	-3.5
44	-0.5 -2	3	4.375	-0.5 -2
45	-2	3	5.25	-2
46	-3.5	3	4.375	-3.5
188	-4.5	3	5.313	-4.5
189	-4.5	1.5	1.125	-4.5 -4.5
190	-4.5	0.75	1.125	-4.5
191	-4.5	0	0.563	-4.5
192	-5 -5	1.5	0.75	-5
193	-5	0.75	0.75	-5
194	-5	0	0.375	-5
195	-5.5	1.5	0.625	-5.5
196	-5.5	0.75	0.578	-5.5
197	-5.5	0 3	0.295	-5.5
198	-6	3	6.375	-6
199	-6	1.5	0.625	-6
200	-6	1.125	0.62	-6
201	-6.5	1.5	0.625	-6.5
202	-6.5	0.75	0.578	-6.5
203	-6.5	0	0.295	-6.5
204	-7	1.5	0.75	-7

Conf. # 2R\_12\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
205	-7	0.75	0.75	-7
206	-7	0	0.375	-7
207	-7.5	3	5.313	-7.5
208	-7.5	1.5	1.125	-7.5
209	-7.5	0.75	1.125	-7.5
210	-7.5	0	0.563	-7.5
58	-8.5	0	1.313	-8.5
59	-9.25	0	1.125	-9.25
60	-10	0	1.125	-10
61	-10.75	0	1.125	-10.75
62	-11.5	0	1.313	-11.5
63	-8.5	1.5	3.75	-8.5
64	-10	1.5	4.5	-10
65	-11.5	1.5	3.75	-11.5
66	-8.5	3	4.375	-8.5
67	-10	3 3 3	5.25	-10
68	-11.5	3	4.375	-11.5

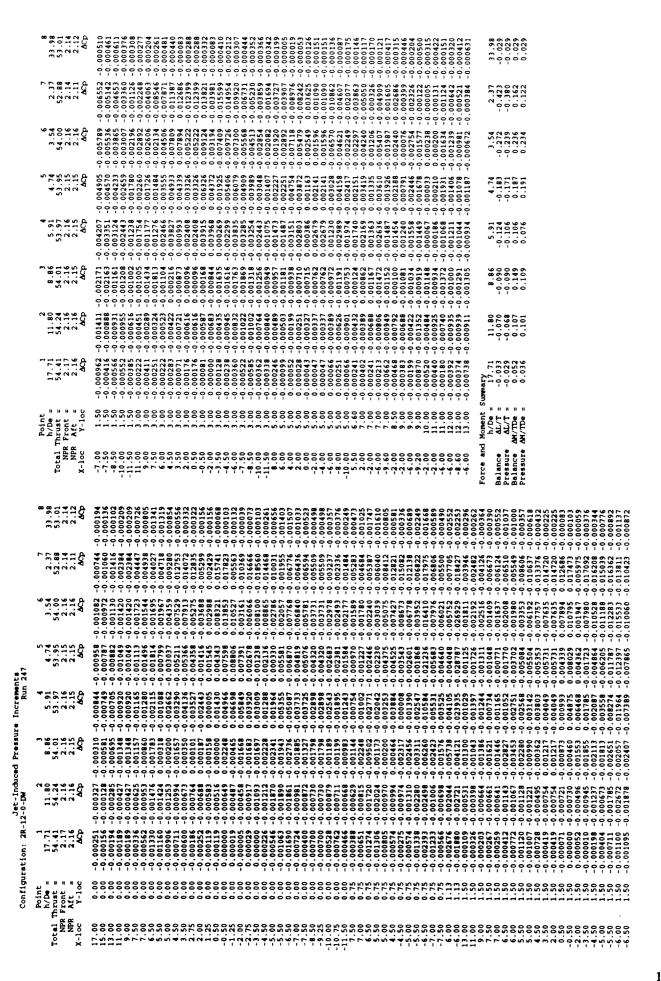
2.35 52.81 2.12 2.12 ACP	0.000000000000000000000000000000000000	00000000000000000000000000000000000000
3.53 3.4.32 2.21 2.11 ACP	0.007244 -0.005244 -0.005280 -0.003180 -0.0031826 -0.0031826 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084 -0.004084	00000000000000000000000000000000000000
5.91 52.14 2.10 2.11 AGP	0.001438	00000000000000000000000000000000000000
8.87 52.31 2.10 2.12 ACP		0.000000000000000000000000000000000000
11.84 52.29 2.10 2.11 ACP	0.000218	0.000949
17.72 51.79 2.11 2.08 ACP	0.000436	0.000119 0.000119 0.0001018 0.0001018 0.0001018 0.0001018 0.0001018 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118 0.000118
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Total T NPR NPR X-loc		

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Jet-Induc -12-0-DW		11.64	• •	:-	8	400000	000354	.000369	.000625	.000625	.000946	.001043	.001661	001014	.000934	.000550	.00064	.00017	10000	66000	.00039	01100.0	00105	.00119	00169	0.00198	0.00208	00124	, 6000 , 6000	0.00083	0.0003	00073	00049	0.00137	0.00189	0.00088	0.00068	0.00148	0.00163	0.00371	0.00124	000101	0.00367	0.00068	0.00040	0.00064	0.00060	0.00162	0.00115	0.00116	0000	00070	0000	9/000	5 5	90	.00164	00203	00163
retion: 2R-		17.72	;;	: 0	8	0.000	0000	00031	.00033	.00033	.00104	.00097	.00103	9000	00074	.00055	.00030	.00019	0000	0000	.00005	.00005	.00013	.00013	0000	00108	.00145	.00094	.00045	.00062	0.00041	00067	00076	0.0003	00178	0000	0.00056	00023	0000	0.00158	000052	0.0005	0.00156	0.0004	0.0002	0.0003	0.00147	0.00167	0.00132	0.0007	0000	00037	0.0000	0000.0	88	0.00019	0.0004	0000	0.0007
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17.70 136.24 4.10 4.14 ACP	0.000134 0.000342 0.000342 0.000342 0.000343 0.000345 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.00035 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.000355 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035 0.00035	0.025
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Point h/De = I Thrust = PR Front = PR Aft = Y-loc	M	AK/TDe = AK/
Total T NPR NPR X-loc	### ##################################	Pressure Balance Pressure
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Jet-Induced Pressure Increments Configuration: 2R-12-0-DW

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Jet-Induced Pressure Increments 2R-12-0-DW	2 3 4 5 6 7 3 5 6 7 5 5 7 5 5 7 5 7 5 7 5 7 5 7 5 7 5	Control   Cont	
Jet-Induced Pressure Increments -12-0-DW	13.99 17.72 11.81 8.86 5.90 4.72 3.55 2 96.02 135.46 135.56 135.50 135.48 135.46 135.51 135 4.11 4.10 4.11 4.11 4.11 4.11 4.13 4.13 4.13 4.13	10.00154   -0.000171   -0.000244   -0.000447   -0.000444   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.000144   -0.00	

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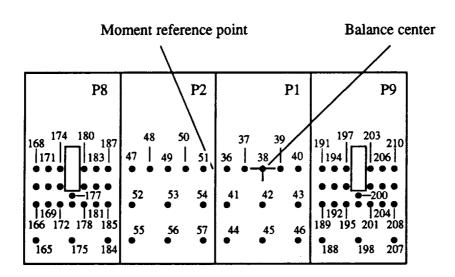


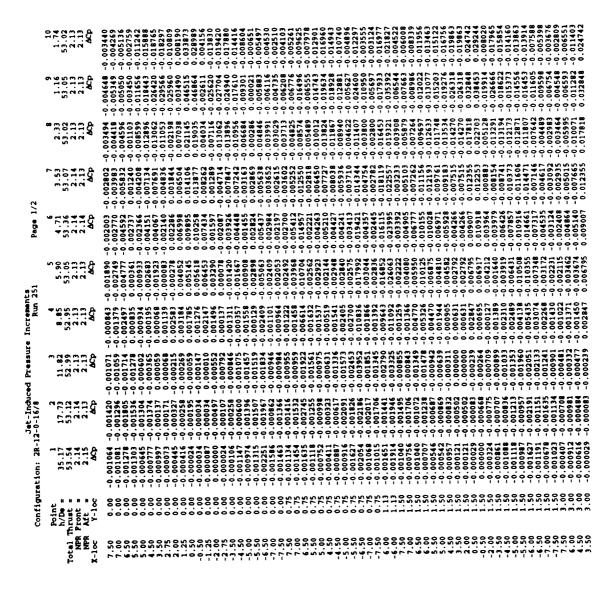
Figure 70. Configuration  $2R_{12_0_16/8}$ ;  $D_e = 1.695$  in.,  $A_{jet} = 2.26$  in.<sup>2</sup>.

#### Conf. # 2R\_12\_0\_16/8

Orif.#	Mom. arm	Sta. y	$\Delta$ . Area	Sta. x
165	7.5	3	5.313	7.5
166	7.5	1.5	1.125	7.5
167	7.5	0.75	1.125	7.5
168	7.5	0	0.563	7.5
169	7	1.5	0.75	7
170	7	0.75	0.75	7 7
171	7	0	0.375	7
172	6.5	1.5	0.625	6.5
173	6.5	0.75	0.578	6.5
174	6.5		0.295	6.5
175	6	0 3	6.375	6
176	6	1.5	0.625	6
177	6	1.125	0.62	6
178	5.5	1.5	0.625	5.5
179	5.5	0.75	0.578	5.5
180	5.5	0.75	0.295	5.5
181	5.5	1.5	0.75	
182	5	0.75	0.75	5 5 5
183	5	0.73	0.375	5
184	5 5 5 4.5	3	5.313	4.5
185	4.5	1.5	1.125	4.5
186	4.5	0.75	1.125	4.5
187	4.5	0.73	0.563	4.5
47	3.5	ő	1.313	3.5
47 48	2.75	0	1.125	2.75
46 49	2.73	Ŏ	1.125	2.73
50	1.25	0	1.125	1.25
51	0.5	0	1.313	0.5
		1.5	3.75	3.5
52	3.5			
53	2	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5	3 3 3 0	4.375	3.5
56	2	3	5.25	2
57	0.5	3	4.375	0.5
36	-0.5	0	1.313 1.125	-0.5
37	-1.25	_		-1.25
38	-2	0	1.125	-2
39	-2.75	0	1.125	-2.75
40	-3.5	0	1.313	-3.5
41	-0.5	1.5	3.75	-0.5
42	-2	1.5	4.5	-2
43	-3.5	1.5	3.75	-3.5
44	-0.5	3	4.375	-0.5
45	-2	3	5.25	-2
46	-3.5	3 3 3 3	4.375	-3.5
188	-4.5	3	5.313	-4.5

Conf. # 2R\_12\_0\_16/8, continued

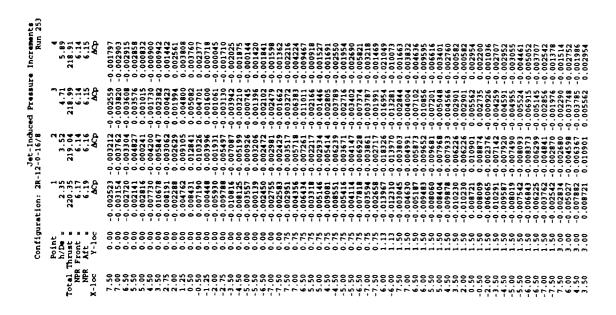
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
189	-4.5	1.5	1.125	-4.5
190	-4.5	0.75	1.125	-4.5
191	-4.5	0	0.563	-4.5
192	-5	1.5	0.75	-5
193	-5	0.75	0.75	-5
194	-5	0	0.375	-5
195	-5.5	1.5	0.625	-5.5
196	-5.5	0.75	0.578	-5.5
197	-5.5	0	0.295	-5.5
198	-6	3	6.375	-6
199	-6	1.5	0.625	-6
200	-6	1.125	0.62	-6
201	-6.5	1.5	0.625	-6.5
202	-6.5	0.75	0.578	-6.5
203	-6.5	0	0.295	-6.5
204	-7	1.5	0.75	-7
205	-7	0.75	0.75	- <b>7</b>
206	-7		0.375	- <b>7</b>
207	- <b>7.</b> 5	0 3	5.313	-7.5
208	-7.5	1.5	1.125	-7.5 -7.5
209	-7.5	0.75	1.125	-7.5 -7.5
210	-7.5 -7.5	0.73	0.563	
210	-7.5	U	0.303	-7.5



	_				_														
	10	1.74	53.02	2.5	ACP	-0.015821	-0.015821	0.019041	-0.008758	-0.016663	-0.012433	-0.006796	-0.004506		1.74	-0.182	-0.151	0.032	0.054
	δ,	1.1	0.00	7.5	ACP.	-0.021496	-0.021496	0.023349	-0.011231	-0.021870	-0.013009	-0.006953			1.16	-0.244	-0.206	0.033	0.097
	<b>60</b> ;	26.33	23.02	2.5	Ş	-0.008935	-0.008935	0.015768	-0.001983	-0.011266	-0.010692	-0.006223	-0.003921		2,33	-0.124	-0.111	0.021	0.033
/3	7	,,,,	5.00		₽Ç	-0.001645	-0.001645	0.011428	0.001410	-0.006837	-0.007656	-0.005372	-0.003375		3.53	-0.067	-0.062	0.034	0.028
Page 2/2	9 .	70.00	41.0	21.5	δÇ	0.001436	0.001436	0.007342	0.002611	-0.004168	-0.005346	-0.005078	-0.002643		4.71	-0.036	-0.035	0.018	0.024
251	20 6	20.00	2.0	2.13	ð	0.001416	0.001416	0.005062	0.001030	-0.002172	-0.003537	-0.004636	-0.002662		5.90	-0.023	-0.028	900.0	0.023
re increments Run 25	4	20.03	2.13	2.13	<b>Q</b>	0.001653		0.001976	0.000675	-0.001232	-0.001304	-0.00229B	-0.000964		8.85	-0.015	-0.013	0.018	0.026
	11 83	000	2.13	2.13	Q.	-0.000049	-0.000049	-0.000684	-0.000792	<b>-0.000694</b>	-0.000955	-0.000926	-0.000000-		11.82	-0.017	-0.018	0.015	0.018
12-0-16/8	12.2	51	2.14	2.13	<b>Q</b>	-0.000917	-0.000917	-0.000463	-0.000716	-0.000444	-0.000783	-0.000679	-0.000650		17.73	-0.018	-0.021	0.004	0.002
Jec-ind Configuration: 2R-12-0-16/8	15.17	45	2.14	2.15	ď	-0.000614	-0.000614	-0.000977	-0.000725	-0.000638	-0.000481	-0.000637	-0.000838	Summary	35.17	-0.016	-0.017	0.013	0.005
Configura	Point h/De =	Frust =	Front =	Aft =	Y-10c	3.00								d Moment St	h/De =	AL/1	<b>∆</b> L/T *	AM/TDe =	AM/TDe =
		Total	NPR	NPR	X-10c	7.00	0.50	-0.50	-7.00	-3.50	-4.50	9-	-7.50	Force and		Balance	Pressure	Balance	Pressure

•	2.32 137.02 4.15 4.17 ACP	0.005710 0.005710 0.015314 0.005634 0.010645 0.008896 0.003383	2.32 -0.105 -0.086 0.013 0.048							
,	3.51 136.98 4.15 4.17 ACP	0.001987 0.001987 0.009459 -0.002955 -0.007007 -0.006285	3.51 -0.058 -0.048 0.010							
	4.71 136.94 4.15 4.17 6CP	0.002349 0.002349 0.005179 -0.001174 -0.004257 -0.004281 -0.003539	4.71 -0.036 -0.035 0.010							
	5.89 136.93 4.15 4.17 ACP	0.001783 0.001783 0.003260 -0.00531 -0.002428 -0.003891 -0.002891	5.89 -0.026 -0.027 0.009 0.019							
	4.84 136.98 4.15 4.16 A.00	0.000025 -0.000287 -0.000673 -0.001131 -0.001135 -0.001175	8.84 -0.020 -0.020 0.014 0.018							
	11.79 137.00 4.15 ACP	-0.000418 -0.000418 -0.000644 -0.000539 -0.000727 -0.000727	11.79 -0.017 -0.018 0.001							
	17.72 136.90 4.15 4.16 ACP	-0.000255 -0.000255 -0.000274 -0.000371 -0.000418 -0.000490	17.72 -0.015 -0.016 0.002 -0.003							
	33.98 136.19 4.13 4.14 ACP	-0.000422 -0.000502 -0.000584 -0.000584 -0.000588 -0.000588 -0.000588	Summary 33.98 -0.012 -0.014 0.005							
	Point h/De = Thrust = R Front = R Aft = Y-loc	000000000000000000000000000000000000000	Moment h/De = AL/T = AL/T = AL/T = AM/TDe =							
	P h Total Thr NPR Fr NPR A X-loc	44444 66666666666666666666666666666666	Force and Balance Pressure Balance /							
	2.32 137.02 4.15 4.17 ACP	0.003275 0.003766 0.004079 0.00338 0.003707 0.010239 0.012176	0.001374 0.015133 0.021701 0.001321 0.007646 0.011966	,,,,,,,	<b></b>		, , , , , , , , ,	7 7 7 7 1	-0.009578 -0.009242 -0.005514 -0.005514 -0.005678 -0.002678 -0.005458 -0.005458	
	2.32 37.02 4.15 6.17	0.003209 -0.003275 0.003785 -0.003766 0.004565 -0.004079 0.005999 0.003336 0.001021 -0.003707 0.005021 -0.010239 0.005919 -0.008732	0.013108 0.0013/4 0.015210 0.021701 0.015211 0.021701 0.014208 0.001221 0.007311 0.001221 0.005392 -0.007464 0.005392 -0.001466	0.003458 0.003458 0.003458 0.003458 0.003458 0.003458 0.003451	0.005030 -0.005030 -0.0050311 -0.0050380 -0.003380 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.005282 -0.00	0.009279 -0.003920 -0.002423 -0.023798	0.008912 0.012155 0.012053 0.007912 0.008912 0.008912	0.013958 0.013958 0.01390 0.01389 -0.007985 -0.008367	-0.0100140.0103530.0058640.0025780.0052870.0052870.005287 -	
	7 2.32 6.98 137.02 4.15 4.15 4.17 4.17 6.09	0.002231 -0.003209 -0.00325 0.00340 -0.003785 -0.003766 0.004717 -0.004655 -0.004079 0.004786 0.005990 0.003305 0.005406 -0.001021 -0.003707 0.002566 -0.005021 -0.010239 0.005517 -0.005659 -0.012136	0.04652 0.03348 0.001348 0.001348 0.001348 0.001348 0.0015133 0.0070623 0.015621 0.021701 0.00524 0.00524 0.00637 0.00637 0.007580 0.007580 0.001458 0.001465 0.001465 0.001467 0.001467 0.001467 0.001467 0.0012443	0.00111 -0.003426 -0.003040 -0.003040 -0.003080 -0.003080 -0.003080 -0.003081 -0.003031 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 -0.003231 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5.89				99	99	,	-0.029	-0.029	0.016	110.0
218.99	6.15 ACP	0.000556	0.002280	-0.003641	-0.003180	4.71	-0.042	-0.047	0.00	010.0
3.52	6.16 ACP	00	- 1	۲۲	99	3.52	-0.061	-0.056	0.015	670.0
2.35 220.35 6.17	6.19 ACP	-0.001636	0.009950	-0.008518	-0.004417		-0.097	-0.098	0.050	P40.2
Point h/De = Thrust = Front :	Aft = Y-loc	3.00	9.6 9.0	3.00	3.00	Moment h/De =	AL/T =	AL/T =	#/T0e	* e7!/17
Totel T	NPR X-10c	2.00	-2.00	-3.50	-6.00	Force and	Balance	Pressure	Bal ance	rressure



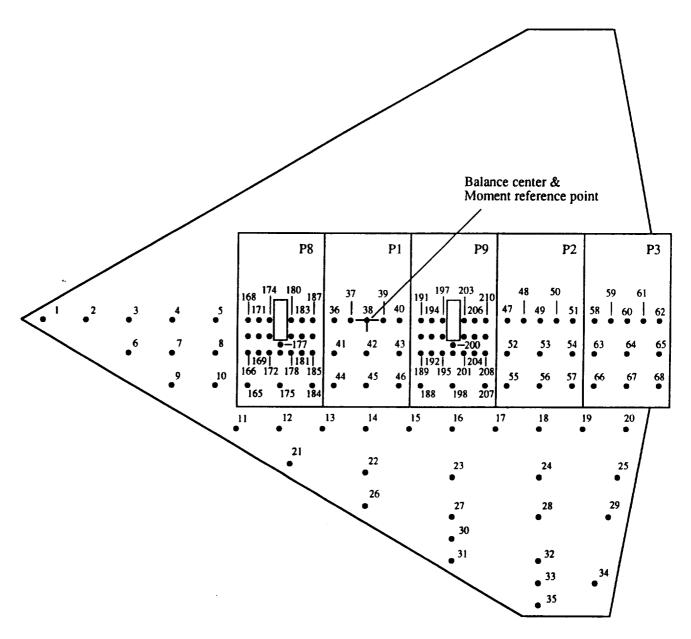


Figure 71. Configuration 2R\_8\_0\_DW;  $D_{\theta}$  = 1.695 in.,  $A_{j\theta t}$  = 2.26 in.<sup>2</sup>.

## Conf. # 2R\_8\_0\_DW

Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
1	14.6	0	2.3	15
2 3 4 5 6 7 8 9	12.86	0	6.918	13
3	11	0	3	11
4	11 9	0	3 3 3	9 7
5	7	0	3	7
6	10.9	1.5	8.546	11
7	10.9 9	1.5 1.5 3 3 5 5 5 5 5 5 5 5	6 6	9 7 9 7 6 4 2 0 -2 -4 -6 -8
8	7	1.5	6	7
9	8.87	3	7.166	9
10	7	3	7	7
11	6.14	5	8.91	6
12	4 2 0	5	8	4
13	2	5	8	2
14	0	5	8	0
15	-2	5	8	-2
16	-4	5	8	-4
17	-6	5	8 8 8 8 8	-6
18	-8	5	8	-8
19	-10	5	8	-10
20	-11.91	5	8.06	-12
21	3.06	6.6 7 7 7	7.302	3.5
22	0	7	16 16	0
23	-4	7	16	-4
24	-8	7	16	-8
25	-11.31	7	10.484	-11.6
26	-0.765	8.5	9.904	0
27	-4	9 9	12 16	-4
28	-8	9	16	-8
29	-11.11	9	8.908	-11.2
30	-4	10	8 8.376	-4 -8 -11.2 -4 -4 -8 -8
31	-4.84	11	8.376	-4
32	-8 -8	11	12	-8
33	-8	12	12 8	-8
34	-10.86	12 13 3	12.005	-10.0
35	-8.17	13	6.883	-8 5.5
165	5.5	3	5.313	5.5
166	5.5	1.5	1.125	5.5
167	5.5	0.75	1.125	5.5
168	5.5	0	0.563	5.5
169	5 5 5	1.5	0.75	5 5 5
170	5	0.75	0.75	5
171	5	0	0.375	
172	4.5	1.5	0.625	4.5
173	4.5	0.75	0.578	4.5
174	4.5	0 3	0.295	4.5
175	4	3	6.375	4

Conf. # 2R\_8\_0\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
176	4	1.5	0.625	4
177	4	1.125	0.62	4
178	3.5	1.5	0.625	3.5
179	3.5	0.75	0.578	3.5
180	3.5	0	0.295	3.5
181	3	1.5	0.75	3
182	3.5 3.5 3 3 2.5 2.5	0.75	0.75	3.5 3 3 2.5
183	3	0	0.375	3
184	2.5	3	5.313	2.5
185	2.5	1.5	1.125	2.5
186	2.5 2.5 2.5	0.75	1.125 0.563	2.5 2.5
187 36	1.5	0 0	1.313	1.5
30 37	0.75	0	1.125	0.75
37 38	0.73	0 0 0	1.125	0.73
39	-0.75	Ô	1.125	-0.75
40	-0.75 -1.5	ŏ	1.313	-1.5
41	-1.5 1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3 3 3 3	5.25	0
46	-1 5	3	4.375	-1.5
188	-2.5 -2.5 -2.5	3	5.313	-2.5
189	-2.5	1.5	1.125	-2.5
190	-2.5	0.75	1.125	-2.5
191	-2.5	0	0.563	-2.5
192	-3	1.5	0.75	-3
193	-3	0.75	0.75	-3 -3
194	-3	0 1.5	0.375	-3.5
195 196	-3.5 -3.5	0.75	0.625 0.578	-3.5
197	-3.5 -3.5	0.73	0.295	-3.5
198	-3.3 -4	0 3	6.375	-3.5 -4
199	-4	1.5	0.625	-4
200	-4	1.125	0.62	-4
201	-4.5	1.5	0.625	-4.5
202	-4.5	0.75	0.578	-4.5
203	-4.5	0	0.295	-4.5
204	-5	1.5	0.75	-5
205	-5	0.75	0.75	-5
206	-5	0	0.375	-5
207	-5.5	3	5.313	-5.5
208	-5.5	1.5	1.125	-5.5
209	-5.5	0.75	1.125	-5.5
210	-5.5	0	0.563	-5.5
47	-6.5 7.25	0	1.313	-6.5 7.25
48	-7.25	0	1.125	-7.25 -8
49 50	-8 9 <b>7</b> 5	0 0	1.125 1.125	-8 -8.75
50 51	-8.75 0.5	0	1.123	-8.73 -9.5
51	-9.5	U	1.313	-7.J

Conf. # 2R\_8\_0\_DW, continued

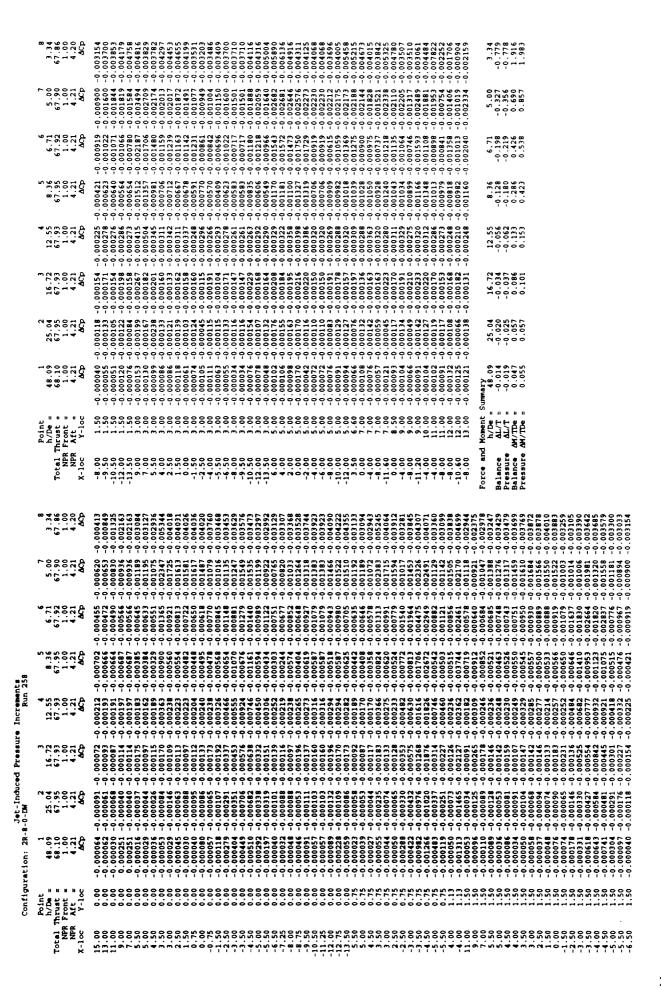
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
52	-6.5	1.5	3.75	-6.5
53	-8	1.5	4.5	-8
54	-9.5	1.5	3.75	-9.5
55	-6.5	3	4.375	-6.5
56	-8	3 3 3	5.25	-8
57	-9.5	3	4.375	-9.5
58	-10.5	0	1.313	-10.5
59	-11.25	0	1.125	-11.25
60	-12	0	1.125	-12
61	-12.75	0	1.125	-12.75
62	-13.5	0	1.313	-13.5
63	-10.5	1.5	3.75	-10.5
64	-12	1.5	4.5	-12
65	-13.5	1.5	3.75	-13.5
66	-10.5	3	4.375	-10.5
67	-12	3 3	5.25	-12
68	-13.5	3	4.375	-13.5

	2.37 52.13 2.13 2.13	0.000343	2.37 -0.390 -0.287 0.280 0.366
	3.54 52.14 2.13 2.13 ACP	0.002544 0.002721 0.002822 0.0028222 0.0028222 0.0028222 0.0028222 0.0028222 0.0028222 0.0028222 0.0028222 0.0028222 0.00282222 0.00282222 0.00282222 0.00282222 0.00282222 0.00282222 0.002822222 0.002822222 0.002822222 0.0028222222 0.00282222222222	0 22 54 -0 22 54 -0 22 54 -0 25 54 -0 55 55 -0 55 -0 55 55 -0 55 -0 55 55 -0 55 -0 55 55 -0 5
	4.71 52.20 2.13 2.13 AQ	0.002233 0.002233 0.00226466 0.002264666 0.00226466666666666666666666666666666666	4 71 -0 166 -0 135 0 148
	5.88 52.25 2.13 2.13	0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131 0.000131	5.88 -0.138 -0.132 0.050 0.050
	8.85 53.02 2.13 2.17 ACP	0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534 0.000534	8.85 -0.095 0.170 0.159
	3 11.80 53.09 2.14 2.17 ACP	0.000134 0.000134 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144 0.000144	11.80 -0.057 -0.096 0.096 0.036
	2 17.71 53.14 2.14 2.16 ACP	0.000233	17.71 -0.035 0.045 0.046 0.046
	33.99 53.43 2.15 2.16 ACP	0.0000134 0.0000134 0.000134 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139 0.000139	Summary Summar
	Point h/De = Thrust = R Front = R Aft = Y-loc		AL/T = AL
	Total T NPR NPR X-loc		Porce and Balance Pressure Pressure Pressure Pressure
	2.33 2.13 2.13 AQD	0.001125 0.001136 0.001136 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.002912 0.0029	0.00365 0.00375 0.00375 0.00475 0.01949 0.01777 0.01157 0.02270 0.02240 0.02604 0.02604 0.02604 0.02604 0.02604 0.02604 0.02604 0.02604 0.02604 0.02604
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2.33 136.97 4.17 4.24 ACP	1107-000 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	-0.347 -0.327 0.322 0.391
3.52 137.05 4.18 4.24 ACP		0.337 0.372 0.337
4.72 137.01 4.17 4.24 ACP	$\mathbf{v}_{ij}$	4:72 -0.177 -0.167 0.364 0.397
5.91 136.95 4.17 4.24 ACP		-0.137 -0.133 -0.133 0.324 0.354
8.86 136.65 4.17 4.23 ACP	· CARTER SETE A STORE TO THE SETE A STORE A ST	8.8 -0.065 -0.065 0.146
11.83 137.01 4.18 4.24 ACP	### ### ##############################	11.83 -0.044 -0.045 0.085
Point h/De = Thrust = Front = Aft = Y-loc	11111111111111111111111111111111111111	AL/T = AL/T = AL/T = AL/T = AL/T = AL/T = AM/TDe
Total 'NPR NPR NPR NPR X-loc	13.50 1.20 1.30 1.30 1.30 1.30 1.30 1.30 1.30 1.3	Balance Pressure Balance Pressure



	3.34 26.41 1.00 2.14 ACP	0.001147 0.001348 0.005639 0.005639 0.0056417 0.004448 0.004488 0.004448 0.004448 0.004448 0.004448 0.004448 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578 0.00578	3.34 -0.799 1.982 1.982 1.984
	5.02 26.44 1.00 2.14 ACP	0.0011734 0.0011734 0.0011737 0.0011737 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131 0.00118131	5 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 . 0 .
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	8.37 26.46 1.00 2.14 ACD	0.000529 0.000538 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548 0.000548	8.37 -0.140 0.3046 0.373
	12.56 26.47 1.00 2.14 ACP	0.000348	12.56 -0.070 -0.1979 0.217
	16.73 26.50 1.00 2.15 ACP	0.0003038	16.73 -0.047 -0.030 0.080
	25.09 26.55 1.00 2.15 ACP	0.000156 0.000156 0.000156 0.000156 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167 0.000167	25. 0.034. 0.1468. 0.046.
	48.11 26.62 1.00 2.15 ACP	0.00000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132 0.0000132	Summary -0.021 -0.017 -0.017 0.145 0.120
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	6.69 5.02 26.44 26.44 1.00 1.00 2.14 2.14 ACP ACP	0.000589 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.000596 -0.0005	0.000740 -0.00128 -0.00078 -0.000740 -0.00178 -0.000740 -0.00178 -0.000740 -0.00178 -0.000740 -0.000740 -0.00178 -0.000740 -0.00178 -0.000740 -0.00178 -0.000740 -0.00178 -0.000740 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.00178 -0.
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Jet-Induced Pressure	5.71 12.55 8.36 6.69 5.03 3.33 5.60 110.74 110.75 110.66 110.68 110.66 1.00 5.30 6.30 6.30 6.30 6.30 6.30 6.30 6.30 6	0.000134	0.000015 -0.000010 0.000000 0.000004 0.000008 0.0000034 0.000011 0.000116 0.000016 0.000011 0.000116 0.0000116 0.0000119 0.0000116 0.0000110 0.0000111 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.0001110 0.000
Jet-Induced Pressure 2R-8-0-DW	5.2 16.71 12.55 8.36 6.69 5.03 3.33 6.36 110.68 110.74 110.75 110.75 110.66 110.68 110.66 110.66 110.66 110.66 110.66 110.66 1.00 1.00	0.000105 -0.000134 -0.000225 -0.000248 -0.000418 -0.000118 -0.000114 -0.000124 -0.000244 -0.000418 -0.000119 -0.000111 -0.000119 -0.000112 -0.000124 -0.000244 -0.000450 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.000111 -0.0001	000159 - 0.000058 - 0.000010 - 0.000000 0.000004 0.000008 0.000003 0.000005 0.000005 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.000015 0.0000015 0.00000015 0.0000015 0.0000015 0.0000015 0.0000015 0.0000015 0.0000010
Jet-Induced Pressure -8-0-DW	1 25.08 16.71 12.55 8.36 6.69 5.03 3.33 10.08 110.35 110.54 110.75 110.66 110.68 110.66 110.66 13.00 1.00 1.00 1.00 1.00 1.00 1.00 1.0	0.000 0.000187 -0.000118 -0.000114 -0.000122 -0.000224 -0.000418 -0.000418 -0.000187 -0.000187 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -0.000118 -	0.000199 -0.000058 -0.000005 -0.000001 0.000004 0.000004 0.000008 -0.000024 -0.0000234 -0.000075 -0.0000114 -0.000014 0.0000711 -0.001112 -0.000313 -0.000001 -0.000011 -0.000114 -0.000124 -0.000071 -0.000114 -0.000114 -0.000475 -0.000114 -0.000124 -0.000077 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.000124 -0.00012

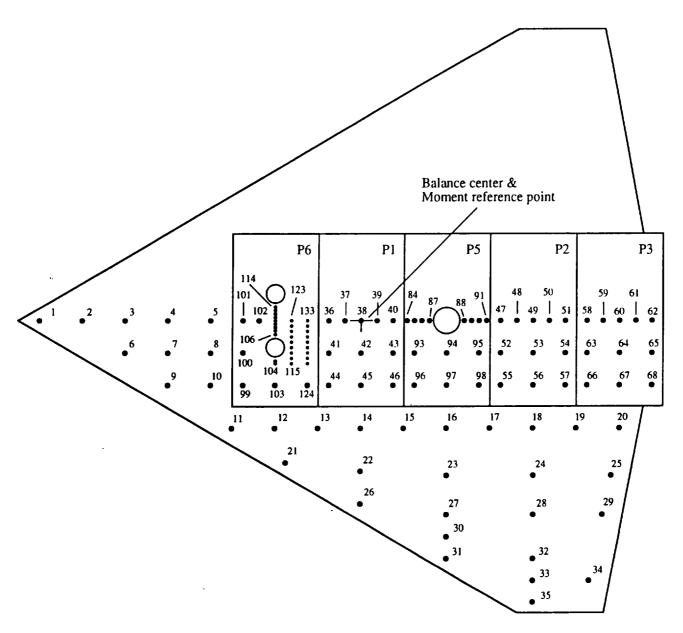


Figure 72. Configuration 3C\_8\_2.5\_DW;  $D_e = 1.699$  in.,  $A_{jet} = 2.27$  in.<sup>2</sup>.

### Conf. # 3C\_8\_2.5\_DW

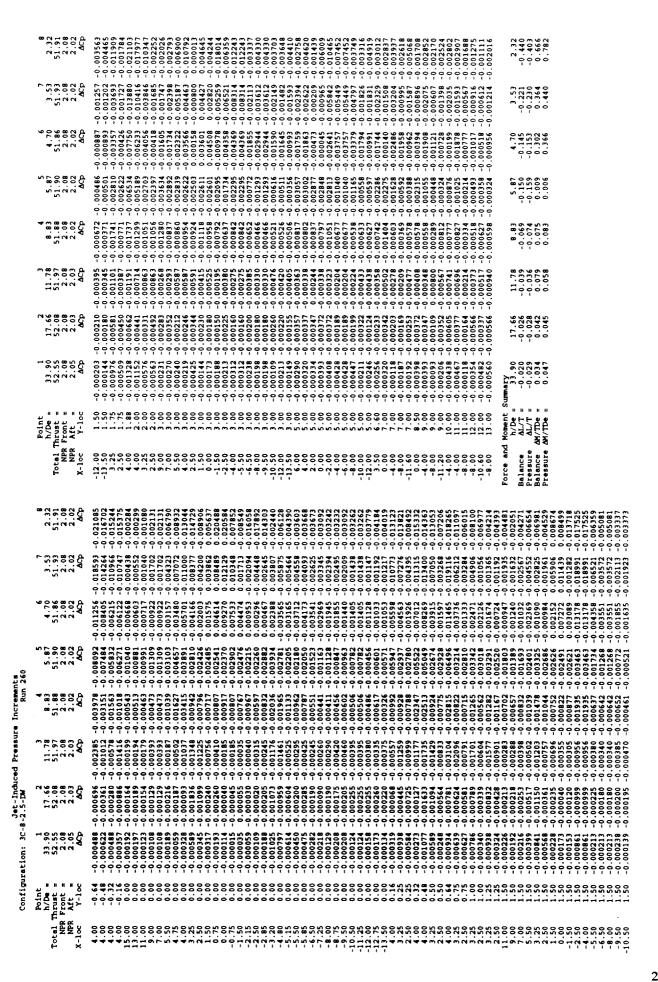
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
1	14.6	0	2.3	15
2	12.86	Ö	6.918	13
2	12.00	ő		11
3	0	Ö	3	9
2 3 4 5 6 7 8 9	11 9 7	0	3 3 3	7
5	10.0	0	3 8.546	
0	10.9 9 7	1.5	8.340	11
/	9	1.5	6 6 7.166	9
8	7	1.5	D	/
9	8.87	1.5 1.5 3 3 5 5 5 5 5 5 5 7 7 7 7 7 8.5	7.166	11 9 7 9 7 6 4 2 0
10	7	3	7 8.91 8 8 8 8 8 8	7
11	6.14	5	8.91	6
12	4	5	8	4
13	2 0	5	8	2
14	0	5	8	0
15	-2	5	8	-2
16	-4	5	8	-4
17	-6	5	8	-6
18	-6 -8	5	8	-8
19	-10	5	8	-10
20	-11.91	5	8.06	-12
21	3.06	6.6	7.302	3.5
21 22	0	7	16	0
23	-4	ή	16 16	<u>-Ă</u>
24	-8	Ź	16	-4 -8
25	-11.31	7	10.484	-11.6
26	-0.765	9.5	9.904	0
20 27		0.2	7.70 <del>4</del> 12	-4
27	-4	9 9	12 16	- <del>-4</del>
28	-8	9	10	-8
29	-11.11	9	8.908	-11.2
30	-4	10	8 8.376	-4
31	-4.84	11	8.376	-4
32	-8 -8	11	12 8	-8
33	-8	12	8	-8
34	-10.86 -8.17	12 13 3	12.005	-10.6
35	-8.17	13	6.883	-8 5.5
99	5.5	3	4.688	5.5
100	5.165	1.5	4.38	5.5
101	5.5	0	1.313	5.5
102	4.75	0 0 3 2	1.125	4.75
103	4	3	5.625	4
104	4	2	0.278	4
105	4	1.88	0.38	4
106	4	0.64	0.38	
107	4	0.48	0.24	À
107	4	0.32	0.24	4 4 4
	4	0.16	0.24	4
109	4	0.10	0.24	4

Conf. # 3C\_8\_2.5\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
110	4	0	0.12	4
111	4	-0.16	0	4
112	4	-0.32	0	4
113	4	-0.48	0	4
114	4	-0.64	0	4
115	3.25	2	0.375	3.25
116	3.25	1.75	0.375	3.25
117	3.25	1.5	0.355	3.25
118	3.25	1.25	0.325	3.25
119	3.25	1 25	0.355	3.25
120	3.25	0.75	0.375	3.25
121 122	3.25	0.5	0.375 0.375	3.25 3.25
122	3.25 3.25	0.25	0.373	3.25
123	2.5	0 3 2	4.688	2.5
125	2.5	2	0.438	2.5
126	2.5	1.75	0.438	2.5
127	2.5	1.5	0.438	2.5
128	2.5	1.25	0.438	2.5
129	2.5	1.23	0.438	2.5
130	2.5	$\hat{0}.75$	0.438	2.5
131	2.5	0.5	0.438	2.5
132	2.5	0.25	0.438	2.5
133	2.5	0	0.219	2.5
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3	5.25	0
46	-1.5	3 3 3 0	4.375	-1.5
84 85	-2.15 -2.5	0	0.634 0.683	-2.15 -2.5
86	-2.85	0	0.683	-2.3 -2.85
87	-3.2	0	0.619	-3.2
88	-4.8	ŏ	0.619	-4.8
89	-5.15	ŏ	0.683	-5.15
90	-5.5	ŏ	0.683	-5.5
91	-5.85	ŏ	0.634	-5.85
93	-2.5	1.5	3.19	-2.5
94	-4	1.5	5.062	-4
95	-5.5	1.5	3.19	-5.5
96	-2.5		4.375	-2.5
97	-4	3 3 3	5.25	-4
98	-5.5	3	4.375	-5.5
47	-6.5	0	1.313	-6.5
48	-7.25	0	1.125	-7.25

Conf. # 3C\_8\_2.5\_DW, continued

Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
49	-8	0	1.125	-8
50	-8.75	0	1.125	-8.75
51	-9.5	0	1.313	-9.5
52	-6.5	1.5	3.75	-6.5
53	-8	1.5	4.5	-8
54	-9.5	1.5	3.75	-9.5
55	-6.5	3	4.375	-6.5
56	-8	3 3 3	5.25	-8
57	-9.5	3	4.375	-9.5
58	-10.5	0	1.313	-10.5
59	-11.25	0	1.125	-11.25
60	-12	0	1.125	-12
61	-12.75	0	1.125	-12.75
62	-13.5	0	1.313	-13.5
63	-10.5	1.5	3.75	-10.5
64	-12	1.5	4.5	-12
65	-13.5	1.5	3.75	-13.5
66	-10.5	3	4.375	-10.5
67	-12	3 3 3	5.25	-12
68	-13.5	3	4.375	-13.5



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Jet-Induced Pressure: 3C-8-2.5-DW	2 11.77 8.83 5.87 4.73 3.53 2 6.5 11.77 18.83 5.87 4.73 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 135.43 13	0.000111 - 0.00134 - 0.00134 - 0.00163 - 0.00475 - 0.00475 - 0.000131 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00134 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00131 - 0.00	-0.000184 -0.000247 -0.000403 -0.000430 -0.001206 -0.001567 -0.002030
Jet-Induced Pressure 3C-8-2.5-DW	1 17.65 11.77 8.89 5.87 4.73 3.53 2.59 135.49 135.49 135.40 4.10 4.10 4.10 4.10 4.10 4.10 4.10 4	000011 - 0.000749 - 0.001345 - 0.001649 - 0.004752 - 0.008291 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001475 - 0.001471 - 0.001471 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.000141 - 0.	1.50 -0.000184 -0.000247 -0.000403 -0.000430 -0.001206 -0.001567 -0.002030

3.51 221.30 6.17 6.07 ACP	0.001205 -0.001145 -0.001510 0.00695 -0.017624 -0.011675	-0.000530 -0.001708 -0.002680 -0.003989 -0.004153	0.003643 0.004564 0.004360 -0.004626	0.003109 0.003109 0.002289 0.001451 0.002830	-0.001074 -0.000308 -0.005412 -0.005611 -0.003858 -0.001785 -0.001785	0.00123 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.00133 0.0013	3.51 -0.214 -0.224 -0.290 0.422
4.70 221.45 6.18 6.07 ACP	001021 001008 001368 001060 007843 005105	001223 001292 001292 002218 001774	002595 000376 003202 003800	001764 001764 001742 001178 000755 001671		001245 000914 000911 000911 000911 001465 001362 000712 000823	4.70 -0.131 -0.131 0.267 0.325
8.51 221.42 6.18 6.07 ACP	000894 000664 000879 000194 005061 004009	000518 000915 001266 001492 000763	001212 000297 0002337 002098	001437 001437 001261 000964 000775 001231	000334 000398 001516 002077 001219 000916 000394	000102 0000102 0000102 0000102 0000102 0000102 0000102 0000102 0000102 0000102	0.51 -0.103 -0.103 0.226 0.249
8.82 221.50 6.18 6.07 ACP	0.000404 0.000408 0.000992 0.000818 0.002504 0.001844	0.000640 0.000812 0.000967 0.000932 0.000992	0.000519 0.000525 0.000525 0.000719	-0.000363 -0.000387 -0.000363 -0.000366 -0.000329	-0.000757 -0.000693 -0.000563 -0.000393 -0.000372 -0.000419 -0.000419	0.000432	8.82 -0.057 -0.061 0.061 0.053
3 221.65 6.18 6.07 ACP	0.00033 0.000232 0.000417 0.000880 0.000880	0.000287 0.000287 0.000249 0.000314	0.000242 0.000242 0.000242 0.000251	0.000250 0.000273 0.000273 0.000265 0.000330	-0.000329 -0.000329 -0.000194 -0.000194 -0.000232 -0.000232	-0.000149 -0.000149 -0.000136 -0.000196 -0.000196 -0.000196 -0.000152 -0.000193	11.79 -0.032 -0.067 0.067 0.056
2 17.68 221.60 6.18 6.07 ACP	000197 000190 000464 000391 002634 001049	000267 0000118 000062 000161	000217 000134 0000183 0000161	000123 000123 000124 000154 000178	000124 000113 000171 000118 000018 000196 000173	-0.000239 -0.000282 -0.0002839 -0.000282 -0.000282 -0.000283 -0.0002382 -0.0002382 -0.0002382 -0.0002382	17.68 -0.010 -0.010 -0.047 0.038
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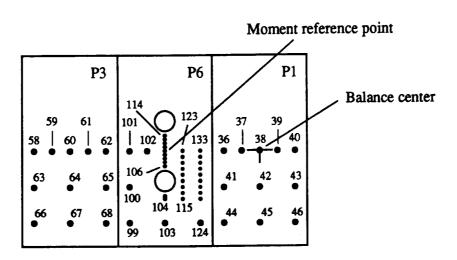


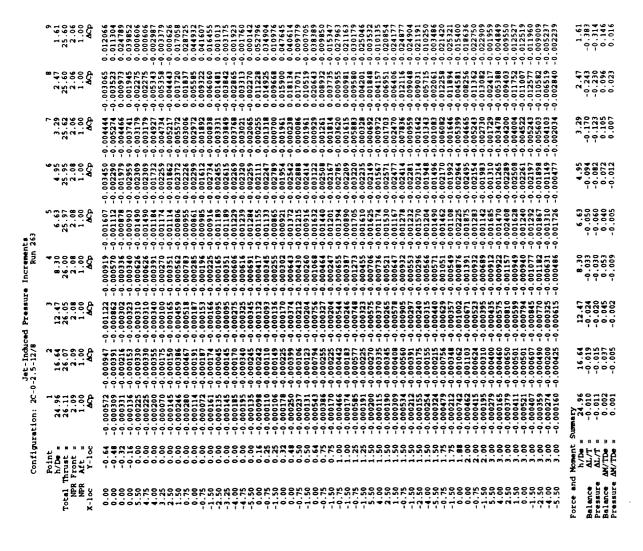
Figure 73. Configuration 2C\_0\_2.5\_12/8;  $D_{\theta}$  = 1.202 in.,  $A_{jet}$  = 1.13 in.<sup>2</sup>.

### Conf. # 2C\_0\_2.5\_12/8

Orif. # 36 37 38 39 40 41 42 43 44 45 46 99 100 101 102 103 104 105 106 107 108 109 110 111 112 113 114 115 116 117 118 119 120 121 122 123 124 125 126 127	Mom. arm -2.5 -3.25 -4 -4.75 -5.5 -2.5 -4 -5.5 -2.5 -4 -5.5 1.5 1.165 1.5 0.75 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	Sta. y 0 0 0 0 1.5 1.5 1.5 1.5 3 3 3 1.5 0 0 3 2 1.88 0.64 0.48 0.32 0.16 0 -0.16 -0.32 -0.48 -0.64 2 1.75 1.5 1.5 1.25 1 0.75 0.5 0.25 0 3 2 1.75 1.5	A.Area 1.313 1.125 1.125 1.125 1.313 3.75 4.5 3.75 4.5 3.75 4.375 4.688 4.38 1.313 1.125 5.625 0.278 0.38 0.38 0.24 0.24 0.24 0.12 0 0 0 0 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375 0.375	Sta. x -2.5 -3.25 -4 -4.75 -5.5 -2.5 -4 -5.5 1.5 1.5 1.5 0.75 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
123	-0.75	0 3	0.188	-0.75
125	-1.5	2	0.438	-1.5

Conf. # 2C\_0\_2.5\_12/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
58	5.5	0	1.313	5.5
59	4.75	0	1.125	4.75
60	4	0	1.125	4
61	3.25	0	1.125	3.25
62	2.5	0	1.313	2.5
63	5.5	1.5	3.75	5.5
64	4	1.5	4.5	4
65	2.5	1.5	3.75	2.5
66	5.5	3	4.375	5.5
67	4	3	5.25	4
68	2.5	3	4.375	2.5



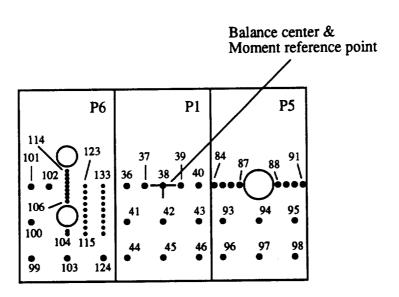


Figure 74. Configuration 3C\_8\_2.5\_12/8;  $D_{\theta}$  = 1.699 in.,  $A_{jet}$  = 2.27 in.<sup>2</sup>.

#### Conf. # 3C-8-2.5-12/8

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
99	5.5	3	4.688	5.5
100	5.165	1.5	4.38	5.5
101	5.5	0	1.313	5.5
102	4.75	ŏ	1.125	4.75
103	4	3	5.625	4
103	4	3 2	0.278	4
105	4	1.88	0.38	4
106	4	0.64	0.38	4
107	4	0.48	0.38	4
107	4	0.48	0.24	4
	4			
109	4	0.16	0.24	4
110	4	0	0.12	4
111	4	-0.16	0	4
112	4 4	-0.32	0	4
113	4	-0.48	0	4
114	4	-0.64	0	4
115	3.25	2	0.375	3.25
116	3.25	1.75	0.375	3.25
117	3.25	1.5	0.355	3.25
118	3.25	1.25	0.325	3.25
119	3.25	1	0.355	3.25
120	3.25	0.75	0.375	3.25
121	3.25	0.5	0.375	3.25
122	3.25	0.25	0.375	3.25
123	3.25	0	0.188	3.25
124	2.5	0 3 2	4.688	2.5
125	2.5	2	0.438	2.5
126	2.5	1.75	0.438	2.5
127	2.5	1.5	0.438	2.5
128	2.5	1.25	0.438	2.5
129	2.5	1	0.438	2.5
130	2.5	0.75	0.438	2.5
131	2.5	0.5	0.438	2.5
132	2.5	0.25	0.438	2.5
133	2.5	0	0.219	2.5
36	1.5	ŏ	1.313	1.5
37	0.75	ŏ	1.125	0.75
38	0.75	ŏ	1.125	0.73
39	-0.75	Ö	1.125	-0.75
40	-1.5	Ö	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5		0
42		1.5	4.5 3.75	
	-1.5 1.5		3.75	-1.5
44	1.5	ა ე	4.375	1.5
45	0	3 3 3	5.25	0
46	-1.5	3	4.375	-1.5

Conf. # 3C\_8\_2.5\_12/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
84	-2.15	0	0.634	-2.15
85	-2.5	0	0.683	-2.5
86	-2.85	0	0.683	-2.85
87	-3.2	0	0.619	-3.2
88	-4.8	0	0.619	-4.8
89	-5.15	0	0.683	-5.15
90	-5.5	0	0.683	-5.5
91	-5.85	0	0.634	-5.85
93	-2.5	1.5	3.19	-2.5
94	-4	1.5	5.062	-4
95	-5.5	1.5	3.19	-5.5
96	-2.5	3	4.375	-2.5
97	-4	3	5.25	-4
98	-5.5	3	4.375	-5.5

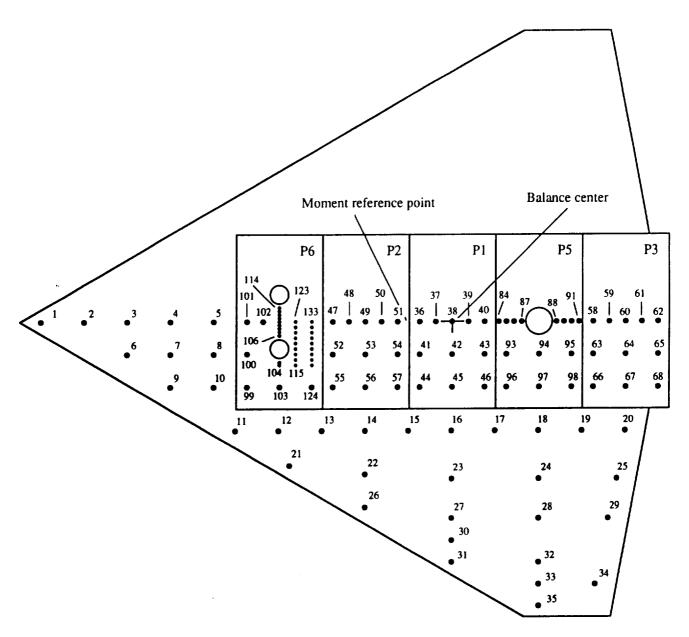


Figure 75. Configuration 3C\_12\_2.5\_DW;  $D_e = 1.699$  in.,  $A_{jet} = 2.27$  in.<sup>2</sup>.

### Conf. # 3C-12-2.5-DW

О-:с н	Mana ama	C4	<b>A A</b>	σ.
Orif. #	Mom. arm 16.6	Sta. y	Δ.Area	Sta. x
1	10.0	0	2.3	17
2	14.86	0	6.918	15
3	13	0	3	13
4	11	0	3	11
2	9	0	3 3 3 8.546	9
0	13	1.5	8.546	13
/	11	1.5	6	11
2 3 4 5 6 7 8 9	9 13 11 9 10.87	1.5	6 7.166	9
9	10.87	3	7.166	11
10	9 8.14	3	7 8.91	9
11	8.14	5	8.91	8
12	6	5	8	6
13	4	5	8	4
14 15	2	5	8	2
15	0	5	8	0
16	-2	5	8	-2
17	-4	5	8	-4
18	4 2 0 -2 -4 -6 -8 -9.91	1.5 1.5 3 3 5 5 5 5 5 5 5 7 7 7 7 7 8.5	8 8 8 8 8 8	8 6 4 2 0 -2 -4 -6
19	-8	5	8	-8
20	-9.91	5	8.06	-10
21	5.06	6.6	7.302	5.5
22	2	7	16 16	2
23	-2	7	16	-2
24	5.06 2 -2 -6 -9.31	7	16	-6
25	-9.31	7	10.484	-9.6
26	1.235	8.5	9.904	-2
27	-2	9	12	-2
28	-2 -6	9	16	-6
29	-9.11	9	8.908	-9.2
30	-2	9 9 9 10	8	-2
31 32	-2 -2.84	11	8 8.376	-2
32	-6 -6	11	12 8	-6
33	-6	11 12	8	-6
34	-8.86	12	12.005	-86
35	-8.86 -6.17	13 3	6.883	5.5 2 -2 -6 -9.6 -2 -6 -9.2 -2 -6 -6 -8.6 -6 7.5
99	7.5	- 3	4.688	75
100	7.165	1.5	4.38	7.5
101	7.5		1.313	7.5
102	6.75	0 0 3 2	1.125	6.75
103	6	3	5.625	6
104	6	2	0.278	6
105	6	1.88	0.38	6
105	6	0.64	0.38	6
100	6	0.48	0.38	6
107	6	0.32	0.24	6
108	6	0.32	0.24 0.24	6
109	U	0.10	U.24	O

Conf. #  $3C_{12}_{2.5}_DW$ , continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
110	6	0	0.12	6
111	6	-0.16	0	6
112	6	-0.32	0	6
113	6	-0.48	0	6
114	6	-0.64	0	6
115	5.25	2	0.375	5.25
116	5.25	1.75	0.375 0.355	5.25 5.25
117	5.25 5.25	1.5 1.25	0.325	5.25
118	5.25 5.25	1.23	0.355	5.25
119	5.25 5.25	0.75	0.375	5.25
120	5.25 5.25	0.73	0.375	5.25
121 122	5.25 5.25	0.25	0.375	5.25
122	5.25 5.25		0.188	5.25
123	5.25 4.5	0	4.688	4.5
124	4.5 4.5	3 2	0.438	4.5
125	4.5	1.75	0.438	4.5
120	4.5	1.73	0.438	4.5
128	4.5	1.25	0.438	4.5
129	4.5	1	0.438	4.5
130	4.5	$\hat{0}.75$	0.438	4.5
131	4.5	0.5	0.438	4.5
132	4.5	0.25	0.438	4.5
133	4.5	0	0.219	4.5
47	3.5	Ŏ	1.313	3.5
48	2.75	Ö	1.125	2.75
49	2	Ŏ	1.125	2.75 2
50	1.25	0	1.125	1.25
51	0.5	0	1.313	0.5
52	3.5	1.5	3.75	3.5
53	2	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5	3	4.375	3.5 2
56	2	3 3 3 0	5.25	2
57	0.5	3	4.375	0.5
36	-0.5		1.313	-0.5
37	-1.25	0	1.125	-1.25
38	-2	0	1.125	-2 -2.75
39	-2.75	0	1.125	-2.75
40	-3.5	0	1.313	-3.5
41	-0.5 -2	1.5	3.75	-0.5
42	-2	1.5	4.5	-2
43	-3.5	1.5	3.75	-3.5
44	-0.5	1.5 3 3 3	4.375	-0.5 -2
45	-2	3	5.25	- <u>L</u>
46	-3.5	5	4.375	-3.5
84	-4.15	0	0.634	-4.15
85	-4.5	0	0.683	-4.5 4.95
86	-4.85	0	0.683	-4.85
87	-5.2	0	0.619	-5.2
88	-6.8	0	0.619	-6.8

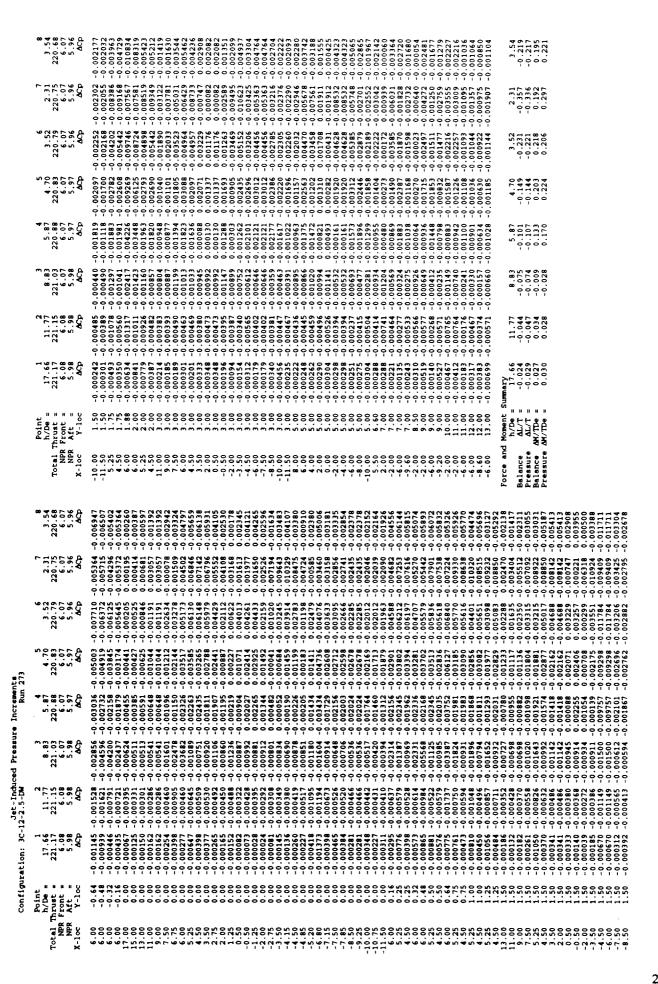
Conf. # 3C\_12\_2.5\_DW, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
89	-7.15	0	0.683	-7.15
90	-7.5	0	0.683	-7.5
91	-7.85	0	0.634	-7.85
93	-4.5	1.5	3.19	-4.5
94	-6	1.5	5.062	-6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3	4.375	-4.5
97	-6	3 3 3	5.25	-6
98	-7.5	3	4.375	-7.5
58	-8.5	0	1.313	-8.5
59	-9.25	0	1.125	-9.25
60	-10	0	1.125	-10
61	-10.75	0	1.125	-10.75
62	-11.5	0	1.313	-11.5
63	-8.5	1.5	3.75	-8.5
64	-10	1.5	4.5	-10
65	-11.5	1.5	3.75	-11.5
66	-8.5	3	4.375	-8.5
67	-10	3 3 3	5.25	-10
68	-11.5	3	4.375	-11.5

	5.89 51.23 2.04 1.98 ACp	-0.000999999999999999999999999999999999	.002041
	10 117 116 116 117 104 ACp	4 - 100 N 0 0 4 4 4 4 0 5 0 0 4 1 0 5 0 4 4 1 0 5 0 4 1 0 5 0 5 0 5 4 5 0 8 7 0 5 0 5 4 8 7 0 5 4 4 6 8 1 4 4 5 6 5 0 4 1 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0 5 0	14.1
		0.0115047 0.0011518 0.0011518 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551 0.0010551	0.019
	11.77 11.15 22.04 11.98	1114488611111768048845020001884112001900000000000000000000000000000000	901
	11.74.4 4	0.00000118 0.00000118 0.0000118 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119 0.0000119	0.007
	0.864638	0 M 1 1 0 0 4 C C 0 C C C C C C C C C C C C C C	2
	2.33 51.16 2.04 1.98 ACP	0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.006103 0.0061	.0037
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	5.86 2.123 2.04 1.98		28
n 27			9
Increments Run 271	51:29 2:04 1:98 ACP	004667 004687 000488 000053 000053 000053 000053 000053 000053 000053 000053 000053 000053 000053 000053 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153 000153	0000
			7
Pressure	11.78 51.32 2.04 1.98 ACP	000133 000134 000137 000137 000137 000137 000137 000137 000137 000137 000137 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138 000138	
₽ Or		999999999999999999999999999999999999	9
et-Induced 2.5-DW	2.05 1.98 1.98 1.98	0000918 0000918 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181 00000181	000283
Jet- 3C-12-2.5			7
on: 3C	33.89 51.61 2.06 1.99 ACP	0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 0001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115 00001115	000131
rati			٥٠
Configuration:	Point h/De = 1 Thrust = PR Front = PR Aft = c Y-loc	444469888888888888888888888888888888888	1.50
	Total Thi NPR FI NPR A	69999999997949797979797989884984979799999999	

	21.61.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 1.996.1 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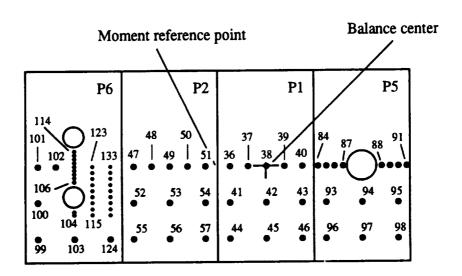


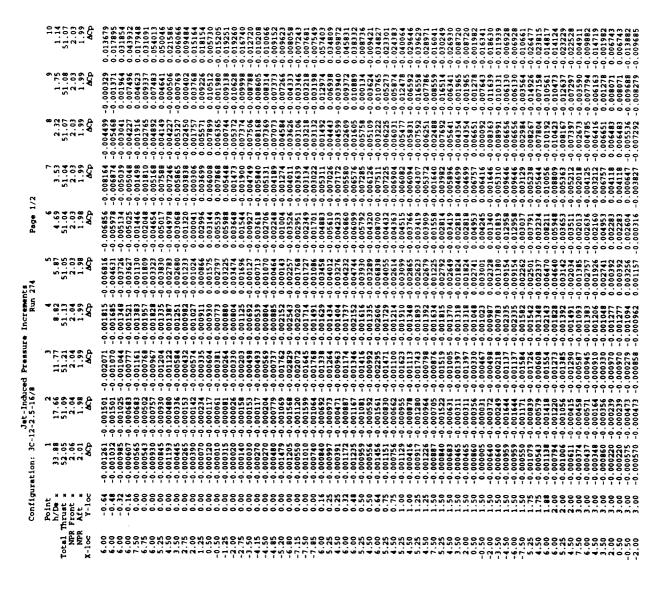
Figure 76. Configuration 3C\_12\_2.5\_16/8;  $D_{\theta} = 1.699$  in.,  $A_{j\theta t} = 2.27$  in.<sup>2</sup>.

Conf. # 3C-12-2.5-16/8

Orif. # 99	Mom. arm 7.5	Sta. y	Δ.Area 4.688	Sta. x 7.5
100	7.165	1.5	4.38	7.5
101	7.5	0	1.313	7.5
102	6.75	0	1.125	6.75
103	6	3 2	5.625	6
104	6		0.278	6
105	6	1.88	0.38	6
106	6	0.64	0.38	6
107	6	0.48	0.24	6
108	6	0.32	0.24	6
109	6	0.16	0.24	6
110	6	0	0.12	6
111	6	-0.16	0	6
112	6	-0.32	0	6
113	6	-0.48	0	6
114	6	-0.64	0	6
115	5.25	2	0.375	5.25
116	5.25	1.75	0.375	5.25
117	5.25	1.5	0.355	5.25
118	5.25	1.25	0.325	5.25
119	5.25	1	0.355	5.25
120	5.25	0.75	0.375	5.25
121	5.25	0.5	0.375	5.25
122	5.25	0.25	0.375	5.25
123	5.25	0	0.188	5.25
124	4.5	3	4.688	4.5
125	4.5	3 2	0.438	4.5
126	4.5	1.75	0.438	4.5
127	4.5	1.5	0.438	4.5
128	4.5	1.25	0.438	4.5
129	4.5	1	0.438	4.5
130	4.5	$\bar{0}.75$	0.438	4.5
131	4.5	0.5	0.438	4.5
132	4.5	0.25	0.438	4.5
133	4.5	0	0.219	4.5
47	3.5	ŏ	1.313	3.5
48	2.75	ŏ	1.125	2.75
49	2.75		1.125	2.73
50	2 1.25	0 0	1.125	2 1.25
51	0.5	ŏ	1.125 1.313	0.5
52	3.5	1.5	3.75	3.5
53	2.3	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5		4.375	3.5
56	2	3	5.25	ວ.ວ າ
57	0.5	3 3 3	4.375	2 0.5
31	0.5	J	4.373	0.5

Conf. # 3C\_12\_2.5\_16/8, continued

Orif.#	Mom. arm	Sta. y	∆.Area	Sta. x
36	-0.5	0	1.313	-0.5
37	-1.25	0	1.125	-1.25
38	-2	0	1.125	-2
39	-2.75	0	1.125	-2.75
40	-3.5	0	1.313	-3.5
41	-0.5	1.5	3.75	-0.5
42	-2	1.5	4.5	-2
43	-3.5		3.75	-3.5
44	-0.5	3	4.375	-0.5
45	-2	3	5.25	-2
46	-3.5	3	4.375	-3.5
84	-4.15	1.5 3 3 3 0	0.634	-4.15
85	-4.5	0	0.683	-4.5
86	-4.85	0	0.683	-4.85
87	-5.2	0	0.619	-5.2
88	-6.8	0	0.619	-6.8
89	-7.15	0	0.683	-7.15
90	-7.5	0	0.683	-7.5
91	-7.85	0	0.634	-7.85
93	-4.5	1.5	3.19	-4.5
94	-6	1.5	5.062	-6
95	-7.5	1.5	3.19	-7.5
96	-4.5	3	4.375	-4.5
97	-6	3 3 3	5.25	-6
98	-7.5	3	4.375	-7.5



	Configu	Configuration: 3C-12-2.5-16/8	-12-2.5-16		Run 274	n 274	Page 2/2	2/2			
	Point	-	~	E ;	7	٠,	9	7	<b>6</b>	•	2:
	h/De =		17.66	11.77	8.82		4.69	3.53	2.32		1.14
Total	Thrust =		51.09	51.21	51.13		51.04	51.04	51.07	51.08	51.07
MPR	Front .		2.04	2.04	7.0		2.03	2.03	2.03	2.03	2.03
KGN	Aft =		1.98	1.99	1.99		1.98	1.99	1.99	1.99	1.99
X-10c	Y-10c		₽Ç₽	\$	₽Ç		₽ Q	₽Ç₽	<b>Q</b>	ĝ	Ş
-3.50	3.00	-0.000450	-0.000433	-0.001549	-0.001221	-0.000428	-0.002339	-0.005188	-0.006575	-0.007470	-0.010226
-4.50	3.00	-0.000550	-0.001171	-0.001584	-0.001582	-0.002262	-0.003037	-0.003129	-0.002984	-0.003564	-0.010661
-6.00	3.00	-0.000480	-0.000463	-0.000554	-0.000845	-0.002226	-0.003537	-0.004169	-0.003916	-0.004872	-0.007778
-7.50	3.00	-0.000480	-0.000463	-0.000554	-0.000845	-0.002226	-0.003537	-0.004169	-0.003916	-0.004872	-0.007778
Force and	Moment	Summery									
	P/De	33.88		11.77	8.82	5.87	4.69	3.53	2.33	1.75	1.1
Relence	AI./T	-0.013		-0.020	-0.031	-0.017	-0.028	-0.054	-0.09	-0.131	-0.219
Presente	AI./T	-0.015		-0.024	-0.035	-0.027	-0.041	-0.056	-0.081	-0.108	-0.194
a Company	Z/A	-0.005		0.001	0.007	-0.005	0.018	0.038	0.043	0.043	0.070
Presente	£/4	0.001	0.010	0.003	0.00	0.027	0.074	0.071	9.00	0.096	0.158

	1.74 135.66 4.03 3.98 ACp	-0.006263 -0.002264 -0.003567 -0.003567	1.74 -0.105 -0.084 0.056																						
	2.31 135.65 4.03 3.98 ACP	-0.006762 -0.002615 -0.003558 -0.003558 -0.003558	2.31 -0.082 -0.069 0.045																						
	3.50 135.59 4.03 3.98 ACP	-0.004804 -0.002619 -0.003363 -	3.50 -0.048 -0.051 0.036																						
	4.71 135.56 4.03 3.98 ACP	-0.002740 -0.002230 -0.003166 -0.003166	4.71 -0.022 -0.028 0.032																						
	5.87 135.62 4.03 3.98 ACP	-0.000757 -0.001874 -0.002491 -0.002491	5.87 -0.012 -0.026 0.021																						
	8.83 135.74 4.03 3.99 ACP	-0.000573 -0.001067 -0.000673 -0.000673	8.83 -0.024 -0.028 -0.007 -0.003																						
	11.78 135.86 4.03 3.99 ACP	-0.000440 -0.001641 -0.000588 -0.000588	11.78 -0.015 -0.017 0.003 0.010																						
	17.67 135.94 4.04 3.99 ACP	-0.000262 -0.000961 -0.000277 -0.000277	5Ummary 17.67 -0.010 -0.011 0.000																						
	Point h/De = Thrust = R Front = R Aft = Y-loc	00.00	Moment :: h/De :: AL/T = AL/T = AL/T = M/TDe :: M/TDe ::																						
	Total 1 NPR NPR X-loc	0000	rorce and Balance Pressure Balance /																						
	135.66 4.03 3.98 ACP				0.005561 0.008127 0.007843	0.007105 0.007105 0.006517	0.005214 0.003985 0.002797	0.002308	0.004712	0.002933 0.006603 0.006630	0.002621	0.005259	0.010944	0.013005 0.006665	0.00/009 0.012311 0.006455	0.003520	0.004631 0.004031	0.008498	0.003647	0.006491	0.009364	0.007263	0.006585	0.004684	0.008017
		003381 0.003790 004375 0.001155 003721 0.004291 003797 0.06877 002026 0.002716	.002410 0.005888 .004927 0.001458 .006487 -0.002352 .006365 -0.001971	000054 0.002583 006688 0.007560 009156 0.009397	001185 004831	006655 007544 006425	004858 002194 003037	002462	003577	006487	005191	004736	004569	004546	005454	005964	002646 002646	007995	004728 002615	007372	010198	008244	005595	005979	.003709
	7.31.1.2.65.135.98.3.36.09.39	009020 -0.003881 0.003790 005615 -0.004375 0.001155 005069 -0.003721 0.004291 004224 -0.003721 0.006877 001152 -0.003205 0.002716	004658 -0.003474 0.005588 006658 -0.003474 0.001221 006025 -0.004927 0.001458 005574 -0.006487 -0.00252 004574 -0.006345 -0.001971 0025954 -0.002945 -0.000844	000650 0.000054 0.002583 003799 0.006688 0.007560 008341 0.009156 0.009397 006888 0.006551 0.002166	003522 0.001189 000282 -0.004831 002939 -0.006572	004400 -0.006655 005532 -0.007544 004293 -0.006425	-0.004858 -0.002194 -0.003037	0.002462	0.003577	.005811 -0.006487 .005427 -0.003731 .006557 -0.003741	.005450 -0.005191 .005400 -0.007112	.005016 -0.004736 .005213 -0.007626	003505 -0.004569	.002084 -0.004546 .004982 -0.005962	.001930 -0.005454 .001930 -0.005454 .004047 -0.007299	003206 -0.005964	004708 0.008645 001725 -0.006465	.005553 -0.007995 .010208 -0.004728	.010208 -0.004728 .002619 -0.002615	004254 -0.007372 011981 -0.011608	007516 -0.010198	004508 -0.008244 001985 -0.002573	.003876 -0.005595 .002580 -0.006527	.006135 0.008635 .004043 0.005979	.000090 -0.003709 .003311 -0.006956
nts 275	3.50 2.31 135.59 135.65 135 4.03 4.03 4.05 3.98 3.98 3.98 4.09	007497 -0.009020 -0.003881 0.003790 006825 -0.006115 -0.004375 0.001155 005137 -0.005169 -0.003721 0.004291 004435 -0.004224 -0.003797 0.006877 0070102 -0.001162 -0.00226	004475 - 0.004658 - 0.003410	001760 0.000650 0.000054 0.002583 004329 0.003799 0.006888 0.007560 004310 0.005156 0.009397 005271 0.006888 0.005551 0.005888 0.005551	005372 0.003522 0.001185 002525 -0.000282 -0.004831 000244 -0.002939 -0.006572	001347 -0.004400 -0.006655 002554 -0.005532 -0.007544 003114 -0.004293 -0.006425	001721 -0.003194 -0.004858 001280 -0.000119 -0.002194 004166 -0.003614 -0.003037	002391 -0.002893 -0.002462 002304 -0.002611 -0.002389 002003 -0.002513 -0.00258	004977 -0.005056 -0.003577 003974 -0.005805 -0.005628	003897 -0.005811 -0.006487 005552 -0.005427 -0.003731 005802 -0.006557 -0.003741	004492 -0.005450 -0.005191 003386 -0.005400 -0.007112 008808 -0.005432 -0.004535	.003970 -0.005016 -0.004736 .003087 -0.005213 -0.007626	001700 -0.003505 -0.004569	001475 -0.002084 -0.004546 002344 -0.004982 -0.005962	001480 -0.001/26 -0.002296 001151 -0.001930 -0.005454 002717 -0.004047 -0.007299	001502 -0.003206 -0.005964 001502 -0.003206 -0.005964	005118 0.006135 0.008635 004877 0.004708 0.002646 001303 -0.001725 -0.006405	002157 -0.005533 -0.007995 011310 -0.010208 -0.004728	011310 -0.010208 -0.004728 002230 -0.002619 -0.002615 002363 -0.002648 -0.007262	002189 -0.004254 -0.007372 002189 -0.004254 -0.007372 008524 -0.011981 -0.011608	006631 -0.007516 -0.010198 002759 -0.004825 -0.008040	002290 -0.004508 -0.008244 001679 -0.001985 -0.002573	002438 -0.003876 -0.005595 001191 -0.002580 -0.006527	003327 0.004135 0.008635 003327 0.004043 0.005979	.001992 0.000090 -0.003709 .001992 0.000090 -0.003709 .000860 -0.003311 -0.006956
re Increments Run 275	4 5 6 7 3.50 2.31 1 135.62 135.56 135.59 135.65 135 4.03 4.03 4.03 4.03 3.98 3.98 3.98 3.98 3.98	-0.006846 -0.007497 -0.009020 -0.003881 0.003790 -0.003882 -0.006885 -0.006815 -0.004375 0.00155 -0.004331 -0.005187 -0.005069 -0.003721 0.004291 -0.003321 -0.004485 -0.004224 -0.003797 0.0068877 -0.00656 -0.001002 -0.001162 -0.002026 0.002716	-0.003112 -0.004478 -0.00458 -0.003474 0.005221	0.001751 0.001760 0.000650 0.000054 0.002583 0.001718 0.004329 0.003799 0.006688 0.007560 0.003758 0.004910 0.008341 0.009156 0.009397 0.005688 0.005771 0.005688 0.005771 0.005688	0.002363 0.005372 0.00552 0.00188 0.002426 0.002525 -0.000282 -0.00483 0.000746 0.000244 -0.002939 -0.006572	-0.000153 -0.001347 -0.004400 -0.006655 -0.001364 -0.002554 -0.005532 -0.007544 -0.001479 -0.003114 -0.004293 -0.006425	-0.000924 -0.001721 -0.003194 -0.004858 0.000828 0.001280 -0.000119 -0.002194 -0.002620 -0.004166 -0.003614 -0.003037	-0.001674 -0.002391 -0.002893 -0.002462 -0.001515 -0.002304 -0.002611 -0.002389 -0.001794 -0.002003 -0.00273 -0.0026	-0.003174 -0.004977 -0.005056 -0.00577 -0.003357 -0.003974 -0.005805 -0.005628	-0.002188 -0.003897 -0.005811 -0.006487 -0.003812 -0.005552 -0.005427 -0.003731 -0.005827 -0.005802 -0.005557 -0.004741	-0.003558 -0.004492 -0.005450 -0.005191 -0.001872 -0.003386 -0.005400 -0.007112 -0.006930 -0.00808 -0.005430 -0.00475	0.002757 -0.003970 -0.005016 -0.004736 -0.001655 -0.003087 -0.005213 -0.007626	0.001388 -0.001700 -0.003505 -0.004569 -0.001481 -0.002676 -0.004765 -0.006500	-0.000751 -0.001475 -0.002084 -0.004546 -0.001598 -0.002344 -0.004982 -0.005962	-0.001/3 -0.001480 -0.001/26 -0.002296 -0.001163 -0.001151 -0.001930 -0.005454 -0.001406 -0.002717 -0.004047 -0.007299	0.000863 -0.001502 -0.003206 -0.005964	0.004838 0.005118 0.006135 0.008635 0.004453 0.004877 0.004708 0.002646 0.001477 0.001303 0.001725 0.006405	0.001132 -0.002157 -0.005553 -0.007995	0.010604 -0.011310 -0.010208 -0.004728 0.001874 -0.002219 -0.002619 -0.002615 0.001611 -0.002363 -0.002348 -0.00272615	0.001041 -0.002189 -0.004254 -0.007372 0.001041 -0.002189 -0.004254 -0.01372 0.007558 -0.008524 -0.011981 -0.011608	0.007097 -0.006631 -0.007516 -0.010198 -0.002182 -0.002759 -0.004825 -0.008040	0.001316 -0.002290 -0.004508 -0.008244 0.001035 -0.001679 -0.001985 -0.002573	0.001675 -0.002438 -0.003876 -0.005595 0.001136 -0.001191 -0.002580 -0.006527	0.000418 0.003118 0.006135 0.008635 0.000418 0.003327 0.004043 0.005979	0.001274 0.001992 0.000090 -0.003709 0.000230 -0.000860 -0.003311 -0.006956
Pressure	4 5 6 7 3.50 2.31 1 135.62 135.56 135.59 135.65 135 4.03 4.03 4.03 4.03 3.98 3.98 3.98 3.98 3.98	-0.006846 -0.007497 -0.009020 -0.003881 0.003790 -0.003882 -0.006885 -0.006815 -0.004375 0.00155 -0.004331 -0.005187 -0.005069 -0.003721 0.004291 -0.003321 -0.004485 -0.004224 -0.003797 0.0068877 -0.00656 -0.001002 -0.001162 -0.002026 0.002716	-0.003112 -0.004478 -0.00458 -0.003474 0.005221	0.001751 0.001760 0.000650 0.000054 0.002583 0.001718 0.004329 0.003799 0.006688 0.007560 0.003758 0.004910 0.008341 0.009156 0.009397 0.005688 0.005771 0.005688 0.005771 0.005688	0.002363 0.005372 0.00552 0.00188 0.002426 0.002525 -0.000282 -0.00483 0.000746 0.000244 -0.002939 -0.006572	-0.000153 -0.001347 -0.004400 -0.006655 -0.001364 -0.002554 -0.005532 -0.007544 -0.001479 -0.003114 -0.004293 -0.006425	-0.000924 -0.001721 -0.003194 -0.004858 0.000828 0.001280 -0.000119 -0.002194 -0.002620 -0.004166 -0.003614 -0.003037	-0.001674 -0.002391 -0.002893 -0.002462 -0.001515 -0.002304 -0.002611 -0.002389 -0.001244 -0.002003 -0.00273 -0.0026	-0.003174 -0.004977 -0.005056 -0.00577 -0.003357 -0.003974 -0.005805 -0.005628	-0.002188 -0.003897 -0.005811 -0.006487 -0.003812 -0.005552 -0.005427 -0.003731 -0.005827 -0.005802 -0.005557 -0.004741	-0.003558 -0.004492 -0.005450 -0.005191 -0.001872 -0.003386 -0.005400 -0.007112 -0.006930 -0.00808 -0.005430 -0.00475	0.002757 -0.003970 -0.005016 -0.004736 -0.001655 -0.003087 -0.005213 -0.007626	0.001388 -0.001700 -0.003505 -0.004569 -0.001481 -0.002676 -0.004765 -0.006500	-0.000751 -0.001475 -0.002084 -0.004546 -0.001598 -0.002344 -0.004982 -0.005962	-0.001/3 -0.001480 -0.001/26 -0.002296 -0.001163 -0.001151 -0.001930 -0.005454 -0.001406 -0.002717 -0.004047 -0.007299	0.000863 -0.001502 -0.003206 -0.005964	0.004838 0.005118 0.006135 0.008635 0.004453 0.004877 0.004708 0.002646 0.001477 0.001303 0.001725 0.006405	0.001132 -0.002157 -0.005553 -0.007995	0.010604 -0.011310 -0.010208 -0.004728 0.001874 -0.002219 -0.002619 -0.002615 0.001611 -0.002363 -0.002348 -0.00272615	0.001041 -0.002189 -0.004254 -0.007372 0.001041 -0.002189 -0.004254 -0.01372 0.007558 -0.008524 -0.011981 -0.011608	0.007097 -0.006631 -0.007516 -0.010198 -0.002182 -0.002759 -0.004825 -0.008040	0.001316 -0.002290 -0.004508 -0.008244 0.001035 -0.001679 -0.001985 -0.002573	0.001675 -0.002438 -0.003876 -0.005595 0.001136 -0.001191 -0.002580 -0.006527	0.000418 0.003118 0.006135 0.008635 0.000418 0.003327 0.004043 0.005979	0.001274 0.001992 0.000090 -0.003709 0.000230 -0.000860 -0.003311 -0.006956
Jet-Induced Pressure 2-2.5-16/8	3 4 5 6 7 1 15.00 13.00 2.31 1 1 15.74 135.56 135.59 135.59 135.59 135.65 135 4 03 4 03 4 03 4 03 4 03 4 03 4 03 4	006846 -0.007497 -0.009020 -0.003881 0.003790 003852 -0.006855 -0.006815 -0.004375 0.001155 004352 -0.005187 -0.005069 -0.003721 0.004291 003321 -0.004455 -0.004224 -0.003797 0.0068877 000526 -0.001002 -0.001162 -0.00202	000644 -0.001373 -0.003112 -0.004478 -0.00458 -0.004514 0.007221 0000795 -0.001371 -0.003112 -0.004478 -0.004522  -0.001795 -0.001371 -0.003111 -0.005144 -0.006025 -0.004927 0.001458  -0.0015131 -0.002253 -0.005144 -0.005574 -0.006487 -0.002352 0.00448 -0.005998 -0.005995 -0.005995 -0.001991  -0.000995 -0.0009975 -0.0009975 -0.000998 -0.0009975 -0.0009978 -0.0009975 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.0009978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.0009978 -0.0009978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000978 -0.000	.000370 -0.000981 0.001751 0.001760 0.000650 0.000054 0.002583 0.00370 -0.001062 0.002583 0.00370 -0.001062 0.001778 0.004329 0.003799 0.005688 0.007560 0.002589 -0.001048 0.0003758 0.004910 0.008341 0.009156 0.009397 0.000329 -0.000870 0.003588 0.00571 0.005888 0.00571 0.00756	000211 -0.000734 0.002363 0.005772 0.003522 0.001185 000257 -0.000838 0.00246 0.00255 0.00282 -0.00483 00025 -0.000837 0.000746 0.000344 -0.002939 -0.00657	.000213 -0.000356 -0.000153 -0.001347 -0.004400 -0.005655 0.000402 -0.000154 -0.001564 -0.002554 -0.005532 -0.007546 0.00429 -0.000563 -0.001479 -0.003114 -0.004293 -0.006429	000665 -0.000818 -0.00024 -0.001721 -0.001194 -0.004856 0013350 -0.001125 -0.000828 0.001280 -0.000119 001827 -0.00117 -0.002620 -0.004166 -0.005614 -0.003194	001711 - 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v.vov12490 001158 - 0.001578 - v.vov168 - v.vov	000364 -0.000981 -0.000863 -0.001502 -0.003206 -0.005964	000319 -0.100973 0.1002898 0.003118 0.008135 0.008653 000308 -0.000835 0.004483 0.004877 0.004708 0.002646 000346 -0.006698 0.001477 0.001303 -0.001725 -0.006405	000331 -0.000441 -0.001132 -0.002157 -0.005553 -0.007995 001110 -0.001284 -0.010604 -0.011310 -0.010208 -0.004728	001110 -0.001284 -0.010604 -0.011310 -0.010208 -0.004128 0001641 -0.001067 -0.001874 -0.002230 -0.002619 -0.002615 0001661 -0.001380 -0.001611 -0.002323 -0.002618	000553 -0.001213 -0.001041 -0.002199 -0.004254 -0.007372 001563 -0.001708 -0.001058 -0.008524 -0.011508	001343 -0.001577 -0.007097 -0.006631 -0.007516 -0.010198 000826 -0.001239 -0.002182 -0.002759 -0.004825 -0.008040	000522 -0.001164 -0.001316 -0.002290 -0.004508 -0.008244 000548 -0.001398 -0.001035 -0.001679 -0.001985 -0.002573	000577 -0.001281 -0.001675 -0.002438 -0.003876 -0.005595 000330 -0.001280 -0.005527	000219 -U.000975 U.002898 U.005118 U.006135 U.008635 000628 -U.001052 U.006418 U.003327 U.004043 U.005979 000628 - U.001052 U.00418 U.003337 U.004043 U.005079	000136 -0.000897 0.001274 0.001392 0.000090 -0.003779 000136 -0.000871 0.001274 0.001992 0.000090 -0.003709 000214 -0.000571 0.000230 -0.000860 -0.003311 -0.006956
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	5.87 220.18 6.05 5.91 ACP	-0.001418 -0.001701 -0.001701 -0.001701 -0.0246 -0.0246			
	8.83 220.25 6.05 5.91 ACP	8.83 -0.006771 -0.000771 -0.018 -0.018			
	11.75 220.48 6.05 5.92 ACP	0.005			
	17.66 220.41 6.06 5.92 ACP	Summary 10.000631 -0.000431 -0.000431 17.66 -0.010 -0.014			
	Point h/De = Thrust = R Front = R Aft = Y-loc	3.00 3.00 3.00 3.00 3.00 A.V.T = AL/T = AL/T = AM/TD= = AM/TD= =			
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0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.000179   0.0000179   0.000179   0.000179   0.000179   0.000179   0.000179

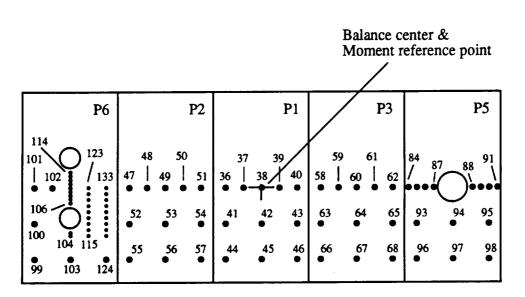


Figure 77. Configuration 3C\_16\_2.5\_20/8;  $D_{\theta}$  = 1.699 in.,  $A_{jet}$  = 2:27 in.<sup>2</sup>.

#### Conf. # 3C-16-2.5-20/8

		_		_
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
99	9.5	3	4.688	9.5
100	9.165	1.5	4.38	9.5
101	9.5	0	1.313	9.5
102	8.75	0 3 2	1.125	8.75
103	8	3	5.625	8
104	8		0.278	8
105	8	1.88	0.38	8
106	8	0.64	0.38	8 8 8 8
107	8	0.48	0.24	8
108	8	0.32	0.24	0
109	8	0.16	0.24	0
110	8	0	0.12	0
111	ð	-0.16	0	8
112	8 8 8	-0.32	0	8 8
113		-0.48	0 0	8
114	8 7.25	-0.64	0.375	7.25
115		2 1.75	0.375	7.25
116	7.25 7.25	1.73	0.375	7.25
117 118	7.25 7.25	1.25	0.335	7.25
119	7.25 7.25	1.23	0.325	7.25
120	7.25	0.75	0.375	7.25
120	7.25 7.25	0.75	0.375	7.25
121	7.25 7.25	0.25	0.375	7.25
123	7.25	0.23	0.188	7.25
123	6.5	3	4.688	6.5
125	6.5	2	0.438	6.5
126	6.5	1.75	0.438	6.5
127	6.5	1.5	0.438	6.5
128	6.5	1.25	0.438	6.5
129	6.5	1	0.438	6.5
130	6.5	0.75	0.438	6.5
131	6.5	0.5	0.438	6.5
132	6.5	0.25	0.438	6.5
133	6.5	0	0.219	6.5
47	5.5	Ŏ	1.313	5.5
48	4.75	Ö	1.125	4.75
49	4	Ö	1.125	4
50	3.25	Ö	1.125	3.25
51	2.5	Ö	1.313	2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4
54	2.5	1.5	3.75	2.5
55	5.5		4.375	5.5
56	4	3 3 3	5.25	4
57	2.5	3	4.375	2.5
	· <del>-</del>	_		

Conf. # 3C\_16\_2.5\_20/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	0	1.313	-1.5
41	1.5	1.5	3.75	1.5
42 43	0	1.5	4.5	0
43 44	-1.5 1.5	1.3	3.75 4.375	-1.5
45	0	3	5.25	1.5 0
46	-1.5	1.5 1.5 3 3 3	4.375	-1.5
58	-2.5	0	1.313	-2.5
59	-3.25	ő	1.125	-3.25
60	-3.23 -4	Ö	1.125	-3.23 -4
61	-4.75	ő	1.125	-4.75
62	-5.5	ŏ	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1 5	4.5	-4
65	-5.5	1.5 3 3 3 0	3.75	-5.5
66	-2.5	3	4.375	-2.5
67	-4	3	5.25	-2.5 -4
68	-5.5	3	4.375	-5.5
84	-6.15	0	0.634	-6.15
85	-6.5	0	0.683	-6.5
86	-6.85	0	0.683	-6.85
87	-7.2	0	0.619	-7.2
88	-8.8	0	0.619	-8.8
89	-9.15	0	0.683	-9.15
90	-9.5	0	0.683	-9.5
91	-9.85	0	0.634	-9.85
93	-6.5	1.5	3.19	-6.5
94	-8	1.5	5.062	-8
95	-9.5	1.5	3.19	-9.5
96	-6.5	3 3 3	4.375	-6.5 -8
97	-8	3	5.25	-8
98	-9.5	3	4.375	-9.5

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Pressure

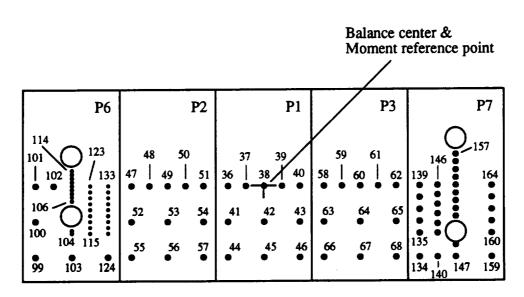


Figure 78. Configuration 4C\_16\_2.5/3.9\_20/8;  $D_e = 1.710$  in.,  $A_{jet} = 2.30$  in.<sup>2</sup>.

Conf. # 4C-16-2.5/3.9-20/8

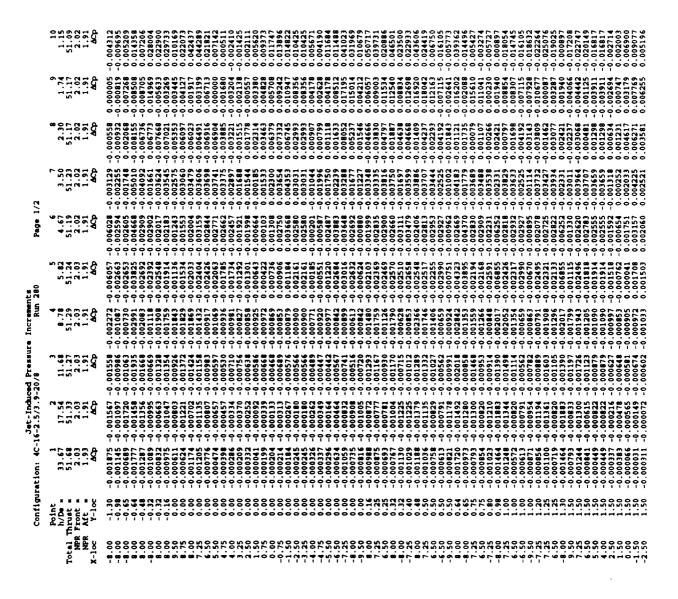
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
99	9.5	3	4.688	9.5
100	9.165	1.5	4.38	9.5
101	9.5	0	1.313	9.5
102	8.75	0	1.125	8.75
103	8	3 2	5.625	8
104	8		0.278	8
105	8	1.88	0.38	8
106	8	0.64	0.38	8
107	8 8 8 8 8	0.48	0.24	8 8 8 8 8
108	8	0.32	0.24	8
109	8	0.16	0.24	8
110	8	0	0.12	8
111	8	-0.16	0	8
112	8	-0.32	0	8
113	8 8 8	-0.48	0	8
114	8	-0.64	0	8
115	7.25	2	0.375	7.25
116	7.25	1.75	0.375	7.25
117	7.25 7.25	1.5	0.355	7.25
118	7.25	1.25	0.325	7.25 7.25
119	7.25	1	0.355	7.25
120	7.25	0.75	0.375	7.25
121	7.25	0.5	0.375	7.25
121 122	7.25	0.25	0.375	7.25
123	7.25	0.23	0.188	7.25
124	6.5	3	4.688	6.5
125	6.5	2	0.438	6.5
126	6.5	1.75	0.438	6.5
127	6.5	1.5	0.438	6.5
128	6.5	1.25	0.438	6.5
129	6.5	1.23	0.438	6.5
130	6.5	0.75	0.438	6.5
131	6.5	0.73	0.438	6.5
132	6.5	0.25	0.438	6.5
132	6.5		0.438	
47	5.5	0	1.313	6.5
		0		5.5
48	4.75	0	1.125	4.75
49	4	0	1.125	4
50	3.25	0	1.125	3.25
51	2.5	0	1.313	2.5
52	5.5	1.5	3.75	5.5
53	4	1.5	4.5	4
54	2.5	1.5	3.75	2.5

Conf. # 4C\_16\_2.5/3.9\_20/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
55	5.5	3 3 3	4.375	5.5
56	4	3	5.25	4
57	2.5	0	4.375	2.5
36 37	1.5 0.75	0	1.313 1.125	1.5 0.75
37 38	0.73	0	1.125	0.73
36 39	-0.75	0	1.125	-0.75
40	-1.5	Ö	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
43	-1.5	1.5	3.75	-1.5
44	1.5	3	4.375	1.5
45	0	3 3 3 0	5.25	0
46	-1.5	3	4.375	-1.5
58	-2.5		1.313	-2.5
59	-3.25	0	1.125	-3.25
60	-4	0	1.125	-4
61	-4.75	0	1.125	-4.75
62	-5.5	0	1.313	-5.5
63	-2.5	1.5	3.75	-2.5
64	-4	1.5	4.5	-4
65	-5.5	1.5	3.75	-5.5
66	-2.5	3	4.375 5.25	-2.5 -4
67 68	-4 5 5	3	4.375	- <del></del> -5.5
134	-5.5 -6.5	3 3 3 2 1.5	3.063	-6.5
135	-6.5	2	0.875	-6.5
136	-6.5	15	0.875	-6.5
137	-6.5	1.5	0.875	-6.5
138	-6.5	0.5	0.875	-6.5
139	-6.5		0.438	-6.5
140	-7.25	0 3 2	2.625	-7.25
141	-7.25		0.534	-7.25
142	-7.25	1.6	0.575	-7.25
143	-7.25	1.2	0.6	-7.25
144	-7.25	0.8	0.6	-7.25
145	-7.25	0.4	0.6	-7.25
146	-7.25	0 3	0.3	-7.25
147	-8	3	2.006	-8
148	-8	2.5	0.54	-8
149	-8	1.3	0.54	-8
150	-8	0.975	0.488	-8
151	-8	0.65 0.325	0.488 0.488	-8 -8
152 153	-8 -8	0.323	0.4315	-o -8
153 154	-o -8	-0.325	0.4313	-8
155	-8	-0.65	Ö	-8
156	-8	-0.975	ŏ	-8
157	-8	-1.3	ŏ	-8
159	-9̃.19		5.688	-9.5
160	-9.163	3 2	1.559	-9.5
	- · - <del>-</del> -			

Conf. # 4C\_16\_2.5/3.9\_20/8, continued

Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
161	-9.163	$1.\tilde{5}$	1.6	-9.5
162	-9.163	1	1.625	-9.5
163	-9.163	0.5	1.625	-9.5
164	-9.5	0	0.6255	-9.5



	1.15 51.09 2.02 1.91 ACP	0.0099139 0.025359 0.025359 0.025359 0.01642 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917 0.0108917	1.15 -0.157 -0.130 0.014 0.035
	1.74 51.17 2.02 1.91 ACP	0.000001 0.010973 0.010973 0.010973 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736 0.00736	1.74 -0.100 -0.072 -0.025
	2.30 2.17 2.02 1.91	0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001 0.005001	2.30 -0.076 -0.043 -0.037
2/3	3.50 51.23 2.02 1.91 ACP	-0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550 -0.0010550	3.50 -0.044 -0.044 0.007
Page 2/2	4.67 51.19 2.02 1.91 ACP	0.0000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.000098 0.	4.67 -0.030 -0.033 0.036
ements Run 280	5.82 51.24 2.03 2.03 1.91	00000000000000000000000000000000000000	5.82 -0.026 -0.031 0.030
Jet-Induced Pressure Increments -2.5/3.9-20/8	8.78 51.29 2.03 1.91 ACP	00000000000000000000000000000000000000	8.78 -0.031 -0.035 0.027
ced Pressu 20/8	11.68 51.27 2.03 1.91 ACP	0.000554 0.000554 0.000554 0.000554 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556 0.000556	11.68 -0.024 -0.026 0.037 -0.012
Jet-Indu 16-2.5/3.9	2 17.54 51.33 2.03 1.91 ACP	0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336 0.000336	17.54 -0.018 -0.020 0.055
Jet-Induced Proposition: 4C-16-2.5/3.9-20/8	33.67 51.68 2.03 1.93 ACP	0.000000000000000000000000000000000000	Summary 33.67 -0.015 -0.015 0.059 -0.000
Configur	Point h/De = Thrust = R Front = R Aft = Y-loc		d Moment h/De AL/T AL/T AM/TDe
	Total 1 NPR NPR X-loc	4.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0.0	Force and Balance Pressure Balance

	1.74 136.11 4.00 3.79 ACP	0.000103 -0.010245 -0.010245 -0.010113 -0.00113 -0.00431 -0.00431 -0.00431 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631 -0.00631	1.74 -0.081 -0.016 -0.018
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	3.50 136.28 4.00 3.79 ACP	0.00975 0.002089 0.002089 0.002089 0.001555 0.001555 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089 0.002089	0.038 0.038 0.018 0.018
	4.65 136.26 4.00 3.79 ACD	0.00283 -0.00241 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274 -0.00274	- 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0
	5.83 136.25 4.00 3.79	0.000564 0.001882 0.001882 0.001884 0.001889 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899 0.001899	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	8.76 136.32 4.00 3.79 ACP	0.000014 0.000584 0.000584 0.000457 0.001584 0.001584 0.001584 0.001584 0.001584 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588 0.001588	8.76 -0.023 -0.027 -0.012 -0.029
	8.75 136.29 4.01 3.79 ACP	-0.000382	8. -0.018 0.0010 0.006
	17.55 136.31 4.01 3.79	0.000344	Stumporty 5.55 -0.013 -0.013 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -0.003 -
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	Total T NPR NPR X-loc	4 N N N N L L L R R R L R N L L N R R R R	Force and Balance Pressure Pressure
	1.74 136.11 4.00 3.79 ACP	0.004061 0.001738 0.004716 0.009892 0.008811 0.004116 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811 0.008811	0.002174 0.01394 0.011996 0.011996 0.013123 0.0188439 0.01884334 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188346 0.0188392 0.0188392 0.0188392 0.0188392 0.0188392 0.0188392
	- 10 - E	0.000158 0.000158 0.0001742 0.001337 0.001338 0.001358 0.001358 0.001766 0.001766 0.001766 0.001766 0.001766 0.001766 0.001766 0.001766 0.001766 0.001736 0.001736 0.001736 0.001736 0.001736 0.001736 0.001736	0.000286 0.000287 0.000287 0.000274 0.000374 0.000374 0.000387 0.000387 0.000387 0.000387 0.000388 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389 0.000389
	2.32 36.20 4.00 4.00 ACP	0.002881 -0.00158 -0.00158 -0.00158 -0.001518 -0.000157 -0.001442 -0.001442 -0.001445 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.001344 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.0014418 -0.	0.001190 -0.000186 0.002191 0.000257 0.002687 0.000574 0.001688 0.000574 0.002111 0.000314 0.002111 0.000316 0.002111 0.000491 0.002111 0.00491 0.002111 0.00491
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Jet-Induced Pressure: 4C-16-2.5/3.9-20/8	7.55 8.75 8.76 5.83 4.65 3.50 2.32 1 6.31 136.29 136.32 136.25 136.26 136.28 136.20 136 4.01 4.01 4.00 4.00 4.00 4.00 4.00 4.00	000556 -0.000817 -0.001701 -0.003201 -0.004766 -0.002881 -0.000158 0000550 0000550 -0.001699 -0.001618 -0.002501 -0.001618 -0.000153 0000552 0000652 0000657 -0.001618 -0.0001518 -0.001618 -0.001618 -0.001618 00001518 -0.001618 -0.001618 -0.001618 00001518 -0.001618 00001518 -0.001618 00001518 -0.001618 00001518 -0.001618 00001518 -0.001618 00001618 00001618 00001618 00001618 00001617 00001617 00001617 00001617 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 00001618 000	0001317 - 0.0004413 - 0.000713 - 0.000174 - 0.001394 0 0.00218 0 0001344 - 0.001348 - 0.001348 - 0.001348 - 0.001348 - 0.001348 - 0.001348 - 0.001348 - 0.001348 - 0.001349 0 0.00218 0 000175 - 0.001348 - 0.001340 - 0.00218 0 000175 - 0.00144 - 0.001349 - 0.00144 - 0.001349 - 0.00147 - 0.001349 0 0.00217 0 000025 0 000057 0 000053 0 0.00184 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849 - 0.001849
Jet-Induced Pressure 4C-16-2.5/3.9-20/8	7.55 8.75 8.76 5.83 4.65 3.50 2.32 1 6.31 136.29 136.32 136.25 136.26 136.28 136.20 136 4.01 4.01 4.00 4.00 4.00 4.00 4.00 4.00	-1.30 -0.001326 -0.000817 -0.001701 -0.001361 -0.002881 -0.001881 -0.000152 -0.055 -0.055 -0.00550 -0.00550 -0.00550 -0.00550 -0.001518 -0.000525 -0.055 -0.0550 -0.001518 -0.000525 -0.055 -0.00550 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.000517 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001519 -0.001519 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518 -0.001518	16 - 0.000550 - 0.000317 - 0.000413 - 0.0001713 - 0.000174 - 0.0012994   0.002218   0.000500 - 0.000324 - 0.001848   0.0017413 - 0.001741 - 0.0012994   0.002218   0.000500 - 0.000324   0.001741 - 0.001741   0.000218   0.000218   0.000218   0.000218   0.000218   0.000255   0.000505   0.0001894   0.001894   0.001894   0.001894   0.001894   0.001891   0.000255   0.000573   0.000528   0.000573   0.000528   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0.000573   0

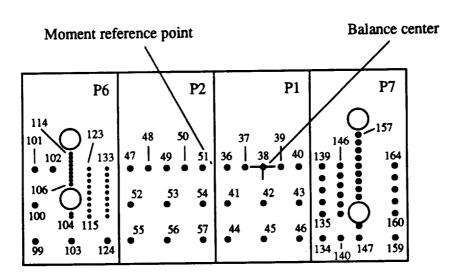


Figure 79. Configuration 4C\_12\_2.5/3.9\_16/8;  $D_e = 1.710$  in.,  $A_{jet} = 2.30$  in.<sup>2</sup>.

#### Conf. # 4C-12-2.5/3.9-16/8

0 '6 "	3.4	σ.		
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
99	7.5	3	4.688	7.5
100	7.165	1.5	4.38	7.5
101	7.5	0	1.313	7.5
102	6.75	0 3 2	1.125	6.75
103	6	3	5.625	6
104	6	2	0.278	6
105	6	1.88	0.38	6
106	6	0.64	0.38	ő
107	ő	0.48	0.24	6
108	6	0.32	0.24	6
100	6	0.16	0.24	6
		0.10		
110	6		0.12	6
111	6	-0.16	0	6
112	6	-0.32	0	6
113	6	-0.48	0	6
114	6	-0.64	0	6
115	5.25	2	0.375	5.25
116	5.25	1.75	0.375	5.25
117	5.25	1.5	0.355	5.25
118	5.25	1.25	0.325	5.25
119	5.25	1	0.355	5.25
120	5.25	0.75	0.375	5.25
121	5.25	0.73	0.375	5.25
122	5.25	0.25	0.375	5.25
123	5.25		0.188	5.25
		0		
124	4.5	3 2	4.688	4.5
125	4.5		0.438	4.5
126	4.5	1.75	0.438	4.5
127	4.5	1.5	0.438	4.5
128	4.5	1.25	0.438	4.5
129	4.5	1	0.438	4.5
130	4.5	0.75	0.438	4.5
131	4.5	0.5	0.438	4.5
132	4.5	0.25	0.438	4.5
133	4.5	0	0.219	4.5
47	3.5	Ŏ	1.313	3.5
48	2.75	ŏ	1.125	2.75
49	2.73	Ŏ	1.125	2.73
	2 1.25	0 0	1.125	1.25
50		0	1.125	
51	0.5	0	1.313	0.5
52	3.5	1.5	3.75	3.5
53	2	1.5	4.5	2
54	0.5	1.5	3.75	0.5
55	3.5	3	4.375	3.5
56	2	3 3 3	5.25	2
57	2 0.5	3	4.375	0.5

Conf. # 4C\_12\_2.5/3.9\_16/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
36	-0.5	0 '	1.313	-0.5
37	-1.25	0	1.125	-1.25
38	-2	$ar{0}$	1.125	-2
39	-2 -2.75	Ö	1.125	-2 -2.75
40	-3.5	0	1.313	-3.5
41	-0.5	1.5	3.75	-0.5
42	-2	1.5	4.5	-0.5 -2
43	-3.5	1.5	3 75	-3.5
44	-0.5	3	4.375	-0.5
45	-0.5 -2 -3.5	3	4.375 5.25 4.375	-0.5 -2 -3.5
46	-3.5	3	4.375	-3.5
134	-4.44	3	3.063	-4.5
135	-4.44	1.5 3 3 3 3 2	0.875	-4.5
136	-4.44	1.5	0.875	-4.5
137	-4.44	1	0.875	-4.5
138	_1 11	0.5	0.875	-4.5
139	-4.44		0.438	-4.5 -5.25
140	-5.25	0 3 2	2.625 0.534	-5.25
141	-5.25	2	0.534	-5.25
142	-4.44 -5.25 -5.25 -5.25 -5.25 -5.25 -5.25	1.6	0.575	-5.25
143	-5.25	1.2	0.6	-5.25
144	-5.25	0.8	0.6	-5.25 -5.25
145	-5.25	0.4	0.6	-5.25
146	-3.23	0	0.3	-5.25
147	-6	3 2.5	2.006	-6
148	-6	2.5	0.54	-6
149	-6	1.3	0.54	-6
150	-6	0.975	0.488	-6
151	-6	0.65	0.488	-6
152	-6	0.325	0.488	-6
153	-6	0	0.244	-6
154	-6	-0.325	0	-6
155	-6	-0.65	0	-6
156	-6	-0.975	0	-6
157	-6	-1.3	0	-6 -7.5
159	-7.19	3	5.688	-7.5
160	-7.163	2	1.559	-7.5
161	-7.163	-1.3 3 2 1.5	1.6	-7.5
162	-7.163	1	1.625	-7.5
163	-7.163	0.5	1.625	-7.5
164	-7.5	0	0.438	-7.5

	Configu	Jec-induced F Configuration: 4C-12-2.5/3.9-16/8	12-2.5/3.5	-16/8	Run	283	Pege 2/2	1/3			
Total 1 NPR NPR X-loc	Point h/De = Thrust = R Front = R Aft = Y-loc	22.93 2.93 1.207 2.93 2.93	17.55 52.52 2.06 1.95 AG	11.72 52.46 2.06 1.95 ACP	8.78 52.39 1.95 ACP	52.38.7 52.38.7 1.955 ACS	4.67 52.33 2.05 1.95 ACP	3.50 52.36 2.05 1.95 ACP	2.28 22.28 2.05 1.95 AQ	22.27 22.27 2.05 1.95 ACP	1.14 52.27 2.05 1.95 0.05
3. 7. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4. 4.		-0.000228 -0.00023 -0.0001099 -0.0001099 -0.000251 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023 -0.00023	-0.001194 -0.000849 -0.0011618 -0.000983 -0.000983 -0.000983 -0.000643 -0.000643 -0.000643 -0.00083 -0.00083 -0.00083 -0.00083 -0.00083 -0.00083 -0.00083 -0.00083	0.001207 0.001264 0.001633 0.001633 0.001373 0.001373 0.000891 0.000881 0.000887 0.000887 0.000887 0.000887 0.000887 0.000887 0.000887 0.000887 0.000887 0.001233	-0.001838 -0.001470 -0.001554 -0.001574 -0.001879 -0.001339 -0.001339 -0.001336 -0.001336 -0.001346 -0.001346 -0.001346 -0.001346 -0.001346	-0.001946 -0.000946 -0.000934 -0.000934 -0.000934 -0.000934 -0.000934 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936 -0.000936	-0.004755 -0.003464 -0.00366 -0.00306 -0.00507 -0.00153 -0.00154 -0.00154 -0.00355 -0.00255 -0.00255 -0.00255 -0.00255 -0.00255 -0.00255 -0.00255	-0.0003030303030303030303030303030303030	0.005341 0.005381 0.005381 0.005381 0.0038236 0.0038236 0.004533 0.004533 0.004533 0.004533 0.004533 0.004533 0.004534 0.004534 0.004534	-0.009263 -0.010221 -0.010221 -0.010328 -0.007261 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368 -0.008368	-0.013614 -0.017815 -0.017815 -0.017815 -0.017816 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818 -0.017818
Force and Balance Pressure Balance Pressure	ভূ বৰ	Homent Summary h/De = 33.67 AL/T = -0.011 AL/T = -0.016 H/TDe = -0.002	17.55 -0.014 -0.019 0.014	11.72 -0.018 -0.024 0.016	8.78 -0.026 -0.035 -0.011	5.87 -0.009 -0.025 -0.036	4.67 -0.007 -0.016 -0.013	3.50 -0.016 -0.025 0.003	2.34 -0.040 -0.041 -0.000	1.74 -0.079 -0.073 -0.006 0.009	1.14 -0.144 -0.131 -0.003

	1.76 135.91 4.02 3.79 ACP	0.000000000000000000000000000000000000
	2.31 135.96 4.02 3.80 ACp	00000000000000000000000000000000000000
	3.47 135.89 4.02 3.80 ACP	0.000000000000000000000000000000000000
	4.68 135.86 4.02 3.80 ACP	0.001594 0.0021817 0.001594 0.001594 0.001594 0.001594 0.001594 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.001694 0.
	5.82 135.82 135.82 3.80 ACP	0.000000000000000000000000000000000000
	8.79 135.88 4.01 3.80 ACp	0.000000000000000000000000000000000000
	11.70 135.88 4.01 3.80 ACP	0.000000000000000000000000000000000000
	17.54 136.01 4.01 3.81 ACP	Manage Ma
	Point h/De = 1 Thrust = R Front = R Aft = r Y-loc	AL/T = 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
	Total Th NPR I NPR X-loc	6 00 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0
	1.76 135.91 4.02 3.79 ACP	0.000000000000000000000000000000000000
	2.31 1.76 135.96 135.91 4.02 4.02 3.80 3.79 ACP ACP	00000000000000000000000000000000000000
	7 2.31 5.96 135 4-02 4 ACP	0.004282 - 0.002865 - 0.003284 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.0032845 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 - 0.003285 -
nts 284	6 2.31 1 3.47 2.31 1 4.02 4.02 4 3.80 3.80 3	0.001582
re Increments Run 284	4.68 3.47 2.31 1 1 2.5.46 135.89 135.96 135 4.02 4.02 4.02 4.02 4.02 ACP ACP ACP	0001819 - 0.001872 - 0.001865 - 0.002066   0004130 - 0.000423 - 0.004589 - 0.002865 - 0.003165   0002131 - 0.000423 - 0.004659 - 0.003165   0002131 - 0.000423 - 0.00446 - 0.003165   0001819 - 0.00287 - 0.002891 - 0.003641   0001819 - 0.00287 - 0.002891 - 0.002641   0001819 - 0.00287 - 0.002891 - 0.002641   0001819 - 0.001819 - 0.001861 - 0.002641   0001819 - 0.001819 - 0.001861 - 0.002641   0001819 - 0.001814 - 0.002715 - 0.002641   0001814 - 0.002811 - 0.002716 - 0.002719   000182 - 0.00184 - 0.001718   000182 - 0.00184 - 0.001718   000182 - 0.00184 - 0.001718   000182 - 0.00184 - 0.001718   000182 - 0.00184 - 0.001718   000182 - 0.00184 - 0.001862   000182 - 0.00184 - 0.001862   000182 - 0.00184 - 0.001862   000182 - 0.00184 - 0.001862   000182 - 0.00184 - 0.001862   000182 - 0.00188 - 0.001862   000182 - 0.00188 - 0.001862   000183 - 0.00188 - 0.002892   000185 - 0.00188 - 0.002892   000185 - 0.00188 - 0.002892   000185 - 0.00188 - 0.002892   000186 - 0.002892 - 0.002892   000187 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.00188 - 0.002892   000188 - 0.001892   000188 - 0.001892   000188 - 0.001892   000188 - 0.001892   000188 - 0.001892   000188 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   000189 - 0.001892   00018
Pressure 8	4 5 6 7 2.31 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.01573 -0.004190 -0.008972 -0.004582 -0.003264 -0.004198 -0.004198 -0.004199 -0.0044199 -0.0044199 -0.0044199 -0.0044199 -0.0044199 -0.004442 -0.004442 -0.004442 -0.004442 -0.004442 -0.004442 -0.004442 -0.004449 -0.004445 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.004449 -0.
Induced Pressure	3 4 5 6 7 7 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	0.001081         0.001081         0.001081         0.001081         0.001081         0.001081         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082         0.001082
Jet-Induced Pressure	1.70 8.79 5.82 4.68 3.47 2.31 1 1 2.5.48 135.82 135.86 135.89 135.96 135.99 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135.90 135	0.001081 - 0.001573 - 0.00248 - 0.008972 - 0.007582 - 0.002066
Induced Pressure	1 2 3 4 5 6 7 7 1.74 11.70 18.79 5 82 4.68 3.47 2.31 1 1 6.01 135.88 135.82 135.86 135.89 135.96 135.94 4.02 4.02 4.01 4.01 4.01 4.01 4.02 4.02 4.02 4.02 3.80 3.80 3.80 3.80 3.80 3.80 3.80 3.80	Control   Cont

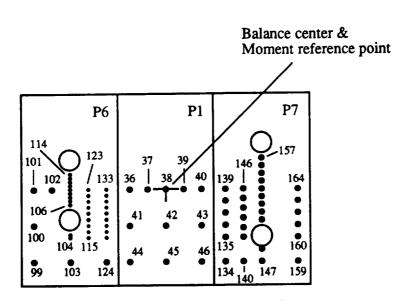


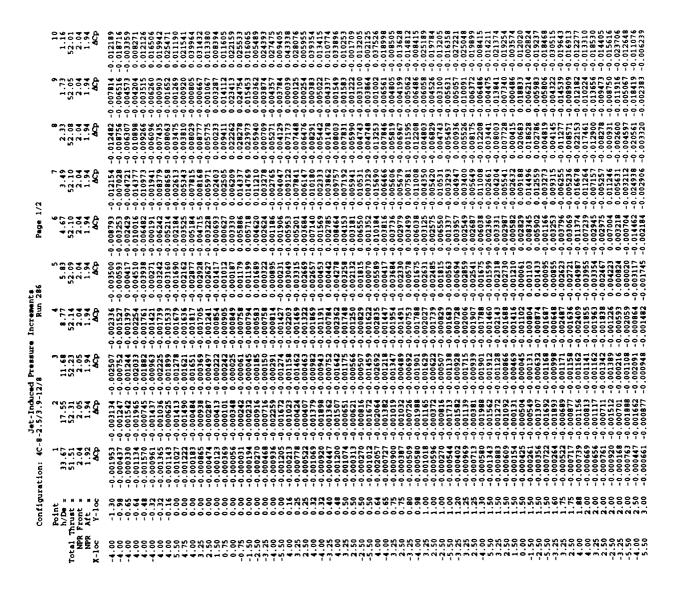
Figure 80. Configuration 4C\_8?2.5/3.9\_12/8;  $D_{\Theta} = 1.710$  in.,  $A_{jet} = 2.30$  in.<sup>2</sup>.

#### Conf. # 4C-8-2.5/3.9-12/8

О-::с н	14	C.	A A	0.
Orif. #	Mom. arm	Sta. y	Δ.Area	Sta. x
99	5.5	3	4.688	5.5
100	5.165	1.5	4.38	5.5
101	5.5	0	1.313	5.5
102	4.75	0	1.125	4.75
103	4	3	5.625	4
104	4	3 2	0.278	4
105	4	1.88	0.38	4
106	4	0.64	0.38	4
107	4	0.48	0.24	4
	4			
108	4	0.32	0.24	4
109	4	0.16	0.24	4
110	4	0	0.12	4
111	4	-0.16	0	4
112	4	-0.32	0	4
113	4 4 4 4	-0.48	0	4
114	4	-0.64	0	4
115	3.25	2	0.375	3.25
116	3.25	1.75	0.375	3.25
117	3.25	1.5	0.355	3.25
118	3.25	1.25	0.325	3.25
119	3.25	1 25	0.355	3.25
120	3.25	0.75	0.375	3.25
121	3.25	0.5	0.375	3.25
122	3.25	0.25	0.375	3.25
123	3.25	0	0.188	3.25
124	2.5	3 2	4.688	2.5
125	2.5	2	0.438	2.5
126	2.5	1.75	0.438	2.5
127	2.5	1.5	0.438	2.5
128	2.5	1.25	0.438	2.5
129	2.5	1.23		
			0.438	2.5
130	2.5	0.75	0.438	2.5
131	2.5	0.5	0.438	2.5
132	2.5	0.25	0.438	2.5
133	2.5	0	0.219	2.5
36	1.5	0	1.313	1.5
37	0.75	0	1.125	0.75
38	0	0	1.125	0
39	-0.75	0	1.125	-0.75
40	-1.5	Ŏ	1.313	-1.5
41	1.5	1.5	3.75	1.5
42	0	1.5	4.5	0
42		1.5		
	-1.5		3.75	-1.5
44	1.5	<u>3</u>	4.375	1.5
45	0	3 3 3	5.25	0
46	-1.5	3	4.375	-1.5

Conf. # 4C\_8\_2.5/3.9\_12/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
134	-2.5	3	3.063	-2.5
135	-2.5	3 2 1.5	0.875	-2.5
136	-2.5	1.5	0.875	-2.5
137	-2.5	1	0.875	-2.5
138	-2.5	0.5	0.875	-2.5
139	-2.5		0.438	-2.5
140	-3.25	0 3 2	2.625	-3.25
141	-3.25	2	0.534	-3.25
142	-3.25	1.6	0.575	-3.25
143	-3.25	1.2	0.6	-3.25
144	-3.25	0.8	0.6	-3.25
145	-3.25	0.4	0.6	-3.25
146	-3.25	Õ	0.3	-3.25
147	-4	ž	2.006	-4
148	-4	0 3 2.5	0.54	-4
149	-4	1.3	0.54	-4
150	-4	0.975	0.488	-4
151	-4	0.65	0.488	-4
152	-4	0.325	0.488	-4
153	-4	0	0.4315	-4
154	-4	-0.325	0	-4
155	-4	-0.65	0	-4
156	-4	-0.975	0	-4
157	-4	-13	0	-4
159	-5.19	3	5.688	-5.5
160	-5.163	3 2 1.5	1.559	-5.5
161	-5.163	1.5	1.6	-5.5
162	-5.163	1	1.625	-5.5
163	-5.163	0.5	1.625	-5.5
164	-5.5	0	0.6255	-5.5
		-	· · · · · ·	



	Confidu	Jet-Induced Confiduration: 4C-8-2,5/3,9-12/	Jet-Induced -8-2.5/3.9-12/8	12/8	ire Increments Run 28	1 286	Pege 2/2	2/2			
	Po de	-	•		•	•			•	•	10
		13 67	17.55	11.68	77.8	5.8	4.67	3.49	2.33	1.73	1.16
Total	Thurst I	51.51	52.31	52.23	52.14	52.09	52.10	52.10	52.08	52.05	52.01
2	Pront =	2.04	2.05	2.05	70.0	7.6	7.0	2.04	2.04	2.04	2.04
2		1.92	1.9	1.94	1.94	1.94	1.94	1.94	1.94	1.9	1.94
X-10c	Y-100	<b>₽</b>	Ş	₽ÇЪ	Q Q	₽ P	<b>P</b> CS	₽Ç9	₽ P	Q.	₽
00.₹	3.00	-0.000665	-0.000732	-0.000879	-0.001460		-0.003748	-0.005652		-0.007185	-0.009239
2.50	3.00	-0.000739	-0.000822	-0.001012	-0.001366	-0.001474	-0.002631	-0.005679	-0.007809	-0.009738	
1.50	3.00	-0.000594	-0.000897	-0.000495	-0.001395	-0.001018	-0.000471	-0.001058	-0.002653	-0.004548	-0.005414
0.0	3.00	-0.000527	-0.000887	-0.000959	-0.001537	0.000339	0.005809	0.008148	0.008829	0.004538	0.004314
-1.50	3.00	-0.000819	-0.000529	-0.000888	-0.001360	0.002070	0.007176	0.011498	0.003281	-0.005658	-0.007487
-2.50	3.00	-0.000880	-0.001037	-0.001193	-0.001110	0.002660	0.004932	0.005419	-0.005215	-0.010575	-0.009248
-3.25	3.00	-0.000122	-0.000481	-0.000145	-0.000523	0.000493	0.002770	0.001006	-0.008163	-0.012233	-0.010308
00.	3.00	-0.000453	-0.001442	-0.001088	-0.000789	0.000221	-0.003363	-0.005259	-0.009404	-0.009754	-0.007297
-5.50	3.00	-0.000956	-0.001497	-0.000893	-0.001557	-0.000156	-0.000618	-0.002373	-0.004220	-0.004146	-0.004920
Force and	d Moment	Summary						:	;		,
	h/De	33.67	17.55	11.68	6.77		4.67	3.49	2.33	1.73	1.16
Belance		-0.013	-0.015	-0.018	-0.023	-0.00	0.010	0.011	-0.017	-0.056	-0.115
Pressure		-0.013	-0.019	-0.017	-0.027	-0.010	0.009	0.014	-0.003	-0.042	-0.078
Balance		-0.010	-0.012	-0.011	-0.014	-0.045	-0.053	-0.065	-0.024	-0.001	0.050
Pressure	AM/TDe .	-0.003	900.0	-0.004	-0.005	-0.042	-0.064	-0.085	-0.042	0.012	0.046

	1.74 135.94 4.01 3.78	-0.006540 -0.008480 -0.004032 0.005261 -0.0088478 -0.011615 -0.009449	4 8 4 5 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6 6	
	2.32 135.98 4.01 3.79	-0.006387 -0.006512 -0.001646 0.01067 -0.004030 -0.009688 -0.010503	0.002 0.002 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004 0.004	
	3.49 136.01 4.01 3.79 ACP	-0.005311 -0.003209 0.00742 0.010203 0.01033 -0.001743 -0.006719	E 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	4.67 135.91 4.01 3.79 AQP	-0.003551 0.002291 0.006943 0.007906 0.003983 0.001505	- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	5.83 135.88 4.01 3.79 ACP	-0.002271 -0.001185 0.002478 0.003633 0.00363	5.83 0.007 -0.007 -0.007	
	8.77 135.94 4.01 3.79 ACP	-0.0010245 -0.0010247 -0.0010247 -0.001098 -0.001098 -0.001455 -0.001455	- 0 0 1 2 4 2 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	
	11.68 136.07 4.01 3.79	0920 0912 0913 0913 0913 0913 0913 0913 0913 0913	- 0.016 - 0.016 - 0.005 - 0.005	
	17.54 136.13 4.01 3.80 ACP	-0.000826 -0.000655 -0.000517 -0.000819 -0.000812 -0.000812 -0.000812	- 1 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	Point h/De = Thrust = R Front = R Aft = Y-loc	M	1 AL	
	Total T NPR NPR X-loc	4.00 2.50 1.50 -1.50 -2.50 -3.25 -4.00 -5.50 -5.50	Pressure Pressure Pressure Pressure	
	1.74 135.94 4.01 3.78 ACP	0.00297 0.007662 0.007643 0.002449 0.00262 0.001198 0.00159 0.00159	0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.015595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0.0159595 0	-0.003013
	2.32 1.74 135.98 135.94 4.01 4.01 3.79 3.78 ACP ACP	001347 001347 001570 001521 000547 00047	0.07439 - 0.001555 0.001558 0 0.001555 0.001553 0 0.001553 0.001553 0 0.001553 0.001553 0 0.001553 0.001553 0 0.001545 0.001553 0 0.001545 0.001531 0 0.001545 0.001531 0 0.001545 0.001531 0 0.001555 0.001531 0 0.001555 0.001531 0 0.001555 0.001531 0 0.001555 0.001531 0 0.001555 0.001531 0 0.001555 0.001531 0 0.00155 0.001531 0 0.001555 0.001531 0 0.001535 0.001531 0 0.001535	003019
	6 2.3 3.49 2.32 136.01 135.98 4.01 4.01 3.79 3.79 &CP &CP	0.001822 -0.01347 -0.004583 -0.00592 -0.004583 -0.00592 -0.010973 -0.01250 -0.00974 -0.00562 -0.009459 -0.00847 -0.008459 -0.00847 -0.00455 -0.00472 -0.004365 -0.00472	0.003432 -0.004343 -0.001555 0.004433 -0.001555 0.0015748 -0.001553 -0.001555 0.0015748 -0.001553 -0.001555 0.0015748 -0.001554 -0.001645 0.0015748 -0.001544 -0.001744 0.0001313 -0.00151 -0.001744 0.0001313 -0.001718 -0.001744 0.0001313 -0.001718 -0.001745 0.001751 -0.001718 -0.001745 0.001751 -0.001718 -0.001745 0.001751 -0.001718 -0.001745 0.001751 -0.001745 -0.001746 0.001751 -0.001775 -0.001766 0.001751 -0.001775 -0.001766 0.001751 -0.001775 -0.001766 0.001776 -0.001776 -0.001776 0.001776 -0.001776 -0.001776 0.001776 -0.001776 -0.001776 0.001777 -0.001776 -0.001776 0.001777 -0.001777 -0.001776 0.001777 -0.001776 -0.001776 0.001777 -0.001777 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001779 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001777 -0.001779 -0.001777 0.001779 -0.001779 -0.001777 0.001777 -0.001777 -0.001777 0.001777 -0.001777 -0.001777 0.001777 -0.001777 -0.001777 0.001777 -0.001777 -0.001777	-0.002524 -0.003019
nts 287	6 2.32 6.01 135.98 4.01 4.01 3.79 3.79 ACP ACP	006052 -0.011822 -0.01347 0021921 -0.004359 -0.00592 001322 -0.015370 -0.01550 001725 -0.010977 -0.012570 001569 -0.003960 -0.00562 006480 -0.008459 -0.00847 0023104 -0.004362 -0.00447 0033104 -0.004362 -0.004725	002304 -0.00442 -0.007429 -0.002552	001730 -0.002524 -0.003019
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Jet-Induced Pressure 4C-8-2.5/3.9-12/8	68 8.77 5.83 4.67 3.49 2.32 (0.7 135.94 135.88 135.91 136.01 135.98 (0.1 4.01 4.01 4.01 4.01 4.01 4.01 4.01 4	.001089 -0.001601 -0.001490 -0.001830 -0.006052 -0.011822 -0.013477004044 -0.001039 -0.001079 -0.000331 -0.00155 -0.006483 -0.00792004044 -0.001035 -0.000294 -0.000033 -0.001573 -0.005458 -0.01570001170 -0.00155 -0.00214 -0.005294 -0.00772 -0.11570 -0.1157000471 -0.00141 -0.000320 -0.00189 -0.001569 -0.010977 -0.01207001059 -0.00120 -0.001146 -0.000289 -0.001569 -0.00368 -0.00978 -0.0010101010101010101010101010101010101	0.001339 -0.001346 -0.00239 -0.004423 -0.001555 -0.001548 -0.001555 -0.000444 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001555 -0.000441 -0.001540 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.0015548 -0.001555 -0.000451 -0.001544 -0.001549 -0.001548 -0.0015548 -0.001558 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001554 -0.001556 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001548 -0.001	000646 -0.000168 -0.001048 -0.001340 -0.001330 -0.002524 -0.0033019
Jet-Induced Pressure -2.5/3.9-12/8	1 1.68 8.77 5.83 4.67 3.49 2.32 1.3 136.07 135.54 135.88 135.91 136.01 135.98 1.01 4.01 4.01 4.01 4.01 1.00 3.79 3.79 3.79 3.79 3.79 1.00 MCP ACP ACP ACP ACP ACP ACP	130   -0.001089   -0.001601   -0.001490   -0.003830   -0.006652   -0.011822   -0.013472   -0.003447   -0.000444   -0.001033   -0.0010342   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.007922   -0.00772   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.015701   -0.00772   -0.015701   -0.00772   -0.015701   -0.00772   -0.015701   -0.00772   -0.015701   -0.00772   -0.015701   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.00772   -0.0	Concess   Conc	50 -0.000694 -0.000668 -0.001048 -0.001340 -0.001730 -0.002524 -0.003019

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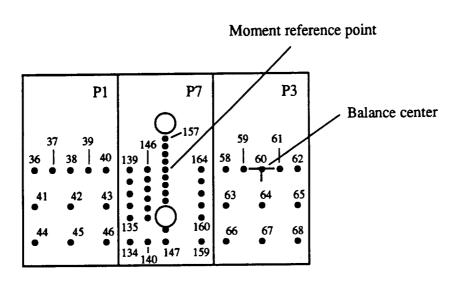


Figure 81. Configuration 2C\_0\_3.9\_12/8;  $D_e = 1.216$  in.,  $A_{jet} = 1.16$  in.<sup>2</sup>.

#### Conf. # 2C-0-3.9-12/8

Orif. # 58 59	Mom. arm -2.5 -3.25	Sta. y 0 0	Δ.Area 1.313 1.125	Sta. x -2.5 -3.25
60	-4	0	1.125	-4
61	-4.75	0	1.125	-4.75
62	-5.5	0	1.313	-5.5 2.5
63 64	-2.5 -4	1.5 1.5	3.75 4.5	-2.5 -4
65	- <del>-4</del> -5.5	1.5	3.75	-5.5
66	-2.5		4.375	-2.5
67	-4	3 3 3 3 2	5.25	-4
68	-5.5	3	4.375	-5.5
134	1.56	3	3.063	1.5
135	1.56		0.875	1.5
136	1.56	1.5	0.875	1.5
137	1.56	1	0.875	1.5
138	1.56	0.5	0.875	1.5
139 140	1.56 0.75	U 2	0.438 2.625	1.5 0.75
140	0.75	0 3 2	0.534	0.75
142	0.75	1.6	0.575	0.75
143	0.75	1.2	0.6	0.75
144	0.75	0.8	0.6	0.75
145	0.75	0.4	0.6	0.75
146	0.75	0	0.3	0.75
147	0	3	2.006	0
148	0	2.5	0.54	0
149	0	1.3	0.54	0
150	0	0.975	0.488	0 0
151 152	0 0	0.65 0.325	0.488 0.488	0
153	0	0.525	0.432	0
154	Ö	-0.325	0.432	ŏ
155	ŏ	-0.65	ŏ	ŏ
156	Ö	-0.975	Ö	Ö
157	Ö	-1.3	0	0
159	-1.19	3	5.688	-1.5
160	-1.163	2	1.559	-1.5
161	-1.163	1.5	1.6	-1.5
162	-1.163	1	1.625	-1.5
163	-1.163	0.5	1.625 0.626	-1.5
164 36	-1.5 5.5	0	1.313	-1.5 5.5
30 37	4.75	0	1.125	4.75
37 38	4.73	0	1.125	4.73
39	3.25	ŏ	1.125	3.25
<b>40</b> ,	2.5	0	1.313	2.5

Conf. # 2C\_0\_3.9\_12/8, continued

Orif. #	Mom. arm	Sta. y	$\Delta$ . Area	Sta. x
41	5.5	1.5	3.75	5.5
42	4	1.5	4.5	4
43	2.5	1.5	3.75	2.5
44	5.5	3	4.375	5.5
45	4	3	5.25	4
46	2.5	3	4.375	2.5

	4.94 26.69 1.00 1.97 ACP	0.000318 0.000318 0.000318 0.0003124 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244 0.0011244	4.94 -0.054 -0.061 -0.022 0.030
	8.22 26.74 1.00 1.97 ACP	0.0001551 0.0001551 0.0001551 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554 0.0001554	8.22 -0.028 -0.026 -0.004 0.006
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	26.58 26.58 1.96 ACP	0.00255 0.00255 0.00251 0.002126 0.002136 0.002136 0.00144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.014491 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.014491 0.014491 0.014491 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0.0144911 0	2.43 -0.188 -0.197 -0.048 -0.011
nts 289	26.41 1.95 1.95 ACP	0.00250430 0.00250430 0.0011100 0.0011100 0.00101100 0.00101100 0.00101100 0.00101100 0.00101100 0.00101100 0.00101100 0.00101100 0.00101100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.00101000 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.00101000 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.00101000 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.0010100 0.00101000 0.00101000 0.00101000 0.00101000 0.00101000 0.00101000 0.0010000 0.00100000 0.00100000 0.00100000 0.00100000 0.00100000 0.00100000 0.00100000 0.00100000 0.00100000 0.0010000000 0.001000000 0.0010000000 0.0010000000000	1.62 -0.308 -0.299 -0.081 -0.034
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ced Pressur	16.46 26.52 1.00 1.96	0.0001449	16.46 -0.004 -0.015 -0.026 0.009
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1.00   0.000015   0.000015   0.000017   0.000017   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.000010   0.	2	, .	-0 000281	-0.000412	9	-0.000427	-0.001026	-0.001617	-0.001234	0
1.00   0.000145   0.000147   0.000175   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.000171   0.	2,5	, .	-0.000115	-0.00009	٩	-0.000317	-0.000801	-0.000694	-0.000752	٥
1.50 1.00 0.000131 0.000133 -0.0001209 -0.000171 -0.0011469 -0.002132 -0.00171 -0.00171469 -0.002132 -0.000131 0.000131 0.000131 -0.000171 -0.00171 -0.00171469 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.0017149 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171 -0.000171	2		-0.000470	-0.000531	9	-0.000752	-0.001501	-0.002381	0.000308	0
1.50 1.00 0.000181 -0.000181 -0.000183 -0.000180 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.000181 -0.0001	5	,	-0.000060	-0.000065	9	-0.000209	-0.000708	-0.001618	-0.002794	٥
1.50	200		-0.000133	-0.000141	٩	-0.000300	-0.000771	-0.001469	-0.002352	٩٠
130 - 0.000051 - 0.000171 - 0.000172 - 0.000172 - 0.001750 - 0.001764 - 0.002717 - 0.001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.0001764 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.000176 - 0.00017	0.75	_	-0.000185	-0.000249	٥	-0.000409	-0.000928	-0.001934	-0.002730	٩
Social Control Contr	00		-0.000470	-0.000531	٩	-0.000752	-0.001501	-0.002381	0.000308	•
1.56	5		-0.000051	-0.000122	٩	-0.000494	-0.000797	-0.001464	-0.002717	٩·
156   1.56   0.000335	9	_	-0.000068	-0.000078	٩	-0.000388	-0.000740	-0.001254	-0.002998	٥٠
1.50 -0.000756 -0.000111 -0.000120 -0.0007458 -0.0007575 -0.0007527 -0.0007518 -0.0007518 -0.0007527 -0.0007518 -0.0007518 -0.0000752 -0.0000752 -0.0007518 -0.0007518 -0.0007518 -0.0007519 -0.0000751 -0.0007518 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.0007519 -0.000751	2.50		-0.000035	-0.000069	٩	-0.000224	-0.000566	-0.001312	-0.004076	٩
1.56	1.50		-0.000076	-0.000111	٥	-0.000462	-0.000763	-0.001426	-0.004148	9 '
1.50	. 50		-0.000149	-0.000300	٩	-0.000458	-0.000846	-0.001727	-0.004501	9
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NBC AL/T = -0.008 -0.009 -0.013 -0.020 -0.030 -0.034 -0.109 -0.109 -0.109 -0.020 -0.035 -0.037 -0.109 -0.037 -0.037 -0.035 -0.035 -0.037 -0.035 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.037 -0.03		h/De	34.6	16.4	12.3	•	Ψ,	4.0	•	7
Bure AL/T = -0.006 -0.009 -0.015 -0.022 -0.036 -0.073 -0.122 -0.026 0.035 0.035 0.015 0.016 0.035 0.035 0.035 0.016	200	1/10	-0.00	-0.00	-0.01	<b>٩</b>	ė,	9.0	P •	ė e
ance AM/TDs = 0.026 0.029 0.030 0.026 0.035 0.033 0.015 0.	- annu		-0.00	-0.00	-0.01	Ŷ	÷	-0.07	P '	ġ
mice 201/ 100 % 0.000 0.000 0.000 0.000 0.000 0.000	1		000	0.02	0.03	•	•	0.03	•	ö
	<b>1</b>			9.0		•	: -	2	9	6
	1									

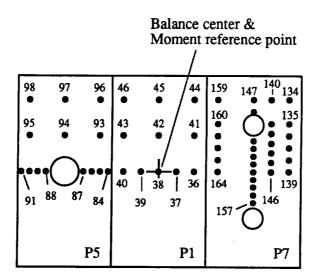


Figure 82. Configuration 3C\_8\_3.9\_12/8;  $D_{\theta}$  = 1.709 in.,  $A_{j\theta t}$  = 2.29 in.<sup>2</sup>.

#### Conf. # 3C-8-3.9-12/8

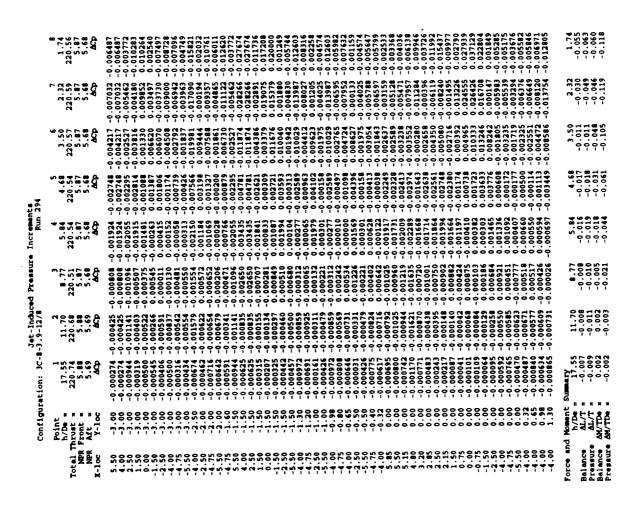
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
134	-5.56	-3	3.063	-5.5
135	-5.56	-2	0.875	-5. <b>5</b>
136	-5.56	-1.5	0.875	-5.5
130	-5.56	-1.5 -1	0.875	-5.5
137	-3.30 5.56	-0.5	0.875	-5.5
	-5.56 5.56	-0. <i>3</i> 0	0.438	-5.5
139	-5.56	-3	2.625	-3.3 4.75
140	-4.75 4.75	-3 -2	0.534	-4.75
141	-4.75		0.575	-4.75 -4.75
142	-4.75	-1.6		-4.13 4.75
143	-4.75	-1.2	0.6	-4.75
144	-4.75	-0.8	0.6	-4.75
145	-4.75	-0.4	0.6	-4.75
146	-4.75	0	0.3	-4.75
147	-4	-3	2.006	-4
148	-4	-2.5	0.54	-4
149	-4	-1.3	0.54	-4
150	-4	-0.975	0.488	-4
151	-4	-0.65	0.488	-4
152	-4	-0.325	0.488	-4
153	-4	0	0.244	-4
154	-4	0.325	0	-4
155	-4	0.65	0	-4
156	-4	0.975	0	-4
157	-4	1.3	• 0	-4
159	-2.81	-3	5.688	-2.5
160	-2.837	-2	1.559	-2.5 -2.5
161	-2.837	-1.5	1.6	-2.5
162	-2.837	-1	1.625	-2.5
163	-2.837	-0.5	1.625	-2.5
164	-2.5	0	0.438	-2.5
36	-1.5	0	1.313	-1.5
37	-0.75	0	1.125	-0.75
38	0	0	1.125	0
39	0.75	0	1.125	0.75
40	1.5	0	1.313	1.5
41	-1.5	-1.5	3.75	-1.5
42	0	-1.5	4.5	0
43	1.5	-1.5	3.75	1.5
44	-1.5	-3	4.375	-1.5
45	0	-3	5.25	0
46	1.5	-3	4.375	1.5
84	2.15	ŏ	0.634	2.15
85	2.5	ŏ	0.683	2.5
86	2.85	ŏ	0.683	2.85
87	3.2	ŏ	0.619	3.2
88	4.8	Ö	0.619	4.8
00	7.0	U	0.017	7.0

Conf. # 3C\_8\_3.9\_12/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
89	5.15	0	0.683	5.15
90	5.5	0	0.683	5.5
91	5.85	0	0.634	5.85
93	2.5	-1.5	3.19	2.5
94	4	-1.5	5.062	4
95	5.5	-1.5	3.19	5.5
96	2.5	-3	4.375	2.5
97	4	-3	5.25	4
98	5.5	-3	4.375	5.5

	Configu	Configuration: 3C-	Jet-Induced 1 -8-3.9-12/8	ced Pressure	ire Increments Run 292	nts 1 292					
	Point h/De	33.71	17.56	11.71	1.78	5.83	4.67	3.48	ભ	1.74	1.14
Total 1	•	53.75	54.30	52.78	52.74	52.64	52.60	52.62	52.66	52.66	52.66
Ž.	-	2.13	2.13	2.02	2.03	2.03	2.63	2.03	2.5	7.03	1.05
X-10c		8	Ŷ	ð	Ş	Q	Q	Q	Ş	Q	₽ C
	-3.00		-0.000635	-0.000489	+69000.0-	-0.002450	0.003647	-0.005006	-0.007027	-0.008451	-0.005883
9.6			ė,	-0.000489	-0.000694	0.002450	0.003647	-0.00000	77		
		-0.000933	٥	-0.000304	-0.000619	-0.001750	0.003913	-0.006562	٠,	-0.01581	
8.0			Ģ	-0.000983	-0.000754	-0.001750	0.002582	-0.002520	7	0	0
-1.50			ဝှဲ	-0.000354	-0.001223	0.000490	0.000575	0.004856	~ `	9	ဗုဗ
-7.50		-0.000/54	۹۹	-0.000366	-0.001512	0.000094	0.000020	-0.005326	ĭĭ	9	9
75			Ģ	-0.000981	-0.000843	0.000263	0.000611	-0.003498	7	٩	ġ.
-5.50		-0.000569	ę.	-0.000778	-0.001022	-0.000238	0.001034	-0.002654	7	9,	ဝှင
9.00		-0.001031	o e	-0.002056	-0.002965	0.002648	0.005602	-0.021748	7 -	7 7	۽ڄ
2.4		-0.000623	99	-0.001407	-0.001304	-0.000442	0.00000	-0.003989	7	٠,	ę
-5.50		-0.000520	-0.000958	-0.000916	-0.001269	-0.000472	0.000572	-0.002166	Τ.	Υ.	9.6
-4.75		-0.000720	٩,	Υ.	-0.001294	-0.001277	0.002053	-0.004487	7 7	7 7	5 6 9 9
200		-0.000955	79	7 7	-0.001647	-0.003065	0.004313	-0.009194	7	~	9
200		-0.001033	۲,	7	-0.001647	-0.003065	0.004313	-0.009194	7	7	9
1.50		-0.000142	۲	7	-0.000150	-0.002405	0.003413	-0.007002	7	Υ.	9
0.0		-0.000563	Ÿ	77	-0.000294	-0.001015	0.001616	0.000150		-	9 0
		-0.000250	77	7 7	-0.001220	0.000636	0.005980	0.012061	_	~Υ	9
a m		-0.000642	,Υ	ĭ	-0.001046	-0.000144	0.000586	-0.002792	7	۲.	
•		-0.001061	Υ,	7	-0.002707	-0.002915	0.006338	-0.011082	īī	77	79
5.75	7.5	-0.000769	-0.0014/3	7 7	966000.0-	0.002240	0.007069	0.014004		, -	9
e un		-0.000598	Υ,	Ŧ	-0.001036	0.000507	0.000741	-0.003006	T	Υ.	٠,
•		-0.001061	Υ.	7	-0.002707	-0.002915	0.006338	-0.011082	7 7	77	7 9
•	9.4	-0.000915	77	7 7	-0.001349	-0.000839	0.002127	-0.005793	īī	ĭŸ	7
	Ď	-0.000326	17	7	-0.000838	0.000651	0.005920	0.013891	_	-	91
L VO	-0.50	9	Υ.	7	-0.001036	0.000507	-0.000741	-0.003006	7 7	77	7 7
••	9.9	99	77	7 7	-0.0013275	0.000690	0.000577	-0.003706	ij	7	7
	8	?	ę	7	-0.000604	-0.002360	-0.002842	-0.003691	ī	7	٩,
5.50	0.00	9	-0.001163	7	-0.000953	-0.002475	-0.002727	-0.003300	ī	77	7 7
5.15	8.6	o c	ဝှင်	7 7	-0.001507	-0.002415	0.003928	-0.004781	1	7	7
20.5	000	? ?	9	1	-0.000858	-0.002765	-0.003032	-0.003386	-	₹	7
2.85	0.0	٩	Ģ	ī	-0.000309	-0.002605	0.002992	-0.006312	1	7 7	ŗ
2.50	9.6	٥٩	ဝှ ရ	7 7	0.000489	-0.002245	0.003793	-0.00/122	1 1	7	79
1.50	88	? ?	9	7	-0.000419	-0.002110	-0,003607	-0.005817	1	7	9
0.75	0.0	9	ę,	7	-0.000145	-0.001510	0.000921	-0.002860	1	7 -	7 -
9.0	88	99	-0.000363	7 7	-0.00018	-0.000465	0.001927	0.009540		_	
-1.50	88	٥٩	ę	7	-0.000494	0.000375	0.005119	0.016537		_	٠.
-2.50	0.0	ı	ę,	1	-0.000957	0.001952	0.005637	0.011965		0.005293	۲
9.4	88	9	-0.000967	1	-0.001116	0.001083	-0.000840	-0.004586		7	ę
-5.50	38	? ?	ė	1	-0.001160	-0.000015	-0.001437	-0.003001		T	ę.
-4.00	0.32	٩,	ှ် ရ	-0.00091	001229	0.000601	0.000318	-0.003373		7 7	
8.8	. a	7 9	9 9	-0.000515	001438	-0.000690	-0.001327	-0.003771	ŀ	7	ö
	1.30	٩	9.0	-0.001035	.002053	-0.001595	-0.002520	-0.008044	1	ī	ဗု
Force and	Moment	Summary						•			
	h/De	= 33.71	17.56	11.71		5.83			2.33		-0.144
Balance	44	9	-0.01	? ?	? ?		7	-0.02		7	
Balance			0.011	•	•		7	-0.07		7	
Pressure	AH/TD•	6	-0.002	٩	•		٢	-0.11		ĭ	

	Configu	onfiguration: 3C	36t- 8-3.9-	ᇫ	ř				
	2	_	11	•		•	•	~	_
Total	Thrust	136.70	136	136	136	136	136	136	136
ž.	Front	86.6	m •	<b>.</b>	m :	m (	m '	~	•
X-10c	Y-10c	Q.							
5.50	-3,00		,	٩	9	3	-0.004166	-0 005823	900
4.00	-3.00		7	٩	9	ī	-0.004166	-0.005823	۰,
	-3.00		1	٩,	9	ī	-0.002956	-0.003662	9
9.50	3,00		1	٩٩	99	1	-0.005497	-0.008361	٩٩
•	-3.00		•	? ?	? 9	, -	0.004076	0.004920	<b>o</b> c
•	-3.00		1	9	•	_	0.004248	0.000220	9
•	-3.00 5.00		1	٩,	9	7	-0.003251	-0.008901	9
	9 9		1 1	99	9	7 7	-0.002037	-0.007241	٩٩
•	2.5		ιī	? 9	٩	īī	-0.015791	-0.020727	? 9
-2.50	2.0		ī	9	0	_	0.008839	0.007194	9
	9 6		+	٩٩	9 9	7	-0.006171	-0.009422	9
	-1.60		īī	? ?	7 9	īī	-0.001539	-0.004824	99
'n	-1.50		7	9	9	Ŧ	-0.002956	-0.003662	? ?
9.0	-1.50		7	٩٠	9	T	-0.007672	-0.012563	9
3.5	7.7		7 7	٩٩	99	7 7	-0.007672	-0.012563	٩٩
0.00	-1.50		iΤ	? 9	9	7	0.001680	0.005888	? 0
~	-1.50		T	9	0	_	0.010008	0.018693	0
~	-1.50		7	٩·	0	_	0.010140	0.008313	0
	1.30		ΤŢ	9	? 9	7 7	-0.002336	-0.005153	٩٩
•	-1.20		7	9	9	т	-0.003903	-0.008350	? ?
re.	 88		7	9	0		0.009905	0.009261	0
0 4	00.1-		7 7	? 9	9	77	-0.001903	-0.004918	99
-4.75	98.0		1	9	0	T	-0.003247	-0.007395	9
71	-0.65		7.	o o	0	7	-0.003745	-0.008763	o,
* •	0.50		īΤ	٩٩	•	7	-0.001903	-0.004918	99
•	0.40		Ŧ	9	0	7	-0.003114	-0.007002	9
~ "	0.0		7 7	99	0		-0.002244	-0.007083	9
5.50	88		T T	9	9	7 7	-0.002998	-0.003695	99
5.15	0.0		7	9	9	7	-0.003212	-0.003601	9
9.6	000		77	99	99	77	-0.003914	-0.004949	o c
2.85	0.0		7	P	9	Ť	-0.004233	-0.006105	٥٥
2.50	88		77	99	99	7`	-0.005016	-0.008936	99
1.55			7	ڄڄ	9	ſΥ	-0.003907	-0.007928	٥٩
57.0	9.0		7	ę,	ę.	۲.	-0.000787	-0.002034	9
90			7	ڄڄ	0		0.011682	0.025668	0
-	0.00	ö	Ŧ	9	0	_	0.015161	0.027950	0
~ 4	9.6		77	99	0 0	~ `	0.011915	0.009917	0 9
•	0.00		7	9	0	-Υ	-0.003452	-0.006350	9
8	9.6	88	-0.000486	ė,	0	۲.	-0.002055	-0.003956	9
, .	0.55		77	9	9		-0.003536	-0.007382	9
88	0.98		77	-0.001130	-0.000218	-0.001359	-0.003745	-0.008263	-0.009304
Force and	4								
•	h/De.	1,5	_;	8.78	8	٠	3.5	۳.	1.7
	AL/1	-0.008	0	2;	-0.015	2		0.04	6
-	AK/17.4	-0.012	o c	ġ	9.5	56	5,5	9,5	9,5
Pressure	AM/TDe =	-0.005		-0.001	-0.049	-0.039	-0.096		.08



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0-4

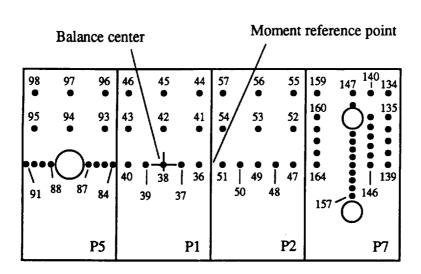


Figure 83. Configuration 3C\_12\_3.9\_16/8;  $D_e = 1.709$  in.,  $A_{jet} = 2.29$  in.<sup>2</sup>.

# Pressure Orifice Locations and Weighting Factors

#### Conf. # 3C-12-3.9-16/8

# Distance from balance center to moment reference point, $X_0 = 0$

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
134	-7.56	-3	3.063	-7.5
135	-7.56	-2	0.875	-7.5
136	-7.56	-1.5	0.875	-7.5
137	-7.56	-1	0.875	-7.5
138	-7.56	-0.5	0.875	-7.5
139	-7.50 7.56	0	0.438	-7.5
	-7.56 -6.75	-3	2.625	-6.75
140	-0.75		0.534	-6.75
141	-6.75	-2	0.334	-0.75 675
142	-6.75	-1.6	0.575	-6.75
143	-6.75	-1.2	0.6	-6.75
144	-6.75	-0.8	0.6	-6.75
145	-6.75	-0.4	0.6	-6.75
146	-6.75	0	0.3	-6.75
147	-6	-3	2.006	-6
148	-6	-2.5	0.54	-6
149	-6	-1.3	0.54	-6
150	-6	-0.975	0.488	-6
151	-6	-0.65	0.488	-6
152	-6	-0.325	0.488	-6
153	<b>-6</b>	0.525	0.244	<b>-6</b>
		0.325	0.244	-6
154	-6	0.65	Ö	-6
155	-6		0	-6
156	-6	0.975		-6
157	-6	1.3	0	
159	-4.81	-3	5.688	-4.5
160	-4.837	-2	1.559	-4.5
161	-4.837	-1.5	1.6	-4.5
162	-4.837	-1	1.625	-4.5
163	-4.837	-0.5	1.625	-4.5
164	-4.5	0	0.438	-4.5
47	-3.5	0	1.313	-3.5
48	-2.75	Õ	1.125	-2.75
49	-2	Ŏ	1.125	-2
50	-1.25	ŏ	1.125	-1.25
	-0.5	ŏ	1.313	-0.5
51	-0.5 -3.5	-1.5	3.75	-3.5
52				-2
53	-2	-1.5	4.5	
54	-0.5	-1.5	3.75	-0.5
55	-3.5	-3	4.375	-3.5
56	-2	-3 -3 -3	5.25	-2
57	-0.5	-3	4.375	-0.5
36	0.5	0	1.313	0.5
37	1.25	0	1.125	1.25
38	2	0	1.125	2
39	2.75	0	1.125	2.75
40	3.5	Ŏ	1.313	3.5
40	٠.٠	0	1.515	5.5

Conf. # 3C\_12\_3.9\_16/8, continued

Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
41	0.5	-1.5	3.75	0.5
42	2	-1.5	4.5	2
43	3.5	-1.5	3.75	3.5
44	0.5	-3	4.375	0.5
45	2	-3	5.25	2
46	3.5	-3	4.375	3.5
84	4.15	0	0.634	4.15
85	4.5	0	0.683	4.5
86	4.85	0	0.683	4.85
87	5.2	0	0.619	5.2
88	6.8	0	0.619	6.8
89	7.15	0	0.683	7.15
90	7.5	0	0.683	7.5
91	7.85	0	0.634	7.85
93	4.5	-1.5	3.19	4.5
94	6	-1.5	5.062	6
95	7.5	-1.5	3.19	7.5
96	4.5	-3	4.375	4.5
97	6	-3	5.25	6
98	7.5	-3	4.375	7.5

8.79 51.23 2.01 1.91	-0.001536 -0.000674 -0.001750 -0.002281 -0.002445	8.79 -0.003 -0.011 0.039 -0.024
5.85 51.27 2.01 1.91 ACD	-0.002453 -0.000862 -0.0004279 -0.006150 -0.006492 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0013871 -0.0	5.85 -0.008 -0.018 0.006 -0.070
3.52 51.31 2.01 1.92 ACP	-0.003726 -0.001493 -0.006355 -0.006259 -0.009145	3.52 -0.042 -0.048 -0.024 -0.076
2.35 51.28 2.01 1.92 ACP	-0.003814 -0.002448 -0.003528 -0.006879 -0.005247	2.35 -0.076 -0.079 -0.034
1.76 51.26 2.01 1.91 ACP	0.001397 0.000036 -0.002643 -0.003872 -0.007279 -0.003117	1,76 -0.118 -0.115 -0.028 -0.095
1.16 51.35 2.01 1.92 ACP	0.025963 0.003060 0.015755 -0.004731 -0.016832	1.16 -0.151 -0.155 -0.023
33.73 51.50 2.01 1.92 ACP	-0.001087 -0.000746 -0.000574 -0.000858 -0.001005	Summary 33.73 -0.014 -0.016 -0.016
Point h/De = Total Thrust = NPR Front = NPR Aft = X-loc Y-loc	0.00 0.32 0.32 0.65 1.30	Homent h/De AL/T AL/T AM/TDe
Total T NPR NPR X-loc	-7.50 -7.50 -6.00 -6.00	Force and Balance Pressure Balance

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Total Threat on 1941-1640a Pressure Increments and the part of the
```

	1.16 136.96 4.03 3.83	0.034116 0.009458 0.023868 0.000703 -0.010104	1.16 -0.122 -0.123 -0.080 -0.068						
	2.33 137.03 4.03 3.83	-0.003240 -0.002211 -0.004340 -0.004490 -0.005401	2.33 -0.057 -0.052 -0.071						
	3.52 137.02 4.03 3.83	-0.002473 -0.001628 -0.004246 -0.005669 -0.008627	3.52 -0.028 -0.027 -0.076						
	4.69 137.05 4.03 3.84 AQD	-0.001 -0.003 -0.005 -0.005	4.69 -0.013 -0.020 -0.061						
	5.84 137.10 4.04 3.84 ACD	-0.001396 -0.000612 -0.002397 -0.003919 -0.006110	5.84 -0.006 -0.008 -0.054						
	8.77 137.29 4.04 3.84	-0.001 -0.001 -0.001 -0.001	8.77 -0.023 -0.025 0.007 0.011						
	11.69 137.32 4.04 3.84 ACP	-0.000638 -0.000638 -0.000659 -0.001097 -0.001118	11.69 -0.015 -0.017 -0.012 -0.004						
	17.57 137.58 4.04 3.86 ACP	-0.000458 -0.000173 -0.00091 -0.000880 -0.000880	Summary 17.57 -0.012 -0.012 -0.010						
	Point h/De = I Thrust = PR Front = PR Aft = Y-loc	0.00 0.00 0.32 0.65 1.30	Homent h/De = AL/T = AL/T = AM/TDe =						
	Total Thr NPR Fr NPR A	-7-50 -7-50 -6-00 -6-00 -6-00	Force and Balance Pressure Balance /						
	1.16 136.96 4.03 3.83 ACP	0.005027 -0.005027 -0.005248 -0.007294 -0.009162	0.008204 0.008204 0.007361 0.006826 0.006240 0.004797	0.014593 0.013257 0.012253 0.018323 0.005248 0.004070	0.006858 0.011887 0.013273 0.002264 0.002840 0.002840	0.017265 0.000267 0.018708 0.012374 0.00267 0.004319	0.002374 0.002374 0.004645 0.004712 0.005322	0.00583 0.00523 0.00523 0.0073 0.012885 0.012885 0.01283 0.01423 0.01423 0.01565	0.013149 0.017958 0.040142
	2.33 137.03 4.03 3.83 AQP	-0.00368 -0.00368 -0.00645 -0.00648	0.0074 0.00921 -0.00561 -0.00864 -0.00287	-0.00518 -0.00488 -0.00281 -0.00476 -0.00480 -0.00480	0.009217 0.009217 0.009217 0.009217 0.001017	0.004891 0.004891 0.002194 0.00456 0.004892 0.004269	0.002562 0.0023513 0.0023513 0.002562 0.002562	0.005120 0.005125 0.005545 0.0056546 0.005657 0.001658	0.001538 0.005267 0.003982
	3.52 137.02 4.03 3.83 ACP	-0.003246 -0.003246 -0.002378 -0.005055 -0.004386	0.005694 0.0076394 0.007512 -0.007512 -0.002154	-0.001692 -0.005233 -0.001857 -0.003955 -0.002378 -0.005691	005835 003793 002134 007638 001372 001372	005923 002622 001815 001341 005332 002332	001341 002253 002474 002593 002593 001710	005125 005473 005473 005486 005028 0101888 0101888	000459 002776 003781
75 296	4.69 37.05 4.03 3.84 ACD	2282444	· ·						777
25	-	-0.0020 -0.0020 -0.0030 -0.0033	0.00273 0.00443 0.00443 0.005183 0.005183 0.001200 0.01200	0.000321 -0.002835 -0.000929 -0.00204 -0.002078 -0.005723	0.001438 0.001246 0.001867 0.004435 0.001577 0.001577 0.000231	0.000469810 0.000469810 0.000469810 0.000469810 0.000469810 0.000469810 0.000469810 0.000469810 0.000469810	0.001591 0.001591 0.002048 0.002165 0.0021165 0.0021165 0.0021165 0.0021165	0.003295 0.003746 0.003284 0.003284 0.00477 0.004117 0.006392 0.006392	0.001519 0.001202 0.002841
re Increments Run 29	5.84 137.10 4.04 3.84 ACP	-0.00205 -0.00205 -0.00173 -0.00135 0.00046	0.0026 0.00270 0.001220 0.001220 0.001288	0.001144 0.00321 -0.001407 -0.002835 -0.000303 -0.000929 -0.001739 -0.002204 -0.005613 -0.005723 -0.005613 -0.005723	0.001962 -0.003438 -0.001246 -0.001246 -0.001246 -0.001246 -0.001247 -0.001867 -0.001577 -0.001867 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 -0.000231 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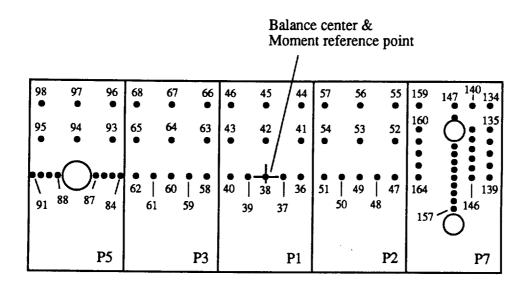


Figure 84. Configuration 3C\_16\_3.9\_20/8;  $D_{\Theta} = 1.709$  in.,  $A_{j\Theta t} = 2.29$  in.<sup>2</sup>.

### Pressure Orifice Locations and Weighting Factors

#### Conf. # 3C\_16\_3.9\_20/8

# Distance from balance center to moment reference point, $X_0 = 0$

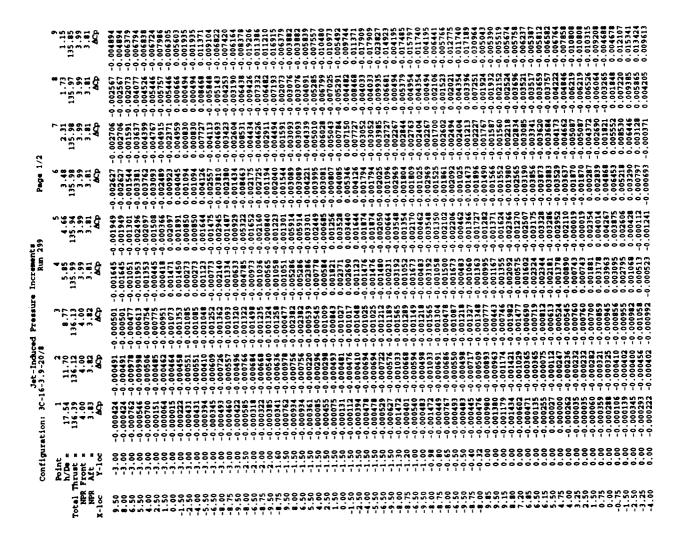
Orif.#	Mom. arm	Sta. y	Δ.Area	Sta. x
134	-9.56	-3	3.063	-9.5
135	-9.56	-2	0.875	-9.5
136	-9.56	-1.5	0.875	-9.5
130	-9.56	-1	0.875	-9.5
137	-9.56	-0.5	0.875	-9.5
138	-9.30 0.56		0.438	-9.5
139	-9.56	0		
140	-8.75	-3	2.625	-8.75
141	-8.75	-2	0.534	-8.75
142	-8.75	-1.6	0.575	-8.75
143	-8.75	-1.2	0.6	-8.75
144	-8.75	-0.8	0.6	-8.75
145	-8.75	-0.4	0.6	-8.75
146	-8.75	0	0.3	-8.75
147	-8	-3	2.006	-8
148	-8	-2.5	0.54	-8
149	-8	-1.3	0.54	-8
150	-8	-0.975	0.488	-8
151	-8	-0.65	0.488	-8
152	-8	-0.325	0.488	-8
153	-8	0	0.244	-8
154	-8	0.325	0	-8
155	-8	0.65	ŏ	-8
155	-8	0.03	ŏ	-8 -8
156	-o -8	1.3	ŏ	-8
157		-3	5.688	-6.5
159	-6.81		1.559	-6.5
160	-6.837	-2	1.6	-6.5
161	-6.837	-1.5		-6.5
162	-6.837	-1	1.625	-6.5
163	-6.837	-0.5	1.625	
164	-6.5	0	0.438	-6.5
47	-5.5	0	1.313	-5.5
48	-4.75	0	1.125	-4.75
49	-4	0	1.125	-4
50	-3.25	0	1.125	-3.25
51	-2.5	0	1.313	-2.5
52	-5.5	-1.5	3.75	-5.5
53	-4	-1.5	4.5	-4
54	-2.5	-1.5	3.75	-2.5
55	-5.5	-3	4.375	-5.5
56	-4	-3	5.25	-4
57	-2.5	-3	4.375	-2.5
3 <i>7</i> 36	-1.5	0	1.313	-1.5
	-0.75	Ö	1.125	-0.75
37		0	1.125	0.75
38	0	0	1.125	0.75
39	0.75		1.123	1.5
40	1.5	0	1.313	1.3

Conf. # 3C\_16\_3.9\_20/8, continued

Orif. # 41 42 43 44 45 46 58 59 60 61 62 63 64 65 66 67 68 84 85 86 87 88 89 90 91 93 94 95	Mom. arm -1.5 0 1.5 -1.5 0 1.5 2.5 3.25 4 4.75 5.5 2.5 4 5.5 2.5 4 5.5 6.15 6.5 6.85 7.2 8.8 9.15 9.5 9.85 6.5	Sta. y -1.5 -1.5 -1.5 -3 -3 -3 0 0 0 0 -1.5 -1.5 -1.5 -3 -3 -3 -3 0 0 0 0 0 0 0 -1.5 -1.5 -1.5 -1.5	Δ.Area 3.75 4.5 3.75 4.375 5.25 4.375 1.313 1.125 1.125 1.313 3.75 4.5 3.75 4.5 3.75 4.375 0.634 0.683 0.683 0.619 0.619 0.683 0.683 0.619 0.619 0.683 0.683 0.694 3.19 5.062	Sta. x -1.5 0 1.5 -1.5 0 1.5 2.5 3.25 4 4.75 5.5 2.5 4 5.5 6.15 6.5 6.85 7.2 8.8 9.15 9.85 6.5 8
93	6.5	-1.5	3.19	6.5
	9.5	-1.5	3.19	9.5
96	6.5	-3	4.375	6.5
97	8	-3	5.25	8
98	9.5	-3	4.375	9.5

	9 10 .02 51.96 .04 2.04 .93 1.93 ACP ACP		999555
	2.32 2.03 2.04 2.04 2.04 2.04 2.04 2.04 3.04 3.04 3.04 3.04 3.04 3.04 3.04 3		05059 0.006 05059 0.006 07147 0.006
	52.09 2.04 1.94 679	0.002758 0.0002758 0.0002758 0.0002758 0.0002758 0.0002758 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.00027768 0.0002777777777777777777777777777777777	0.005224 0.0 0.005224 0.0 0.005573 0.0 0.003057 0.0
Page 1/2	22.67 22.07 1.94 ACP	0.002229 0.002229 0.002229 0.002229 0.002229 0.002229 0.002229 0.002229 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292 0.002292	0.00416 0.00476 0.00331 0.00102
ments un 298	5.86 8.52.08 8.22.08 4.1.94 ACD	4	0.00419 0.00378 0.00229
Pressure Increments Run 298	3 8.79 .71 8.79 .13 52.08 .04 2.04 .94 1.94 ACP ACP		5596 0.0015 5591 0.0008 550 0.0007 550 0.0007
t-Induced Pre-	17.58 11. 52.09 52. 1.93 11.		,,,,,,,
3C-16-3	15.52.2.5 11.56.2.2.9.9	22222222222222222222222222222222222222	99999
Configuration:	oint VDer Sort H SS Y-loc		22222
ខ	E REE	# 9 # # # # # # # # # # # # # # # # # #	0.00 0.11 0.50 0.50 0.50 0.50

	Config	Jet-Indu Configuration: 3C-16-3.9-20/	Jec-Ind	aced Press	Jet-Induced Pressure Increments	ents n 298	Page 2/2	2/2			
	Point	-	79	•	•	5	φ	7	C	đ	-
	# 0/4 	33.71	17.58	11.71	8.79	5.86	4.67	05 E	2 2	1 74	-
Total	Thrust =	52.28	52.09	52.13	52.08	52.08	52.07	52.09	52.03	20.00	F1 . 14
MPR	Front .	2.0	2.0	7.07	2.04	2.04	7.07	20.0	2		20.10
Ž	YEt =	1.94	1.93	1.94	1.94	1.94	1.94	-		5.0	7.0
X-100	Y-10c	Ş	Ş	₽Ç	<b>Q</b>	Q	Q	Ş	8	<b>3</b>	. 93 203
-4.75	0.00	-0.000232	-0.000333	-0.000661	-0.001183	-0 001764	97600 0-	210000		,	. :
-5.50	0.0	-0.000312	-0.000460	-0.000661	-0.001203			0.000.0-	-0.000.0-	0.002206	0.009360
-6.50	0.0	-0.000270	-0.000512	-0.000657	-0.001696	-0.002992	-0.003620	0.003678	007100	/ S#100.0	0.007765
. 8 . 00	0.0	-0.000770	-0.000828	-0.001334	-0.001652	-0.002962	0.002460	-0.00004	AC 100.0-	0.0000	0.01/621
-8.75	0.0	-0.000665	-0.000803	-0.000983	-0.000823	-0.001923	-0.000955	-0.001260	-0.001859	0.00700	0.034987
-9.50	0.0	-0.000840	-0.000994	-0.001229	-0.000683	-0.000853	-0.000788	000000	-0.00543	00.00	0.024069
-8.00	0.32	-0.000290	-0.000864	-0.000858	-0.001646	-0.002631	-0.002079	-0 002148	-0.00033	000000	0.01040
-8.00	0.65	-0.000920	-0.000864	-0.001188	-0.001662	-0.003037	-0.002305	-0.00000	1000000	900000	0.021018
-8.00	0.98	-0.000795	-0.001094	-0.001264	-0.002214	-0.002776	-0.002947	-0.00565	0.002980	0.00186	-0.000186
•••	1.30	-0.001201	-0.001335	-0.001424	-0.002781	-0.005331	-0.004750	-0.003132	-0.003412	-0.001377	-0.012558
Force and	Moment	Sumary									
	h/De	33.71		11.71	8.79	5.86	4.67	2 50	,	. 74	:
Balance	4	-0.013	-0.018	-0.023	-0.010	-0.019	-0.033	-0.047	080	0-110-	1.1
Pressure	7	-0.015		-0.026	-0.022	-0.027	-0.040	-0.055	020	110	
Balance	AN/TD	-0.003		0.005	0.007	-0.043	-0.062	-0.066	-0.074	-0.097	567.0
Pressure	AT/M	-0.001		900.0	-0.005	-0.056	-0.072	-0.075	-0.104	-0.112	-0.114



	Configu	Jet-Inducation: 3C-16-3.9-20/8	Jet-Induced -16-3.9-20/8	iced Pressur/8	• Incr	ements Run 299	Page 2/2	77		
							•			
	Point	-	~1	•	~	••	9	^	•	•
	h/De =	17.54	11.70	8.77	5.85	4.66	3.48	2.31	1.73	1.15
Total .	Thrust =	136.39	136.12	136.13	135.99	135.94	135.98	135.98	135.97	135.85
NP.R	Front =	00· <b>*</b>	₩.00	00· <b>†</b>	3.99	3.99	3.99	3.99	3.99	3.99
ž	Aft.	3.83	3.82	3.82	3.81	3.81	3.81	3.81	3.81	3.81
<b>x</b> -10c	Y-10c	₫	Ş	ξ	₽ P	Ą	₽CD	<b>Q</b>	Q.	Q
-4.75	0.00	-0.000363	-0.000474	-0.000920	-0.001051	-0.001862	-0.001827	-0.001121	0.002545	0.008330
-5.50	0.00	-0.000255	-0.000383	-0.000905	-0.001624	-0.002058	-0.002036	-0.002460	0.001231	0.011570
-6.50	0.0	-0.000360	-0.000419	-0.001143	-0.001855	-0.002581	-0.001746	-0.002073	0.004614	0.028480
. 00 . <del>E</del> -	0.00	-0.000293	-0.000474	-0.001385	-0.001434	-0.001546	-0.001736	-0.001554	0.009197	0.040347
-8.75	0.0	-0.000466	-0.000703	-0.001164	-0.000669	-0.001312	-0.001605	-0.001256	0.004785	0.029891
-9.50	0.0	-0.000324	-0.000557	-0.001162	-0.000321	-0.000511	-0.001257	-0.002029	-0.000160	0.005889
00. <b>B</b> -	0.32	-0.000349	-0.000455	-0.001221	-0.001325	-0.001789	-0.001882	-0.002196	0.005237	0.027275
-8.00	0.65	-0.000349	-0.000784	-0.001177	-0.001701	-0.001939	-0.002010	-0.003132	0.001129	0.005673
-B.00	0.98	-0.000629	-0.000693	-0.001425	-0.002238	-0.002902	-0.002025	-0.003547	-0.002363	-0.005519
- <b>B</b> .00	1.30	-0.001605	-0.000931			-0.004661	-0.002894	-0.002746	0.001359	0.008842
Force and	d Moment Summary	Summary								
	h/De =	17.54	11.70	8.77	5.85	4.66	3.48	2.31	1.73	1.15
Balance		-0.012	-0.015	-0.038	-0.010	-0.022	-0.035	-0.062	-0.082	-0.145
Pressure		-0.014	-0.019	-0.035	-0.019	-0.039	-0.034	-0.059	-0.085	-0.148
Balance		-0.017	-0.012	0.014	-0.048	-0.057	-0.074	-0.063	-0.057	-0.075
Pressure		-0.006	-0.003	0.013	-0.057	-0.075	-0.091	-0.093	-0.083	-0.102

	1.73 220.53 5.89 5.72	0.003093 0.008881 0.008881 0.013765 0.011632 0.011655 0.00159 0.00759	- 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	
	2.32 220.52 5.89 5.72 ACP	-0.000591 -0.0004298 -0.0004298 -0.000524 -0.000224 -0.000203	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.0	
	3.48 220.59 5.89 5.72 5.72	-0.002412 -0.002710 -0.002479 -0.002479 -0.002479 -0.002479 -0.002479 -0.002479 -0.002479 -0.002930 -0.006793	0.000 0.000 0.000 0.000	
	4.66 220.61 5.89 5.72 6Cp	06666	- 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0 - 0	
	5.84 220.64 5.89 5.72 5.72	80000000000000000000000000000000000000	10.00.00.00.00.00.00.00.00.00.00.00.00.0	
	8.75 220.61 5.89 5.72 ACP	-0.000227 -0.000471 -0.0011904 -0.001190 -0.001385 -0.001380 -0.001364 -0.001364	0.0000	
	220.65 220.65 5.90 5.73 ACP	-0.000544 -0.000692 -0.000693 -0.000809 -0.000809 -0.000809 -0.000908	0.00 0.00 0.00 0.00 0.00 0.00 0.00	
	17.54 220.56 25.96 5.90 5.73 ACP	000000000000000000000000000000000000000	▼0.0000 0.00000 0.000000000000000000000	
	Point h/De = Thrust = R Front = R Aft = Y-loc	0.00 0.00 0.00 0.00 0.32 0.32 0.32 1.30	AL/T AL/T AL/T AL/T AL/T AL/T AL/T AL/T	
	Total Ti NPR NPR X-loc	-4.75 -5.50 -6.50 -8.75 -9.50 -8.00 -8.00 -8.00	Balance Pressure Balance Pressure	
		щ	<b>点 4 点 6</b>	
	220.53 5.89 5.72 5.72	002815 002815 002815 004882 005651 006718 000497 0007557 000312	0007350 0007350 00084878 00084878 00094878 00097958 00093380 00093380 0009339 0009531 0009533 0009533 0009533 0009533 0009533 0009533 0009533 0009533 0009533 0009533	0.003989
	2.32 220.52 220.53 5.89 5.89 5.72 Acp Acp	0.002668 0.002815 0.002668 0.002815 0.001555 0.001812 0.004154 0.004882 0.005075 0.00551 0.005100 0.00575 0.007000 0.007557 0.001288 0.000497 0.001288 0.000312 0.001288 0.000312 0.001288 0.000312	0.003562 -0.007350 0.003562 -0.005403 0.003454 -0.006432 0.004454 -0.004458 0.004454 -0.003488 0.004454 -0.003746 0.003543 -0.003746 0.005543 -0.003746 0.005543 -0.00373 0.005543 -0.00373 0.005531 -0.00373 0.005531 -0.003746 0.005531 -0.00374 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005531 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005262 -0.00574 0.005264 -0.00730 0.005264 -0.00730 0.005264 -0.00730 0.005264 -0.00730 0.005264 -0.00730 0.005564 -0.00730 0.005564 -0.00730 0.005661 -0.00730 0.005661 -0.00730 0.005661 -0.00730 0.005661 -0.00730 0.00574 -0.00730 0.00574 -0.00730 0.00574 -0.00730 0.00574 -0.00730 0.00571 -0.00730	-0.000035
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The jet-induced forces generated on short takeoff and vertical landing (STOVL) aircraft when in close proximity to the ground can have a significant effect on aircraft performance. Therefore, accurate predictions of these aerodynamic characteristics are highly desirable. Empirical procedures for estimating jet-induced forces during the vertical/short takeoff and landing (V/STOL) portions of the flight envelope are currently limited in accuracy. The jet-induced force data presented in this report significantly add to the current STOVL configurations data base. Further development of empirical prediction methods for jet-induced forces, to provide more configuration diversity and improved overall accuracy, depends on the viability of this STOVL data base. The data base may also be used to validate computational fluid dynamics (CFD) analysis codes.

This report presents the hover data obtained at the NASA Ames Jet Calibration and Hover Test (JCAHT) facility for a parametric flat-plate model. The model tested was designed to allow variations in the planform aspect ratio, number of jets, nozzle shape, and jet location. There were 31 different planform/nozzle configurations tested. Each configuration had numerous pressure taps installed to measure the pressures on the undersurface of the model. All pressure data, along with the balance jet-induced lift and pitching-moment increments, are tabulated. For selected runs, pressure data will be presented in the form of contour plots that show lines of constant pressure coefficient on the model undersurface. Nozzle-thrust calibrations and jet-flow-pressure survey information are also provided.

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